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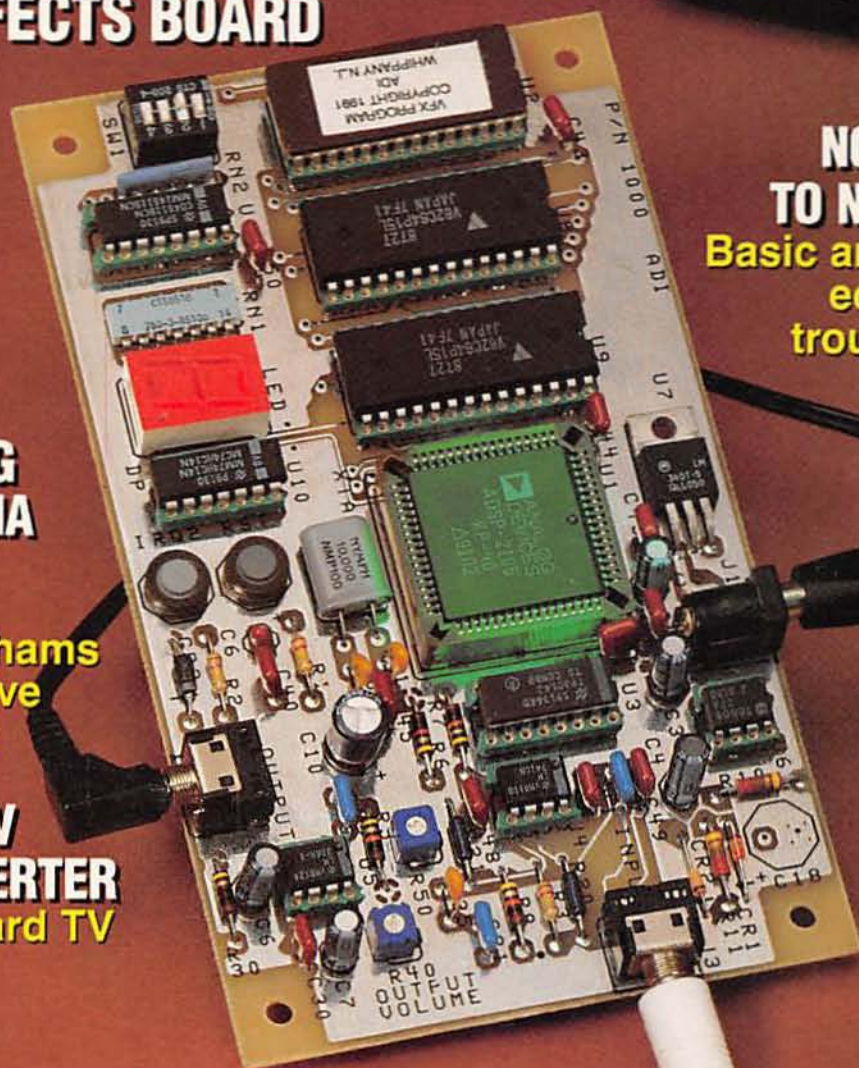
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New! TL75 Hard Point™ Test Leads: Comfort grip with extra strong tips for extended service life.

September 1992 **Electronics NOW**

Vol. 63 No. 9

BUILD THIS

37 VFX DIGITAL SIGNAL PROCESSOR

Use this voice effects processor to change the pitch of your voice and to create special effects.

Craig Borax and David Beck

71 SLOPING VEE ANTENNA

A low-cost boost for your shortwave or ham transmissions.

Richard A. Formata

79 ATV LINEAR AMPLIFIER

Our low-noise downconverter lets you receive amateur TV signals on a standard TV!

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Basic and advanced equipment for troubleshooting local-area networks.

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Learn how to use the 555 in practical timer applications.

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Jeff Holtzman

The 555 A Versatile Timer



Learn to use the 555 and 556 timer IC in practical circuits to obtain accurate time delays and square waves.

The 555 timer IC is a versatile IC that can be used in a wide variety of applications. It is a monolithic integrated circuit that contains all the components of a timer, including a timing network, a flip-flop, and a comparator. The 555 timer is available in two versions: the 555 and the 556. The 555 is a bipolar IC, while the 556 is a CMOS IC. Both versions are available in a variety of packages, including DIP, SOIC, and TO-18. The 555 timer is a very popular IC because of its simplicity and versatility. It can be used to generate square waves, to create time delays, and to control the speed of a motor. The 555 timer is also used in many other applications, such as in pulse generators, frequency dividers, and oscillators. The 555 timer is a very easy IC to use, and it is a great choice for anyone who is interested in electronics.

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Receive amateur TV signals on a standard TV with our downconverter.



ATV Downconverter

The ATV Downconverter is a simple circuit that allows you to receive amateur TV signals on a standard television. It is a very easy circuit to build, and it is a great choice for anyone who is interested in amateur TV. The ATV Downconverter is a very simple circuit that consists of a few basic components, including a diode, a resistor, and a capacitor. The ATV Downconverter is a very easy circuit to build, and it is a great choice for anyone who is interested in amateur TV. The ATV Downconverter is a very simple circuit that consists of a few basic components, including a diode, a resistor, and a capacitor. The ATV Downconverter is a very easy circuit to build, and it is a great choice for anyone who is interested in amateur TV.

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ON THE COVER



One of the latest electronic buzzwords is "digital signal processing" or DSP. We're not surprised to hear so much talk about it. DSP is being used in everything from compact disc players, to weather satellites, to the retrieval of photographs from NASA space missions. If you're curious about DSP technology, turn to page 37. Our VFX Digital Processors lets you take a hands-on approach to an exciting new technology, and have some fun while you're at it. The VFX (voice effects) processor uses DSP techniques to alter the pitch of your voice, or to produce verb and echo effects. It's much less expensive than any commercially available DSP product, and you'll learn about the technology as you build and use it.

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How and why to use a differential probe.

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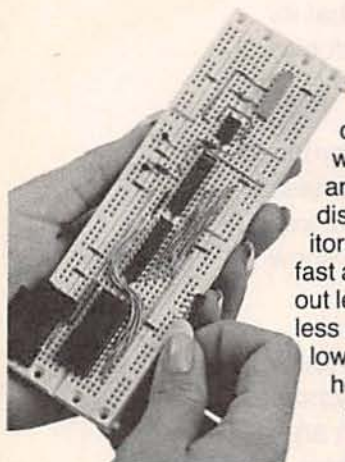
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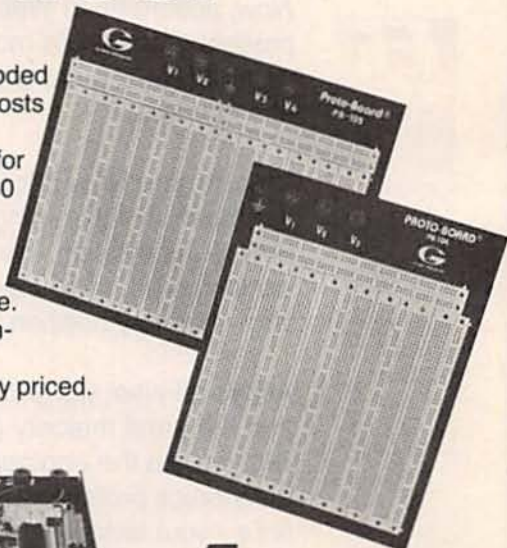


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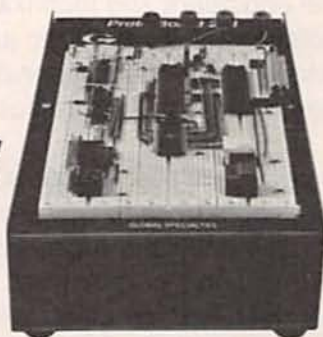
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large numbers of circuits. Here are two oversized PROTO BOARDS Brand, with expanded area, tie points, and more to keep your ideas together. PB-104 features 3,060 tie points, which can handle to 32 16-pin ICs with ease. Four color coded binding posts, and roomy 9.2" x 8" metal panel make it big...but simple. The humungous PB-105 lets you load up to 48 16-pin ICs, and much more onto its



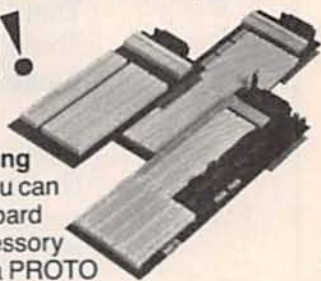
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EDITORIAL

NOW'S THE TIME

Now, according to Webster's New World Dictionary, means "at the present time; at this moment." **Electronics Now** is just what its name implies: a compilation of what is happening in electronics at this moment!

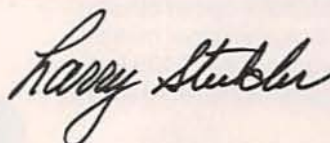
Electronics Now brings you the latest news, the newest products, the most useful training, the most exciting projects, the newest how-to information. We help you learn how it works, how to keep it working, and, of course, how to make your own. We even show you what may happen tomorrow.

Above all else, we remain *your* electronics magazine. We know that the great majority (89%) of you earn your living in electronics. But you are the engineers and technicians to whom being an electronics professional is more than just a job. In your spare time—your leisure time—your personal time—you still want to know and learn more about electronics.

You want to know how Caller ID works. You want to know how digital audio tape compares to digital compact cassettes. You need to know about cellular telephone services and the personal communication networks of tomorrow. You need to know what microprocessor your next computer will have. You have to know what the next generation IC's will be like.

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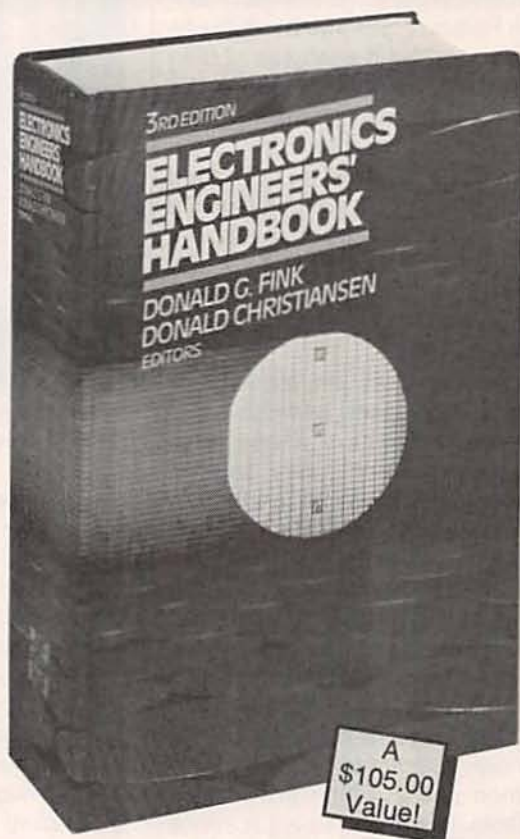
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WHAT'S NEWS

A review of the latest happenings in electronics.

World's smallest hard-disk drive

Hewlett-Packard Company introduced the world's smallest hard-disk drive in June. Its 1.3-inch Kittyhawk Personal Storage Module can store up to 21.4 megabytes of data (formatted). The introduction of the matchbox-size drive by HP, not known for its expertise in that technology, seems to assure continued life for rotating disk memories. HP's development makes it highly unlikely that disk drives will be driven out of the market by semiconductor memory modules in the foreseeable future.

The drive was developed for palmtop, pen-based and sub notebook-size computers whose manufacturers are continually seeking component size, weight, and power reductions. The disk drive package measures 0.4 inch \times 2 inches \times 1.44 inches, and it weighs about one ounce. The platters rotate at 5400 rpm, and average seek time is less than 18 milliseconds.

HP says the drive—which will be priced at \$250 in high volume—is far more resistant to shock than the 1.8-inch and 2.4-inch drives now available. In addition to applications in existing products, HP predicts that Kittyhawk will find a place in such future products as printers, fax machines, medical equipment, communications gear, and digital imagers. Company officials even see a place for it in consumer video-game cartridges and as data storage media for cellular telephones and digital copiers.

The sub-mini disk drive was developed in cooperation with several companies including AT&T Microelectronics (Berkeley Heights, NJ) and Citizen Watch Co., Ltd., of Japan. Working with AT&T Microelectronics, HP was able to reduce the 20 to 30 IC's typical of most of today's 1.8- and 2.5-inch drives to just seven.

According to HP, the cost of semiconductor memory equivalent



HEWLETT-PACKARD'S 1.3-INCH DRIVE shown here actual size.

to the capacity of the Kittyhawk is about five times the price of the drive—and that is before the learning curve price reductions have taken effect. Twenty megabytes of semiconductor memory now has an OEM price of about \$1000 (\$50 per Mbyte); by comparison, at Kittyhawk's present OEM prices, the cost of memory is \$12 per Mbyte.

The drive module stores data like a standard Winchester drive, and it connects with a Personal Computer Memory Card International Association (PCMCIA) or standard AT interface. The 21.4-Mbyte drive has two platters and three heads. The modules contain a sensor that detects impact and causes them to shift to a self-protective mode to preserve data.

Advanced MRI technique

Advanced magnetic resonance imaging (MRI) now permits the measurement of the flexibility of blood vessels, a key predictor of heart disease. Scientists at GE Research and Development Center (Schenectady, NY), working closely with researchers from the Imperial College of Science, Technology, and Medicine (London, U.K.), have developed a non-invasive technique

based on MRI technology that simultaneously determines blood-flow velocities at different points along a blood vessel.

The measurements obtained can then be used to calculate the speed at which a pressure pulse travels away from the heart and down a vessel after the heart contracts. Those wave propagation speeds permit the computation of vessel-wall flexibility, a factor in the determination of the presence of diseases such as atherosclerosis.

GE's MRI technique is expected to be able to follow changes in blood-vessel flexibility as people age or as diseases develop. Because it relies on MRI angiography, there is no need to insert a pressure transducer on the end of a catheter that must be snaked through the arteries, a potentially dangerous invasive process.



A BLOOD-FLOW VELOCITY measurement made with an MRI imaging technique is studied by GE scientists Charles Dumoulin and Robert Darrow.

In MRI inspection of internal organs and tissues is done with a combination of powerful magnetic field, radio-frequency emissions and computer computation. A superconducting magnet within the barrel-shaped MRI equipment can produce a 1.5 Tesla field within its one-meter bore where the patient is located.

The patient within the bore is
continued on page 21

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AM or FM capability



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- +12VDC @ 1 Amp
- -12VDC @ 1 Amp
- +5VDC @ 1 Amp
- 30VAC Center tapped @ 15VAC at 1 Amp

Analog - Section

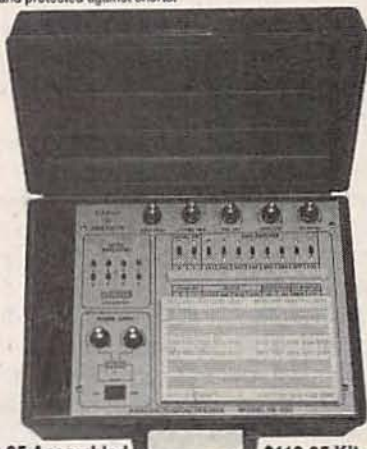
- Function Generator Sine, Triangular, Square wave forms
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VIDEO NEWS

What's new in the fast-changing video industry.

DAVID LACHENBRUCH

● **Flat panels for HDTV.** There's still no substitute for the CRT when it comes to large-screen resolution, but that doesn't mean that developers around the world aren't still trying to find that elusive giant picture on the wall for HDTV. Two promising developments recently surfaced in Japan.

Flat plasma display. The prestigious Japan Broadcasting Corporation (NHK), Japan's public-television broadcaster, recently held an impressive progress-report demonstration of a thin glass sandwich HDTV plasma display panel that it says could be commercialized as soon as 1997. The system is being developed as a joint effort with Matsushita (Panasonic), NEC, Oki Electric, and Dai Nippon Printing. Texas Instruments has a contract to develop semiconductors for the system. NHK is now demonstrating a working model HDTV display panel with a 16:9 widescreen aspect ratio. The model is three inches thick and weighs less than 18 pounds.

NHK concedes that there's more work to do, but thinks the answers to the remaining problems are in sight. The screen has 1344 display cells horizontally and 800 vertically, for a resolution of 1,075,000 pixels, but it still falls short of the necessary brightness and life for a consumer display. The final version will have smaller cell size. NHK is promising to show a 55-inch working prototype next year.

Ferroelectric LCD. Working with a technology that others have rejected, Canon of Japan believes that it has found the solution to the need for giant thin color screens with no flicker and with a wide display angle for digital HDTV. While others work with the frustratingly difficult problems of active matrix LCD's, Canon has chosen to gamble on ferroelectric LCD (FELCD), a technology known since 1974. Canon is already planning to build several plants to mass-produce consumer HDTV panels.

Canon scientists believe that there is no theoretical limit to the size of FELCD screens. FELCD material differs from active matrix LCD transistors in that it's bi-stable—it can only be switched off or on. Once switched on, an FELCD molecule remains on until turned off, and vice versa. That would make it ideally suited to digital TV transmission if the problem of color rendition and gray scale could be solved. Canon says it has done this by calling on its work in black-and-white and color printers.

Canon says that it will start making computer monitors using the FELCD material next year, moving to color in 1994. The company already has displayed a still color screen with nearly HDTV resolution—four times better than computer VGA color CRT monitors. The planned 15-inch computer display has a resolution of 1280 x 1024 pixels, and the proposed 16:9 HDTV display is scheduled to have 1920 pixels in each of 1152 horizontal lines.

● **Widescreen sets in the U.S.**

Thomson Consumer Electronics continues to dole out information about its widescreen 16:9 aspect ratio TV sets just a little at a time. The first sets, due out late this year under the RCA and ProScan labels, will have 34-inch picture tubes made in Thomson's tube plant in Italy. The company is shooting for a price of \$4000–\$5000 for the first sets, less than the price tags for Thomson widescreen sets that are already available in Europe. However, Thomson plans to start manufacturing widescreen tubes in the U.S. in 1994, and its goal for that time is a 34-inch widescreen set at about the price of today's 35-inch standard aspect ratio (4:3) sets, which now start at less than \$2000. In addition to the 34-inch direct-view set, Thomson plans to offer widescreen projection sets in larger sizes beginning next year.

● **Hughes-JVC projection pact.** Hughes Aircraft, which has manufactured multi-million dollar video projectors for the Pentagon, is gearing up for civilian production. Hughes has been seeking a consumer-electronics partner to develop a consumer version of its liquid-crystal lightvalve (LCLV) projection system. It finally found that partner in Japan's JVC. Hughes-JVC Technology Corp., 60% owned by Hughes and 40% by JVC, will develop consumer and commercial versions of LCLV projectors. The system combines a high-resolution CRT for image generation with separate LCD panels and an external light source to provide a very bright picture with high resolution. It is a candidate for future giant-screen HDTV projection sets.

This fall, Hughes-JVC will market professional models already developed by Hughes, priced from \$8000 to more than a million dollars; consumer versions will cost from \$2000 to \$7000. JVC will manufacture consumer projectors and key components in Japan, and will distribute LCLV projectors worldwide through its sales network. Hughes said that HDTV resolution has been achieved with LCLV projectors, and 35mm-film resolution is the next target it will be shooting for.

● **8mm video decks here.** The success of the 8mm video format in camcorders must be followed by decks for showing and editing home videos. Sony was the only source 8mm decks, but two others have appeared. The compact decks with hi-fi stereo sound, which carry the RCA and Samsung brand names, are expected to sell for about \$499. They're both made by Korea's Samsung. In the future is a dual-well 8mm/VHS deck to transfer 8mm videos to VHS cassettes and for editing home videos. Go-Video has already shown a prototype model, due next year. **R-E**

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DOUBLE AND HIGH DENSITY

Is there any truth to the rumor I've heard that the only difference between 3½-inch double- and high-density disks is the extra hole in the corner of the plastic package? Just about everybody I know buys the double-density variety and then punches a hole in the plastic case to turn the disks into high-density ones. I've done it myself and can't see any difference between these disks and the ones with "HD" stamped on them.—F. Foeg, Frish, CA

This is one of those times when I have to say that your guess is as good as mine. I've done the same thing to double-density disks and have never had a problem either. I know people who swear they're different but I've never had a practical example of it.

I remember reading a long description of the chemical difference in the media but it seems to have made little impression on me since all I remember is that the article was long and technical—the details have disappeared completely from my mind.

From a practical point of view, I've had more trouble with "real" high-density 3½-inch disks than with the ones I've punched or drilled into existence. This is just as true for name-brand disks as it is for the generic (and cheaper) variety.

Just about the only piece of hard information I have for you is the fact that some older high-density 3½-inch disk drives don't have the LED and sensor setup to look for the extra hole. Those drives are usually found on the older PS2 computers from IBM.

I know that this letter—and the answer—will spark a host of mail from people who are into disk media chemistry. That may be a good thing because this rumor about 3½-inch disks has been floating around since the high-density variety first



FIG.1—A SECOND HOLE INDICATES that a disk is high-density.

came on the market. If people out there really have the answer, and the credentials to back it up, I look forward to hearing from them and I'll be sure to pass the "real" information along.

THE APPLE FAMILY

I'm thinking about buying a used Apple IIe for my son since there are some good buys around, but I'm not sure about the difference between these computers and the other members of the Apple family. Also, I'd like to know if I can use my color TV for a monitor or will everything be unreadable?—S. Gibbs, Redondo Beach, CA

Apple isn't what Apple once was. It's sad but true that while Apple made a lot of money with the Apple II series by saturation selling in the educational market (mostly grade schools), they seemed to have shifted their corporate focus to the Macintosh. While there are some similarities between all the members of the Apple II family, they are a completely different breed from the Macintosh.

Once upon a time, Apple II computers were targeted mostly at the schools and the Macintoshes were aimed at the graphic arts, but this seems to have changed. Apple has reduced the amount of corporate resources devoted to the Apple II and has been touting the Macintosh

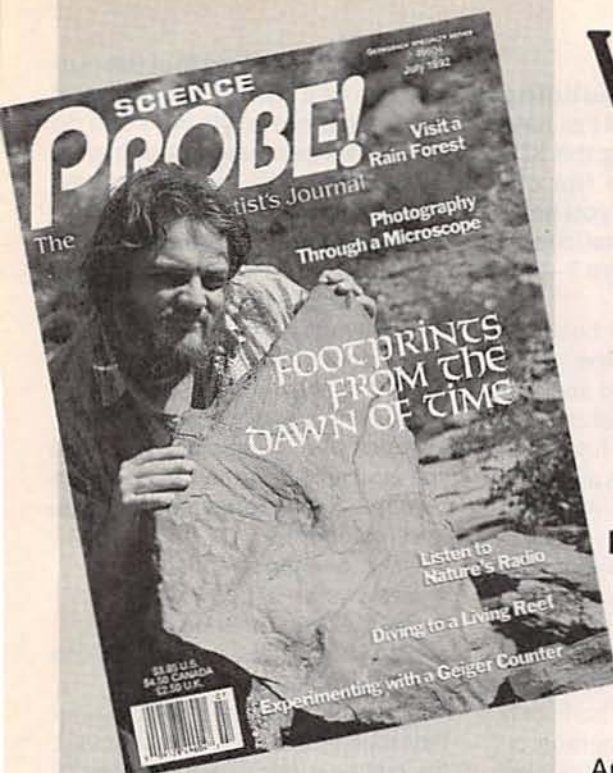
as an alternative to IBM compatibles in the business world.

To answer your first question more specifically, there's a big difference between the Apple IIe and the Apple IIgs. The "e" stands for "enhanced" to highlight the difference between it and the older Apple II+ it replaced. The "gs" stands for "graphics/sound" and is a way of emphasizing the difference between it and the older Apple IIe you're thinking of buying.

While the Apple IIgs can run a lot of the software written for the Apple IIe, the reverse isn't true at all. The hardware is very different and so are the capabilities of the two machines. If you have some specific software in mind, a used Apple IIe can be a good buy but, if you're sold on the idea of having one of the Apple II series of computers, spring for the extra bucks and hunt up a used Apple IIgs.

It may interest you to know that friends of mine who teach the computer courses in grade schools tell me that it's getting harder and harder to find new software for the Apple II computers—even for the top of the line Apple IIgs. You should check with people in the schools near you and find out for yourself since even the world's greatest computer isn't worth anything if the larger software companies are withdrawing their support. Remember these people are market driven and they may know something we don't. It's not always wise to rely completely on the advice of the salesmen in the Apple stores. They make their money selling computers, not writing the software that will run on them.

As far as using a TV is concerned, it might be OK for games but if you want to do anything more serious, you'll find it entirely unsuitable. You might save some money by not buying a real monitor but it's a safe bet that all those savings will go into eye exams and new glasses.



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VIDEO IC's

I'm interested in building some video devices but I'm having a hard time locating the IC's that are best suited to the circuits I have in mind. Do you have any supplier that specializes in carrying these chips?—M. Brown, London, UK

I sympathize with you because I've frequently run into the same problem myself. It's a hard and fast rule that the more specialized the IC, the harder it is to find—especially in single quantities and without having to meet any minimum order.

The best place to begin your hunt for these parts is with the very people who make them—the IC manufacturers. If you're lucky, you'll be able to get some freebie "engineering samples" from them. This is only true if you get the right person on the phone and you identify yourself in such a way as to let them think it's worth their while to send you the stuff you want.

Remember, they're in the business of making chips for sale and if they believe that a small sample now can lead to a large order later on, you'll get what you need.

A second line of approach is to find out who their distributors are in your area and trying the same line with them. Your chances aren't as good with a distributor, but you never know. The salesperson might let you pay for a few parts (and shipping), without having to meet their minimum order quantity.

The last alternative—although you might not like it—is to fill out the minimum order by stocking up on parts you'll be able to use later on. This means stuff that may be needed for something else you have in mind but don't intend to actually start for a while.

Getting anything in single quantities is the hardest thing an experimenter can do. There are, however, suppliers who stock a wide variety of components and low or no minimum orders.

SPEEDING CURSOR

I recently upgraded from my old XT computer and got a much faster 386SX that runs at 20 MHz. Everything runs much

faster now, but I find that the cursor speed hasn't changed much. Is there anything I can do about this because speeding up the cursor will make my new computer seem to run even faster.—B. Geoff, Fischer, IN

Although your expectations haven't quite been met, I guarantee that making such a major change in your computer horsepower has also made a change in the speed of your cursor. The reason you haven't seen as much of a change as you would like is simply that the speed of the cursor is dependent on three separate factors:

- Basic computer speed
 - Basic video speed
 - Basic keyboard speed
- and all you've done is changed one of these factors.

Now that you have a computer that runs at a furious rate of speed, the cursor speed is being limited by the speed of either your video adapter or your keyboard—which ever is less.

Remember that when the keyboard sends an instruction to move the cursor, the computer tells the video adapter to do it. The computer does its part of the job pretty quickly, but the other two components operate much more slowly—particularly the keyboard.

However, it's a good thing that the keyboard is the slowest component because the keyboard repeat rate can be changed with software. (There isn't much you can do about the speed of your video adapter, short of spending a lot of money for fast video card.)

There are several public domain programs (and some commercial ones as well) for changing the keyboard repeat rate, but all of them have one slight disadvantage: they steal a certain amount, however little, of valuable memory. That can be a really big problem.

The answer is a small public domain program called FAST.COM that cuts the keyboard repeat delay to a bare minimum. I've been using it for several years without any trouble, and I run it automatically every time I turn on my computer. I've put it on the RE-BBS (516-293-2283, 1200/2400, 8N1) so you can download it and see if it works. **R-E**

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SOLID-STATE RELAY UPDATE

Regarding the article, "Solid-State Relay" (**Radio-Electronics**, May 1992), a very important feature is the zero-current switch-off characteristic inherent in the triac.

The interruption of the circuit at the instant the current is zero avoids voltage spikes that could be produced by the stored energy (E) in the distributed inductance of the power line and leakage inductance of the mains (line) transformer (L) if the current is suddenly interrupted at a non-zero value, as occurs with mechanical contact breakers. As we know, $E = \frac{1}{2} Li^2$. At the instant the current crosses zero, the stored energy is also zero.

These voltage transients, which are caused by switching heavy currents, are often the reason for failure of electronic equipment connected to the same line. The solid-state relay prevents such damage.

LEO BATISTA

*Professor of Electric Automation
University of Sao Paulo
Sao Paulo, Brazil*

A REAL HUM-DINGER

I appreciated the response to the 60-hertz hum question that appeared in *Ask R-E* in the June issue of **Radio-Electronics**. I had the same problem with my speaker system. I took your advice, and my problems were solved. Thanks!

JEFF FRUSCELLA

Kirtland, OH

ANOTHER HUM STOPPER

I enjoy reading *Ask R-E* each month. The 60-hertz hum problem described in the June issue could be caused by a ground loop. When components of a stereo system that are connected by patch cords receive their power from different 120-volt receptacles, a ground loop can be formed by a small amount of alternating current flowing in the shield of a shielded patch cord. That

current flow is caused by a small potential difference in the neutral conductor wiring in a building's 120-volt circuits.

There is help for this type of hum problem. Radio Shack has a stereo ground-loop isolator, No. 270-054, which is a patch cord with two audio isolation transformers included. Those transformers break the ground-loop circuit, thereby stopping the current flow that causes the hum.

The ground loop isolator is listed on page 60 of Radio Shack's 1992 catalog in the automotive section. It can be used in line-level circuits of any audio equipment. I have successfully used this device in audio component hookups.

JACK P. SONNEMAN

Fayetteville, OH

ROSICRUCIANS, ALIVE AND WELL

I am writing in response to the item in *Ask R-E* (**Radio-Electronics**, June 1992) about FM antennas that use household wiring. Perhaps they have disappeared, which is fine by me, but Rosicrucians (AMORC) haven't. I subscribe to **Radio-Electronics** and have done so for quite some time. I am also a member of the Rosicrucian Order, AMORC, and have been a member for just as long, if not longer.

Until the time comes when I no longer receive the valued information that I do from both **Radio-Electronics** and AMORC, I will be affiliated with both. Your questions are welcome.

CHARLES R. BAILEY

2123 Grand St. N.E.

Minneapolis, MN 55418

TURN-SIGNAL AMPLIFIER

Regarding the request from W. Baker in *Ask R-E* (**Radio-Electronics**, April 1992) for a turn-signal amplifier, I have designed a simple, low-cost device that is intended to solve that problem.

The product requires no wiring in any vehicle, be it a bus, truck, or automobile, and operates with a time delay. A 2800-Hz beep is generated after a fixed-time delay and is repeated at this same delay for as long as the turn-signal switch is on. For example, when the turn-signal switch is selected to indicate a turn, 45 seconds later if the selector switch is still on, a 2800-Hz beep is emitted. The beep is repeated 45 seconds later, and will keep occurring at 45-second intervals for as long as the turn signal remains on. The time delay can be designed for any value. Most customers will likely prefer a 60-second delay, but there will be 30-second and 45-second delays available, or any other that the market might desire. Two volumes of sound are selectable by a slide switch.

The product is simply installed in any vehicle in less than two minutes, and will be available from my company for less than \$20 starting in December 1992.

ALBERT P. GREGORY

*A.G. Technologies
27211 El Pico Lane
Sun City, CA 92486*

TURN-SIGNAL AMPLIFIER

In April's *Ask R-E*, your response to W. Baker's request for a turn-signal amplifier—to purchase and add a chime—is expensive and gives an undesirable indication. The "chime" is not something most people want to hear every time their turn-signal lamps flash. Here are two other practical solutions.

Wagner Lighting now markets a fully solid-state, two-terminal automotive flasher. One specification that has been an issue since the project started is the audio output, since there is no bimetallic blade or relay to make the sound. An audio transducer was added to generate the familiar click that drivers associate with flashers.

Because a solid-state flasher re-

The DMM our customers designed.



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For more information on these new DMMs call (outside CA) 1-800-854-2708 or (inside CA) 1-800-227-9781. Beckman Industrial Corporation, 3883 Ruffin Rd., San Diego, CA 92123-1898.



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CIRCLE 98 ON FREE INFORMATION CARD

quires an external audio transducer, Wagner's new flasher has incorporated an attention timer that beeps for eight flashes after a delay of about three minutes. Beeps alert the driver that his turn signal flasher has been left on. Because this flasher has two terminals, it can replace any existing automotive turn-signal flasher.

Another way to get the driver's attention is by making the click louder. A capacitor in series with a speaker across the load and battery terminal of the flasher will create a click at every lamp on/off transition. When the flasher turns the lamps on, a voltage spike will dissipate through the speaker and create a "click." The same thing will happen when the flasher turns the lamps off. The larger the capacitor and speaker, the louder the click. A value of 47 microfarads works well with a 1½-inch speaker.

I've enjoyed **Radio-Electronics** for years and use it to keep my design and practical skills up to date. Keep up the good work.

TIMOTHY W. BROOKS
*Senior Design Engineer
Wagner Lighting
Sevierville, TN*

TV AND X RAYS

I'm writing in regard to the item about TV and X-rays that appeared in *Video News* (**Radio-Electronics**, June 1992). I'm aware that the changes in modern-day TV sets—including solid-state circuitry and redesigned shielded CRT's—probably make them safer to be near than ever.

However, I'm also aware that many manufacturers design their products very close to the product safety guidelines as a matter of cost containment. Many individuals, including office workers, children who play video games, and students may spend considerable time in close proximity to CRT's—either in TV sets or computer terminals. That doesn't even take into account the increasing time that many children spend watching TV.

In the auto industry, we are buying

safety in the form of redesigned car bodies, safety restraints, air bags, safety glass, anti-lock brakes, and making sure that we crash-proof this and that.

I agree that we must not hamper the electronics industry, but at the same time, I believe that we must do more to safeguard people against radiation, which is both invisible and harmful.

DONALD HANG
North Canton, OH

SNOOPER STOPPER SUGGESTION

The article "The Snooper Stopper" (**Radio-Electronics**, April 1992) was very interesting. But if a person is only interested in protecting his cable box from the bullet and ID signal, then why not use an FM-trap, which is available from Radio Shack (Cat. No. 15-577) for \$3.69? That would save about \$20 compared to the cost of your project, and it needs no adjusting.

MATT STANTON
Shrewsbury, MA

R-E



If you're in the market for great test and measurement gear, here's some food for thought: Tek makes a bunch of it. All with the same enduring quality that made our scopes famous. We even have catalogs so you can order these

WHAT'S NEWS

continued from page 6

probed with high-frequency radio signals. Those signals, under the influence of the magnetic field, "excite" the nuclei of the hydrogen atoms concentrated in blood and body organs, causing them to resonate. Those resonance signals are transmitted to a computer which converts them into digital data. Computer software reconstructs the data into a picture of the object being imaged on the computer's monitor.

A flow encoding procedure that distinguishes between resonance signals emitted by moving hydrogen atoms in the bloodstream and those in the stationary organs and structures sets GE's MRI angiography technique apart. Signals emitted by the motionless hydrogen atoms are suppressed while those from the moving atoms are highlighted. The technique can measure and calculate the flexibility of the aorta and

various major arteries as well as most blood vessels.

To explore the clinical relevance of the quantitative measurement technique, GE and Imperial College researchers will examine how various agents such as nicotine and nitroglycerine alter the flow dynamics of blood within a vessel.

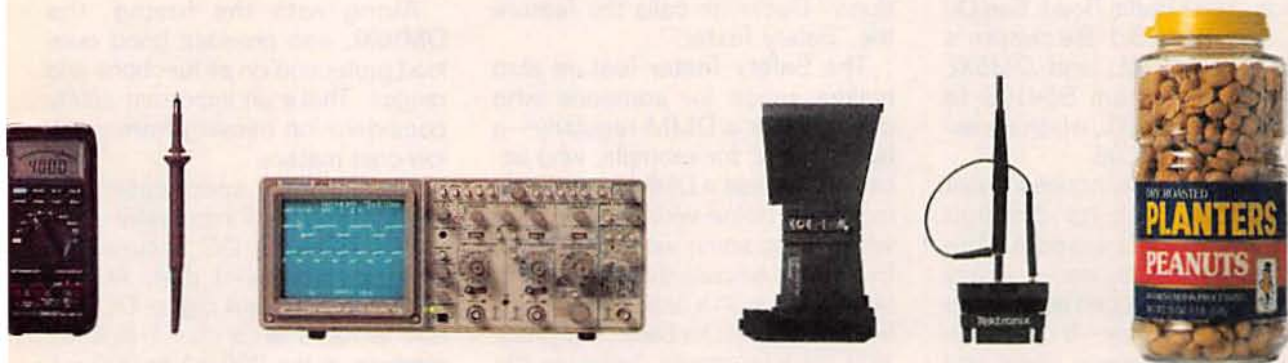
Military technology for law enforcement

In an effort to shed its type casting as an exclusive defense contractor, the Westinghouse Electronics Systems Group (Baltimore, MD) has unveiled a shopping list of law-enforcement related products that it has developed. They are intended for the war on drugs and are expected to make law enforcement safer and more effective. Among the products and systems are:

- A vehicle equipped with advanced electronics providing an automatic communications link to criminal and motor-vehicle data banks, and still-frame video capture and transmission.

- A multi-sensor surveillance aircraft equipped with advanced sensors, communications, and navigation systems for aerial surveillance.
- A handheld instrument that detects trace amounts of illicit drugs or explosives and displays its findings. The instrument does a chemical analysis of a card that is passed over a suspect container.
- Software for computer-assisted report entry and law enforcement management.

By down-linking the multi-sensor aircraft's infrared and radar image to a ground base, the aircraft can also serve as an airborne command center to direct and coordinate ground activities. The vehicle-integrated payload-elevated reconnaissance (VIPER) system integrates radar, electro-optical, communications, and computer technologies into a mobile target-detection and reporting system intended for border surveillance. These are commercial versions of military systems that the company has developed over the past five decades. **R-E**



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Beckman Industrial DM10XL Digital Multimeter

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Multimeter buyers on a budget have never had it so easy—nor have they ever had it so hard. It used to be difficult to find a low-cost DMM that was full-featured and built with an eye toward safety. These days, it's easier than ever to find such meters, but it's getting more difficult to choose from among them. The latest crop of low-cost high-quality DMM's to hit the market are from Beckman Industrial (Instrumentation Products Division, 3883 Ruffin Road, San Diego, CA 92123.) Beckman's DM15XL, DM10XL, and DM5XL range in price from \$34.95 to \$59.95. The DM10XL, which we examined, costs \$44.95.

The first thing we noticed about the DM10XL was its 3½-digit (2000-count) LCD readout. The large (0.7-inch) digits are very easy to read. We also noticed the meter's non-traditional color—a charcoal-gray cabinet with green labels and accents. Although we certainly wouldn't buy a DMM because of its color, the people at Beckman say they did a lot of market research that led them to choose the green shade.

The dimensions of the DM10XL are roughly 6×3×1¼ inches. The meter's face is dominated by a large rotary function-selector knob roughly in the center. The LCD is above the knob, and a row of 4 input jacks is below it. Along the left front edge is what we regard as the unit's

most innovative feature: A row of LED's give a rough idea of the voltage level at the probes even if the meter's battery is dead! It's a good feature because many DMM users are careless about replacing the battery when the low-battery annunciator indicates that it's time to do just that. (We assume that's because they don't know that a low battery can reduce a meter's accuracy tremendously, which could result in potentially dangerous situations.) Beckman calls the feature the "Safety Tester."

The Safety Tester feature also makes sense for someone who doesn't use a DMM regularly—a home-owner, for example, who occasionally uses a DMM when working on a home-wiring project or when doing some work on his car. Even when he pulls the meter out of his tool box with a dead battery, he'll be able to use it for basic, low-precision measurements, because the Safety Tester is powered by the voltage being measured, not by the DMM's battery.

Seven LED's indicate the voltage being measured: One yellow LED is used to indicate a negative voltage (or, in combination with another LED, an AC voltage.) A row of six red LED's indicates the voltage level; the levels indicated are 6, 12, 24, 50, 110, and 230 volts.

The DMM section of the meter measures AC volts in two ranges; (200 and 740 volts), DC voltage in

five ranges (200 mV, 2, 20, 200, and 1000 volts); and resistance in six ranges (200, 2K, 20K, 200K, 2000K, and 20 megohms). A diode-test/continuity feature is also available.

The DM10XL can measure DC current over five ranges (200 µA, 2 mA, 20 mA, 200 mA, and 10 A). One test lead must be moved for current measurement to one of two current jacks—one jack handles current levels up to 200 milliamps; the second handles 10 amperes. Beckman has included two important safety features here. First, both current inputs are fused to protect both the user and the meter. Second, the meter will sound a warning tone if you have the test leads set up for current measurement while the function switch is in a voltage-measurement range. That's important because trying to measure a voltage with the test leads set for current could cause an excessively high current to flow.

Along with the fusing, the DM10XL also provides good overload protection on all functions and ranges. That's an important safety consideration missing from many low-cost meters.

The accuracy specifications of the DM10XL are impressive for a low-cost meter. DC accuracy is rated at ±0.7%+1 digit; AC accuracy at ±1%+4 digits. DC current is rated at ±1%+1 digit for readings in the 200-µA to 200-mA ranges, and at ±2%+3 digits for readings in the 10-amp range.

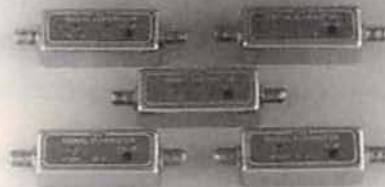
The lowest-cost meter in the series, the DM5XL does not offer the Safety Tester feature and, in general, provides lower accuracy and reduced measurement capabilities. The DM15XL also lacks the Safety Tester, but adds AC current measurement and a logic-probe mode.

We were impressed by the convenience and safety features built into the \$44.95 DM10XL. We recommend it highly. **R-E**



ELEVEN-PIECE RACHET TOOL KIT

Includes reversible ratchet handle, extension bar, six bits, two precision screwdrivers, and a cutter. Comes in fitted case. Get one for your shop, another for your car, another for your tool kit. To order send \$11.75 USA shipping only. **ELECTRONIC TECHNOLOGY TODAY INC., PO Box 240, Massapequa Park, NY 11762-0240.**



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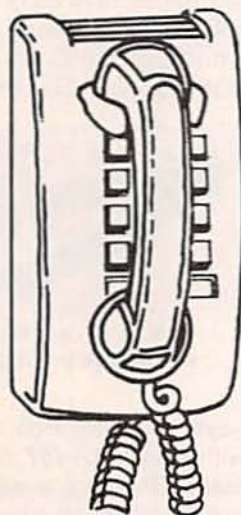
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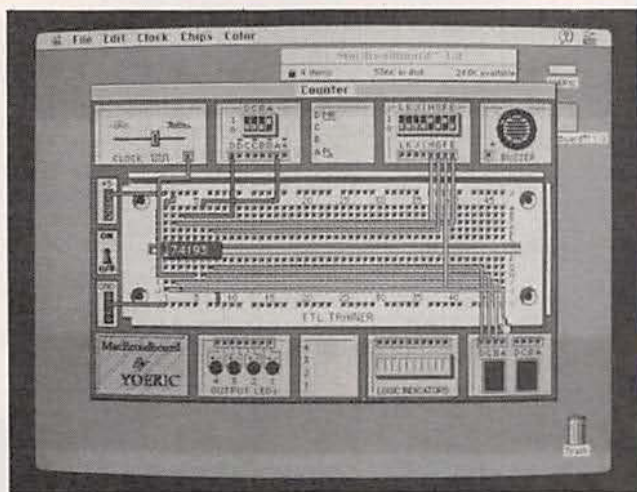
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MACINTOSH DIGITAL-CIRCUITS TRAINER.

Owners and users of a Macintosh computer (512ke with System 4.1 or greater) who want to learn more about digital electronics can do so with Yoeric Software's *MacBreadboard 1.0*. Intended for hobbyists and students, the transistor-transistor logic (TTL) trainer was designed to act like the hardware simulators used in many digital circuit courses. Unlike those simulators which are based on a schematic approach, *MacBreadboard* provides a computer representation of a real-world object; the student manipulates IC chips and conductors, not individual gates.

Students select a TTL device by number (i.e. 7400) from a menu, place it on the representation of a PC board on the MAC computer's screen, and "draw" conductors to connect the power supply, resistors, capacitors, switches and other components just as they would in putting together a lab breadboard. According to Yoeric, the program permits students to simulate their laboratory



CIRCLE 16 ON FREE INFORMATION CARD

assignments before actually doing them. The program is said to be able to supplement or be an alternative to a formal course on digital circuits.

MacBreadboard permits the student to select from among over 30 two-state devices, breadboard, power supply, wires, LED's, buzzer, seven-segment displays, switches, and a logic probe. Timing diagrams of circuits that have been simulated can be displayed and printed out. A "snapshot" of the breadboard can also be printed. Integrated circuit sche-

matics can be displayed by double-clicking on the symbol of a device. The program runs in color, gray scale, and black-and-white. In the color mode, the traces can be colored by length or node, or the user can specify the color desired. A 50-page manual with diagrams of sample circuits that can be simulated is included.

MacBreadboard 1.0 costs \$59.95; educational discounts are available.—**Yoeric Software**, 600 South Churton #24, Hillsborough, NC 27278; Phone: 919-644-1620.

PACKET MODEM/TERMINAL MODE CONTROLLER A

Commodore 64/128 computer and a handheld VHF or HF single-sideband transceiver with the MFJ-1271 are your tickets for admission to packet communication. MFJ's modem/terminal mode controller plugs into your Commodore's rear cassette port. It works both



CIRCLE 17 ON FREE INFORMATION CARD

VHF packet at 1200 baud and HF packet at 300 baud. A data carrier detected circuit and adjustable threshold control reduces noise

susceptibility and increases the chances of making QSO connections—especially on HF bands.

A DCD circuit with a LED indicates when you are receiving signals properly. The device also features remote packet operation, mailbox-like message forwarding, and Net/ROM emulation. It uses MFJ En-

terprises's Digicom/64 public software (MFJ-1293).

The MFJ-1271 costs \$49.95.—**MFJ Enterprises, Inc.**, P.O. Box 494, Mississippi State, MS 39762; Phone: 601-323-5869 (for orders: 1-800-647-1800); Fax: 601-323-6551.

GENERAL-PURPOSE CUTTER.

Cable TV and computer network installers, and technicians working with different kinds of coaxial cable and wire need sharp, general purpose cutters. GC Electronics



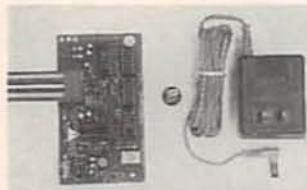
CIRCLE 18 ON FREE INFORMATION CARD

says it meets this need with its No.12-457 5-inch cutter. The tool is said to cut through all sizes of coaxial cable cleanly and crisply, without crushing the cable. It is also capable of cutting other kinds of wire used in electrical and electronic work.

The No. 12-457 cutter sells for \$3.50.—**GC Electronics**, 1801 Morgan Street, Rockford, IL 61102.

AUDIO REFERENCE GENERATORS.

The ARG-440 and ARG-1000 audio reference generators from Tobin Cinema Systems are said to generate pure, accurate 440-Hz (A4 to musicians) and 1000-Hz tones. The generators also provide precision "pink" and



CIRCLE 19 ON FREE INFORMATION CARD

"white" noise for audio tests.

A 440-Hz frequency standard is used in tuning musical instruments and even whole orchestras. The frequency can also verify that tape speed is correct and that 0 VU reference levels are set. A frequency of 1000 Hz is the traditional reference level. Both models of audio reference generator have stated accuracies of 10 parts per million, 3 ppm (0.0003%) typical.

Pink noise applied to tape heads after the reference tone permit playback

equalization to be precisely set when used with a real-time analyzer. That noise can also be used for room equalization. Moreover, pink and white noise can be mixed to simulate the sound of rain, a waterfall, surf, or various hissing noises.

The outputs of the audio reference generators are electronically balanced at 600 ohms and deliver 0 dBm. They can also be unterminated at +6 dBu, unbalanced at 0 dBu, or loaded for a lower signal level. Each generator set includes a calibrated circuit board, color-coded detachable 16-wire cable, a wall-outlet AC to DC converter, and a mating DC power plug. Both can be operated from any +12- to +35-volt DC source.

ARG-440 and ARG-1000 audio reference

generators are priced at \$150.—**Tobin Cinema Systems**, 3227 49th Avenue SW, Seattle, WA 98116; Phone: 206-932-7280.

ALLIGATOR CLIPS. A family of five alligator clips from *ITT Pomona* permits the safe electrical testing of components and systems carrying up to 250 volts. The clips are available in a range of sizes: large heavy duty, large, medium, miniature, and disposable. All alligator clips are coated with durable plastic insulation to prevent shock hazard, shorting, or grounding to conductive surfaces.

Tinned copper-alloy jaws firmly grasp wires or leads and receptacles with connectors accept 2- to 4-mm (0.087- to 0.157-inch) lead wires. The miniature and disposable clips are intended for tests on densely pop-

ulated circuit boards in restricted locations. They are also useful in such medical applications as electrocardiogram testing. The larger clips are suitable for testing for high-current withstand capability and electrostatic-control products.



CIRCLE 20 ON FREE INFORMATION CARD

The large, heavy-duty *Model 5785* grips objects up to 9.5-mm (0.37 inch) in diameter. It has an overall length of 81 mm (3.19-inch), and it accepts a sheathed banana plug. It will protect against 250 volts. The large *Model 5786* clip grips objects up

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to 10 mm (0.39 inch) in diameter. It includes a screw connection for lead wires up to 18 AWG (2.4 mm). Its overall length is 80.5 mm (3.17 inches).

The Model 5787, 56-mm (2.20-inches) long medium clip, connects to a standard 4-mm banana jack. The Model 5788 miniature clip has a miniature banana jack and an overall length of 40 mm (1.57 inches). The disposable Model 5791 clip, with an overall length of 53 mm (2.09 inches), has a button fix/release for lead retention and a standard banana jack.

The alligator clips are priced from \$.98 to \$3.45 each.—**ITT Pomona Electronics**, Customer Service, 1500 East Ninth Street, P.O. Box 2767, Pomona, CA 91769; Phone: 714-469-2900; Fax: 714-629-3317.

INTEGRATED SURFACE MOUNT WORKSTATION.

Manufacturers who perform paste and place surface-mount component assembly in small volume can improve their yields and their productivity with the SMT-6000 pick/place/dispense system from **OK Industries**.

The mechanically assisted, solder-paste dispensing and component placement system is designed to achieve placement rates of up to 600 components per hour. It integrates a solder-paste dispenser and vacuum pick-up head onto a single arm assembly. That arm can be moved in the X-Y-Z-0 axes while the operator's hand is stabilized on a movable hand rest.

Needle positioning for paste dispensing, is said to be precise and repeatable, reducing placement location error by as much as 67%. According to OK In-



CIRCLE 21 ON FREE INFORMATION CARD

dustries, the mechanical assistance of arm assembly provides a three-fold increase in production over manual pick-and-place methods. For prototyping and batch production, a board can be pasted and populated in one workstation while secured in the adjustable, locking PC board holder. Movement is minimized because the board remains fixed during both the pasting and populating operations.

The SMT-6000 is sold complete with a 45-compartment carousel, 12-inch and 15-inch PC board holders, a self-contained vacuum source for pick-and-place operations, time/pressure controls for dispensing, a hand rest, and a pick/place nozzle kit. Optional accessories such as stick and reel component feeders, a light/magnifier, interchangeable spare carousels, and a feeder-mounting bracket are also available.

The SMT-6000 SMT workstation sells for \$3750.—**OK Industries, Inc.**, 4 Executive Plaza, Yonkers, NY 10701; Phone: 914-969-6800; Fax: 914-969-6650.

TRANSDUCER POWER SUPPLY.

The Model 4130 encapsulated power supply from **Calex** offers adjustable voltage output for powering transducers, strain gages, and many kinds of laboratory equipment. The power supply provides 4 to 15 volts DC at up to 1590 milliamperes, enough power for three

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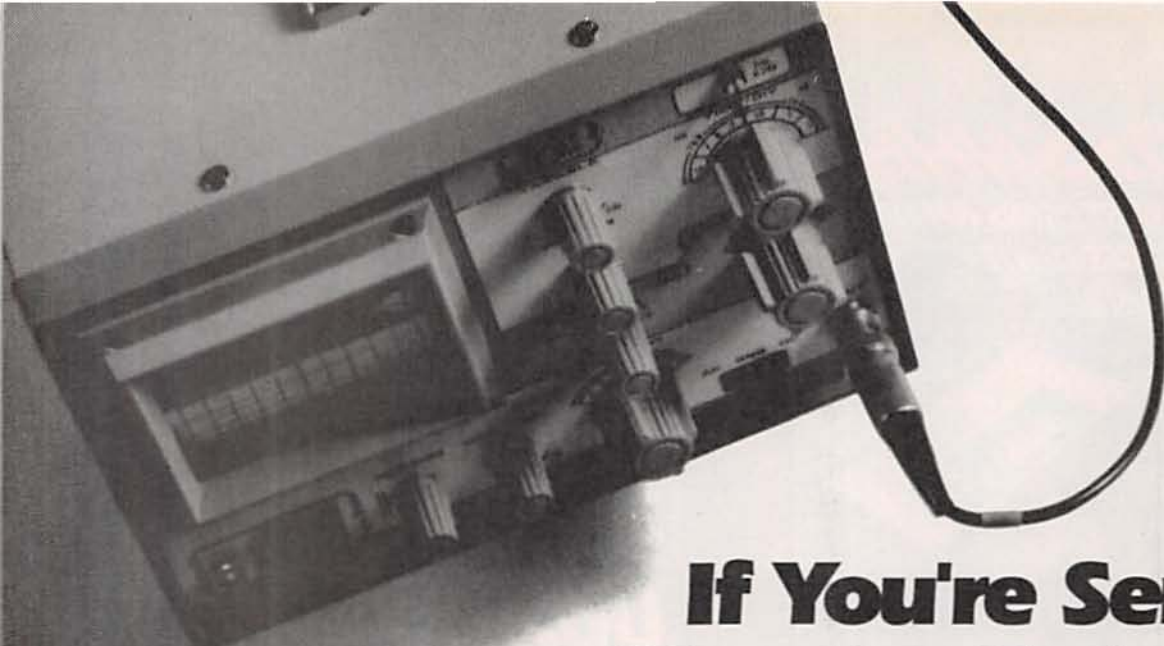
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Procedure

Figure 16 shows the circuit diagram for this experiment. You'll see the pin numbers for the IC aren't included on the diagram. For those, you'll have to refer to Fig. 17, which shows pertinent 74151A data. For the data sheet, you'll see an eight-pole DIP switch in conjunction with 10 420-ohm resistors. For the S1 and S2 switches, finally, you'll see the output data switches.

1. With the power off, mount the 74151A IC and the DIP switch on the breadboard.
2. Connect the eight 420-ohm resistors to the DIP switch as shown in Fig. 16. Connect the opposite end of each of these resistors to the +5V supply. The second terminal of each switch is to be connected to circuit ground.
3. Connect the V_{CC} pin to +5V; connect the GND pin to circuit ground.
4. Next, connect the three data switches to the S1, S2, and S3 inputs on the IC, using Fig. 17 as a guide. Finally, set SW1 through SW3 to 1.
5. Connect the three 1-LEDs to the Y output, and connect the 1-LED to the B output.

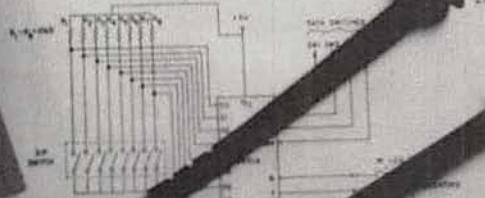


Fig. 16 Circuit for Experiment 3.

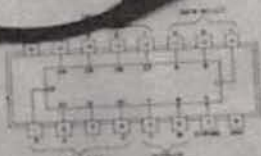


Fig. 17 Pin diagram for 74151A.

1. Turn the power on. The 1-LED on the Y output should be off, and the B LED should be on. If you don't observe these conditions, turn off the power and check your connections.
2. From the present input conditions, on the inputs, you can see that the inputs will be changed.
3. Set the appropriate DIP switch (1) to 0, and verify your condition. Record your results in terms of the selected input Y, where Y is the number of the selected data line on the appropriate space of the truth table in Fig. 15.

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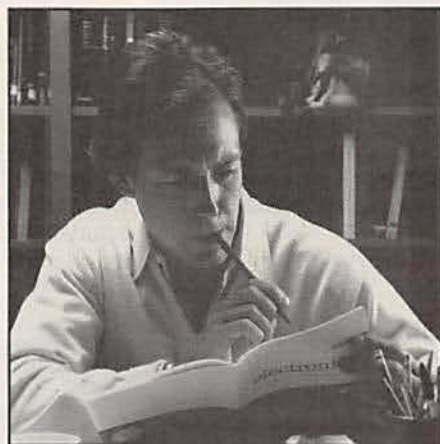
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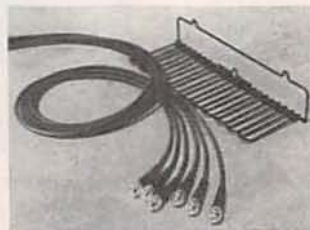
Options for input voltages for the Model 4130 are 110, 115, 220, 230, or 240 volts AC. Prices start at \$122.—Calex Mfg. Co., Inc., 2401 Stanwell Drive, Concord, CA 94520-4841; Phone: 800-542-3355; Fax: 510-687-3333.

COAXIAL ADAPTER CABLE KIT AND CONNECTOR KIT.

Test Probes' universal coaxial adapter cable kit, TPI-5010, is intended for use with the company's TPI-3000A connector kit. Each of the six adapter cables in the kit accepts all combinations of BNC, TNC, SMA, N, UHF, Mini-UHF, F, and RCA connectors.

According to the manufacturer, any combination of two connectors from the 24 available in the TPI-3000A kit can be at-

tached to the ends of one of the six universal cables in the TPI-5010 kit. Because no crimping or soldering is required, the cables can be used repeatedly and in different configurations. The six RG-58 cables in the kit are double-braid shielded, 48 inches long, and have soft poly-



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vinyl chloride (PVC) jackets.

The TPI-3000A connector kit include two male and two female connectors for BNC, N, UHF, and TNC adapters and one male and one female connector for the SMA, Mini-UHF, F, and RCA adapters along with six universal interfaces.

All connectors have silver-plated machined brass shells and gold-plated contacts. Both kits are said to be convenient for servicing communications equipment and local-area networks in the field, and interfacing or connecting for various RF systems and test equipment.

The TPI-5010 kit containing six cables and a plastic-coated wall rack is priced at \$98. The TPI-3000A connector kit with 24 connectors sells for \$150.—Test Probes, Inc., 9178 Brown Deer Road, San Diego, CA 92121; Phone: 800-368-5719.

BRIGHT LED LAMPS. The light-emitting diode lamps in this new family from Lumex Opto/Components are intended as replace-



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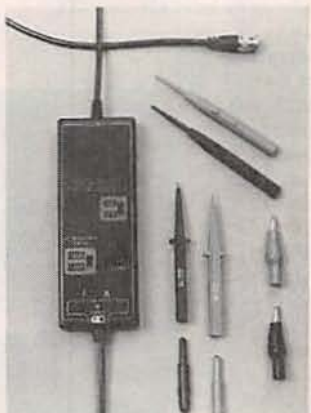
ments for incandescent lamps in existing products. McLED's are made with from two to eight LED dies to obtain light output comparable to that of the incandescent bulb it replaces. The multi-LED lamps are offered with wire ends or standard incandescent lamp bases. They are said to run cooler and save the time and cost of frequent filament lamp replacement in the field.

The lamps are being sold as replacements for miniature and sub-miniature incandescent lamps with ratings from 2 to 20 volts AC or DC. The AC lamp replacements include miniature rectifier bridges to permit them to operate from AC sources. (Individual LED dies draw currents of 2 to 25 milliamperes at 1.5 to 2.8 volts DC.) The DC lamp replacements can be mounted directly on PC boards or front panels. Lumex obtains a near-white light output for its lamps by mixing LED dies that emit different colors on the same lamp header.

The prices of McLED's vary from \$1.00 to \$10 each, depending on order quantity, color, and package.—Lumex Opto/Components Inc., 292 East Hellen Road, Palatine, IL 60067; Phone: 708-359-2790; Fax: 708-359-8904.

DIFFERENTIAL OSCILLOSCOPE PROBE. Two different signals can be measured on one oscilloscope channel with this active differential os-

cilloscope probe, and there is no need for a ground reference to make the measurement. The model ADF15, from Test Probes, Inc. was designed to permit the oscilloscope to be grounded for safety while measurements are made without isolation ampli-



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fiers. This feature is said to eliminate errors caused by the voltage differences between two amplifiers and two probes.

The ADF15 is intended for making high voltage differential measurements in switching power supplies, motor controllers that include thyristors, and power MOSFET's. It can also make accurate measurements of small signal differences in the presence of high common-mode voltage. The probe's bandwidth covers the range of DC to 15 MHz and it has a switchable x20 to x200 attenuation mode.

The probe is powered by four AA batteries or an external 6-volt DC converter (not supplied). The price includes standard probes, alligator clips, and spring-tip probes with banana-plug leads.

The ADF15 probe is priced at \$375.—Test Probes, Inc., 9178 Brown Deer Road, San Diego, CA 92121; Phone: 619-535-9292. **R-E**

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sumer on-line databases including EasyNet, Dialog, BRS, MEAD, STN, ORBIT, Dow Jones, and EPIC. Techniques are presented for evaluating information obtained through on-line systems and putting it to profitable use.

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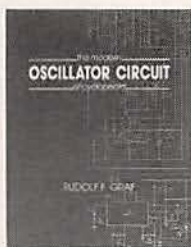
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THE MODERN OSCILLATOR CIRCUIT ENCYCLOPEDIA; by Rudolf F. Graf. TAB Books, Division of McGraw-Hill Inc., Blue Ridge Summit, PA 17294-0850; Tel. 1-800-822-8138; \$12.95.

This circuit encyclopedia is a handy reference for those who want instant access to more than 250 proven, practical oscillator circuit designs. Some of the circuits contain late-model ICs that simplify their construction and reduce the number of components needed. Needless to say, they add to the versatility and reliability of the resulting oscillator.

Mr. Graf's encyclopedia includes schematics for virtually every type of oscillator circuit that has ever been designed—some that are very familiar and others that are obscure—even to experts. The names of many of the oscillator circuits are familiar to students and seasoned professionals alike. Their operation is taught in engineering classes as well as vocational and military tech schools. There are, for example, the old familiar Armstrong, Clapp, Colpitts, Franklin, Hartley, Hertz, Miller, Pierce and Wien-bridge oscillators as well as audio, blocking, crystal, multivibrator and electron-coupled versions.



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The schematics and descriptions are organized by application for easy reference. The circuit schematics and descriptive text have been reproduced in the same form in which they were originally published in such sources as **Radio-Electronics**. This was done by Mr. Graf to prevent transcription errors and make them instantly recognizable to readers who might have seen them in the past. The original source for each circuit is listed in a section at the back of the encyclopedia. That permits readers to refer back to the source publications for additional information on construction and application.

THE ARRL SATELLITE ANTHOLOGY; 2nd Edition; from

The American Radio Relay League, 225 Main Street, Newington, CT 06111; \$8.00.

In the 30 years since the first amateur-radio satellite was launched, satellite technology has become increasingly sophisticated. Nevertheless, communication with satellites has become easier. This collection of articles from ARRL's *QST* magazine is intended to help amateur radio operators participate in satellite communications; they dispel the myth that satellite operating is expensive and difficult.



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Amateurs can access satellites with equipment they already own. The informative articles discuss active amateur satellites, their operating features, and how to access them. Several articles, whose content is still valid today, were retained from the first edition. Subjects include satellite tracking and conversing with other operators in other countries. More recent articles discuss presently operating satellites such as AMSAT-OSCAR 13, and look at the next generation of OSCAR satellites.

TROUBLESHOOTING & REPAIRING ELECTRONIC MUSIC SYNTHESIZERS; by Delton T. Horn. TAB Books, Division of McGraw-Hill Inc., Blue Ridge Summit, PA 17294-0850; Tel. 1-800-822-8138; \$16.95.

As music synthesizers become more popular,

there is an increasing demand for instruction material on their maintenance and repair. This book was written for musicians who want to repair their own equipment as well as electronic hobbyists and technicians who need a reliable source of information on synthesizer troubleshooting and repair. Mr. Horn's book gives complete, step-by-step instructions for servicing synthesizers and replacing their components. Both the older analog and more modern digital instruments are covered.

The first half of the book is devoted to locating and repairing problems that commonly occur in analog synthesizers. Those include nonexistent, weak, or noisy output signals. Also described are methods for repairing voltage sources, function generators and keyboards.

The book's second half covers digital synthesizers. It gives instructions for re-



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pairing digital oscillators, amplifiers, and their power supplies. Topics discussed include logic probes and logic pulsers. One whole chapter is devoted to MIDI with discussion of cabling, channels and circuitry. Instructions are given on what to do if your synthesizer fails to respond to MIDI commands. In addition, the book offers advice on how to restore old or unusable synthesizers as well as how to modify and expand existing units.

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VFX

DIGITAL SIGNAL PROCESSOR

WOULD YOU LIKE TO CHANGE THE pitch of your voice or create such special audio effects as echo or reverb? We will show you how to build a voice effects processor (or VFX processor, for short) that can generate such unusual effects. We'll explain the basic algorithms used to perform these DSP (digital signal processing) techniques, and examine the heart of the VFX hardware, the Analog Devices-2105 digital signal processing microcomputer. If you're on a tight budget, you'll appreciate that this project costs much less than any commercial single-effect generator.

Before we describe the details of the hardware and software, let's look at what the VFX processor does. The VFX processor accepts audio signals, digitally processes the information in one of three user-selected modes, and amplifies the signal for listening with a speaker or a pair of headphones. All you need besides the VFX processor is a microphone, a pair of headphones, and a 9-volt DC power source—all of which are available from the source given in the Parts List.

Basic operation

The VFX block diagram is shown in Fig. 1. A four-position DIP switch (of which only three are used) puts the VFX into one of four operating modes: harmonizer, echo, reverb, and test. Table 1 shows the DIP switch

positions for each mode. The harmonizer voice effect raises or lowers the pitch of your voice. A high pitch makes you sound as if you're breathing helium, and a low pitch makes you sound like a baritone singer. In this mode, a single-digit LED readout indicates the pitch change level; 0 is the maximum down shift (3% or Hz) and 9 is

the maximum upshift (+305 Hz). The VFX board powers up in level 4, which is no shift at all. A SHIFT button lets you step through the range of pitch shifts; after 9 the processor returns to 0. Each pitch shift increment is approximately 51 Hz; we'll explain why later.

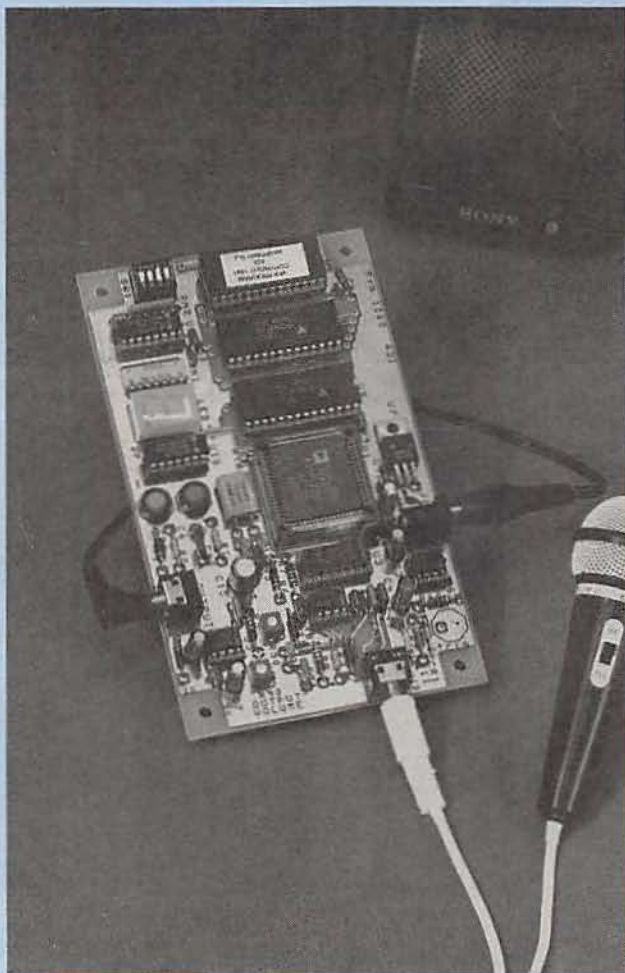
The echo effect has an adjustable delay; you can decrease the echo delay time by pressing the SHIFT button. In this mode the LED displays a number from 9 to 0 indicating a delay time of 0.63 to 0 seconds. Each press of the SHIFT button decreases the time delay by 70 milliseconds.

The reverb effect is similar to the echo effect, except that the delay time is fixed at 78 milliseconds and the amplitude of the feedback signal is adjustable from 0.5 to 0 with the SHIFT button. The effect is more subtle than the echo effect and simulates the acoustics of a large room.

The test mode helps troubleshoot the VFX board. The test mode will be discussed in greater detail later on.

The basic circuit

As shown in the block diagram (Fig. 1), the VFX processor consists of a microphone input circuit that uses a National Semiconductor TP3054 CODEC (coder-decoder), an Analog Devices ADSP-2105 DSP (digital signal processor), an 8K x 8 EPROM (erasable program-



***A little DSP goes a long way
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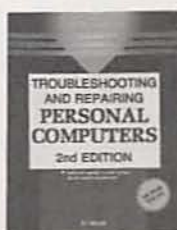
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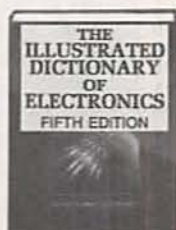
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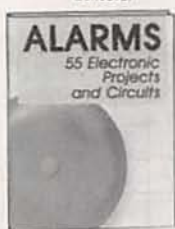
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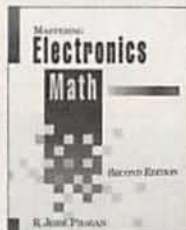
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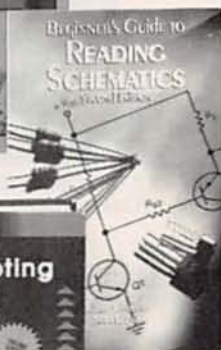
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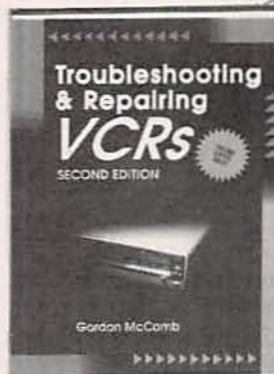
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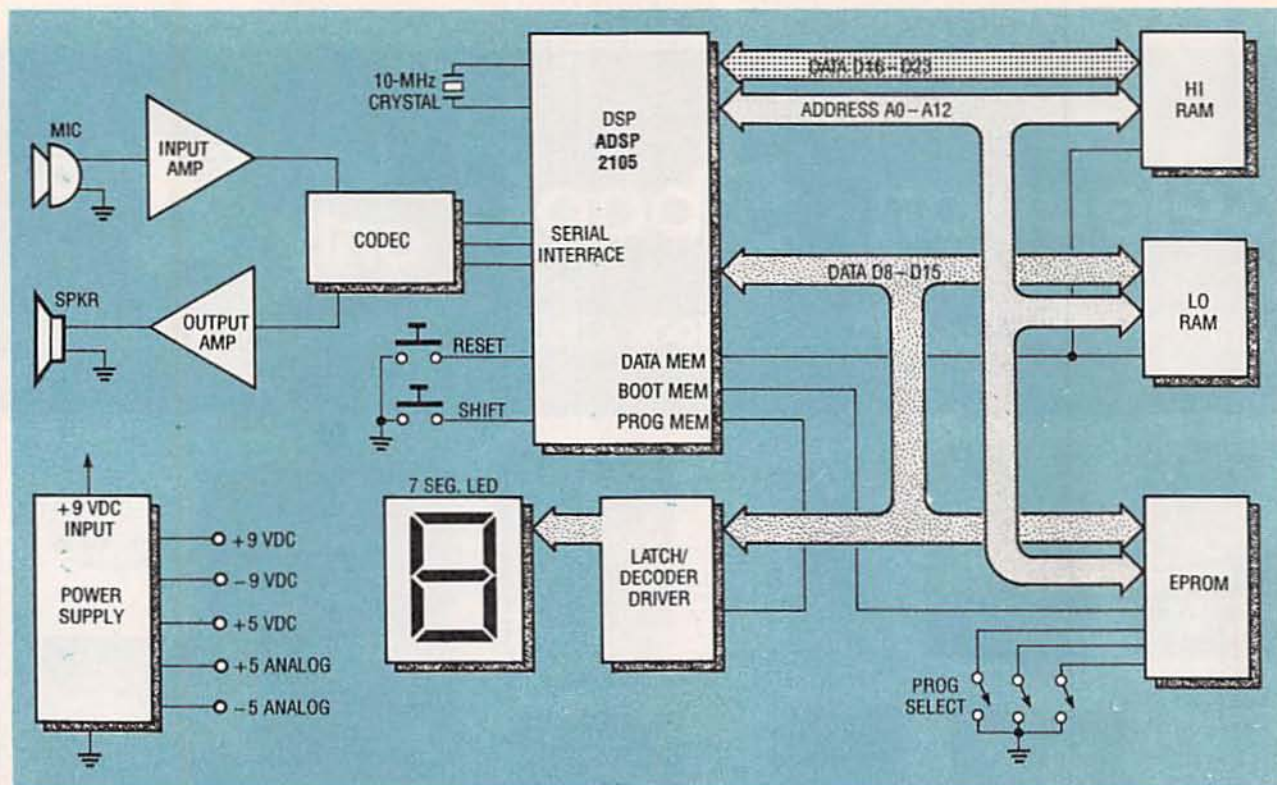


FIG. 1—VFX BLOCK DIAGRAM. The VFX has a microphone input, a CODEC, a DSP, EPROM, SRAM, power-supply circuitry, and audio conditioning.

mable read-only memory), two 8K × 8 SRAM's (static-random access memory), power-supply circuitry, and audio conditioning. The CODEC incorporates an input anti-aliasing filter, an A/D converter, a D/A converter, an output filter, and control circuitry. The SRAM's provide 8K × 16-bit words of data storage to supplement the 2105's internal 512 words. The DSP can access external memory in 100 nanoseconds but has an internal wait-state generator to allow the use of slower devices. The VFX processor has three wait states programmed for external data memory access.

The VFX processor performs four functions; the theory of operation for each implemented in hardware is virtually identical. The software makes the hardware perform these multiple

effects. The EPROM hex code will be posted on the RE-BBS (516-293-2283, 1200/2400, 8N1), as a file called VFX.HEX. Let's look at the algorithms used for each effect.

Algorithms

The harmonizer shifts the pitch of an audio signal, such as music or speech, up or down. One of the most widely known uses of this technique is seen in the novelty musical group, the Chipmunks. Recorded in the early 60's, the Chipmunks' up-pitch effect was made simply by playing back audio tapes at a higher speed. Today, the high-tech approach is to use digital signal processing.

The principal algorithms performed by the DSP hardware for the harmonizer are the fast Fourier transform (FFT) and the inverse FFT (IFFT). Those al-

gorithms convert the audio signal in the time domain to the frequency domain, and then back again. Figure 2 shows an original audio signal and the data at each stage in the process as it is spectrum-shifted. Figure 2-a plots the audio input versus time. Figure 2-b shows the frequency spectrum of the audio signal in 2-a. Figure 2-c shows the original spectrum at the top and the up-shifted spectrum at the bottom. Figure 2-d shows the original audio signal on top with the processed audio signal, which contains higher-frequency components, at the bottom.

The timing of the algorithm of the harmonizer is shown in Fig.

THE FFT

The Fourier series and its related transforms and algorithms are widely used in electronics. The Fourier transform (FT) is a mathematical method for converting a signal from the time domain to the frequency domain, or simply a way of expressing a continuous waveform as a series of sine waves. The fast Fourier transform (FFT) is an algorithm enhanced for computer computation of a discrete Fourier transform (DFT), which is the digital equivalent of the Fourier transform. R-E

TABLE 1—DIP SWITCH SETTINGS

	S1-a	S1-b	S1-c	S1-d
Harmonizer	X	ON	ON	ON
Echo	X	OFF	ON	ON
Reverb	X	ON	OFF	ON
Test Mode	X	OFF	OFF	ON

3, and its block diagram is shown in Fig. 4. In Fig. 3, the input signal from the microphone is sampled at a 6.5-kHz rate. At that rate buffer #1 is filled in 19.7 milliseconds with 128 samples. (That determines the pitch resolution because the resolution in the frequency domain is the inverse of the sampling period, or 50.7 Hz.) Then the next 128 samples are stored in buffer #2. (The double-throw switch in Fig. 4 is there to suggest the toggling from one buffer to the other.) While buffer #2 is being filled, the VFX processor begins the harmonizing effect by processing buffer #1 through a 128-point FFT, then comes the shift, and then the IFFT. The entire FFT/Shift/IFFT algorithm takes approximately 6 milliseconds so that all processing is finished before the next buffer is filled. That allows real-time processing with a minimal two-buffer delay of 39.3 milliseconds between the time the microphone input arrives at the VFX processor and when it is output to the speaker.

The echo-effect algorithm uses a digital implementation of an adjustable-length analog delay line as shown in Fig. 5. The input signal from the microphone is sampled at a 6.5-kHz rate. It is then summed with the delayed signal received $n \times 455$ periods ago (where n is a number from zero to nine as shown on the VFX's LED display). The delay line is implemented in 4K of external SRAM. The software allows the adjustment of the delay from 0.63 to 0 milliseconds.

The reverb effect is very similar to the echo effect (see Fig. 6) except that the length of the delay line is fixed at 78 milliseconds, and the reflection factor is adjustable from 0% to 50% with the SHIFT button. The reflection factor determines the attenuation of the signal before it is stored in the delay line and simulates the reflection factor of a room.

The test mode can be used during hardware checkout to isolate problems with your VFX board. We'll discuss how to use the test mode later.

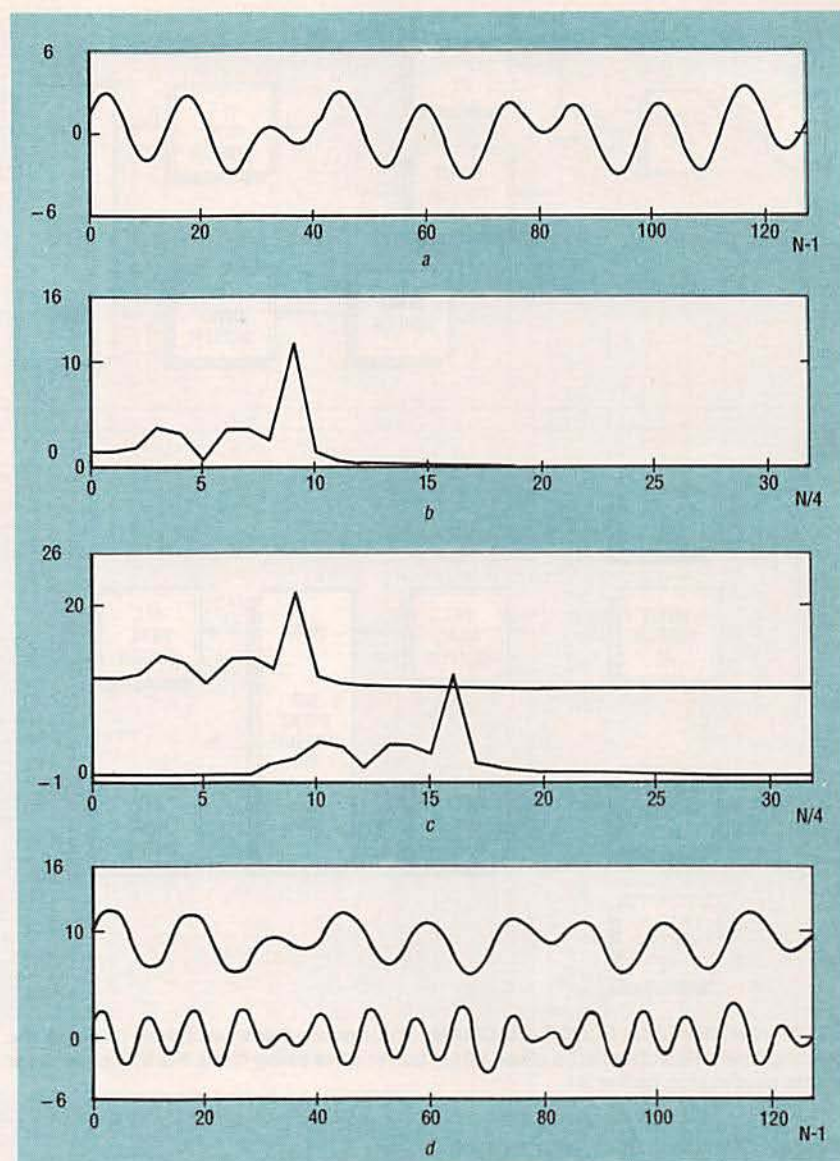


FIG. 2—HARMONIZER ALGORITHM. In *a* you see the audio input vs. time, *b* shows the frequency spectrum of the audio signal, *c* shows the original spectrum at the top and the up-shifted spectrum at the bottom, and *d* shows the original audio signal on top with the processed audio signal at the bottom.

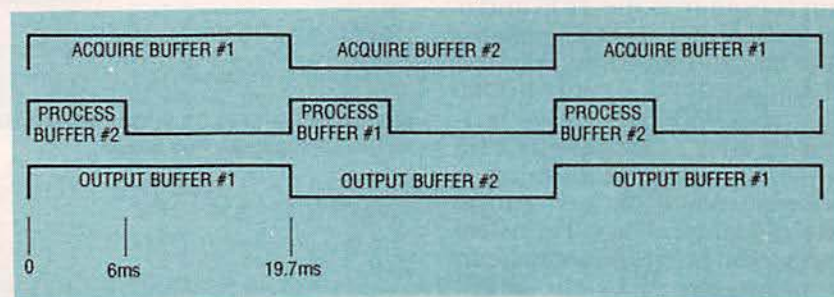


FIG. 3—HARMONIZER TIMING DIAGRAM. The input signal is sampled at a 6.5-kHz rate and fills buffer #1 in 19.7 milliseconds with 128 samples. The next 128 samples are stored in buffer #2.

Circuitry

The schematic diagram for the VFX processor is shown in Fig. 7. The ADSP-2105 DSP mi-

croprocessor, IC1, has $1K \times 24$ -bit words of fast program memory (PM) on chip. An on-chip oscillator requires a 10-MHz

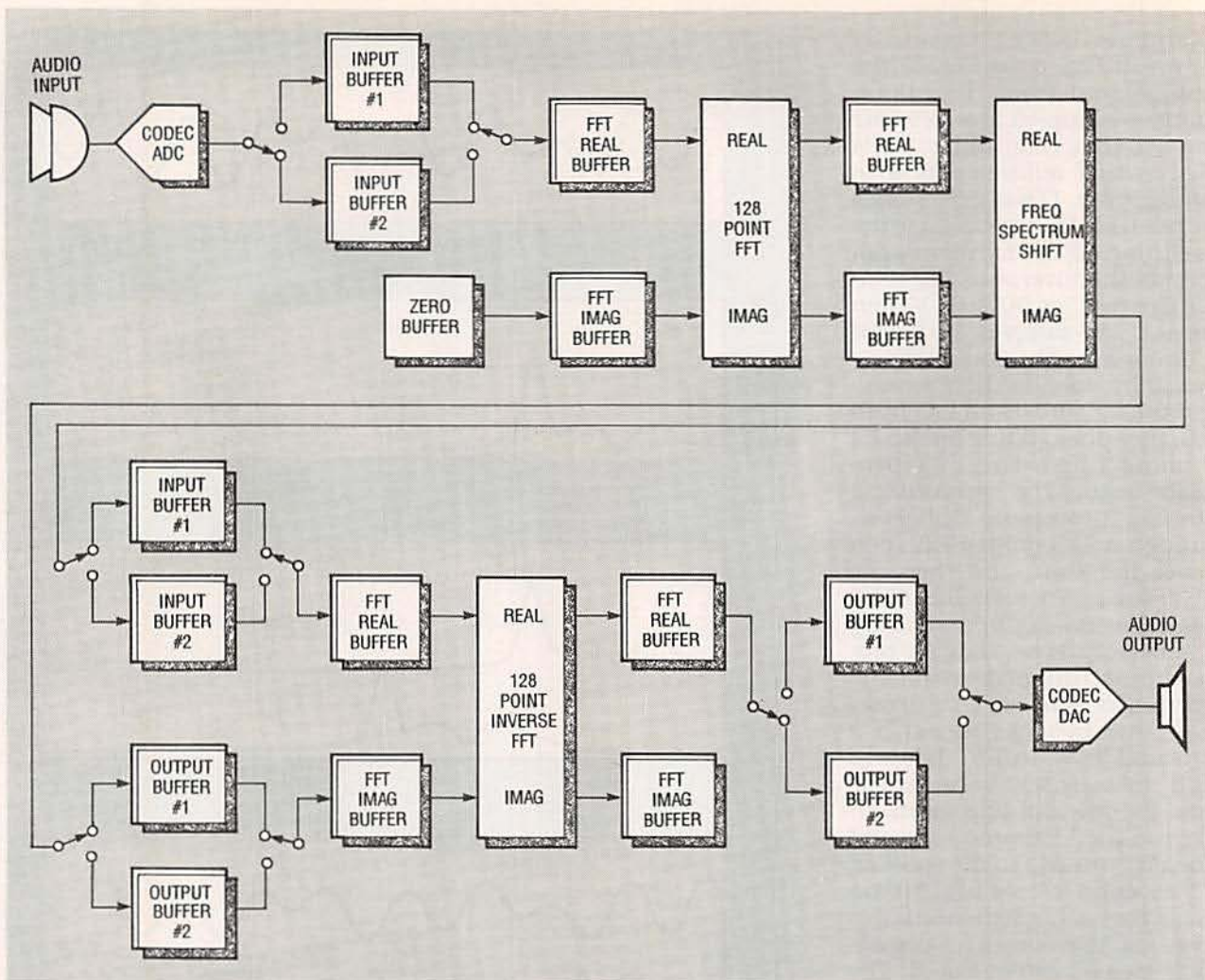


FIG. 4—HARMONIZER BLOCK DIAGRAM. The double-throw switches indicate the toggling from one buffer to the other. While buffer #2 is being filled, the VFX processor begins processing buffer #1.

crystal (XTAL1) and two small capacitors (C1 and C2). On power-up and after a reset, the 2105 boots the program from the EPROM (IC2) into the on-board memory. The boot function is built into the 2105 and it allows a slower and inexpensive EPROM (250 ns) to supply the 1K words (3K bytes) of PM. The BOOT MEMORY SELECT (BMS) output of the 2105 selects the EPROM, and the addressing is automatically generated on the external address bus. The selection of the program booted can be programmed by the 2105, but to simplify the VFX hardware and software, the program is selected by setting the three most-significant bits (MSB's) of the EPROM's address with DIP switch S1.

In addition to the on-board PM, there is $0.5K \times 16$ -bit words

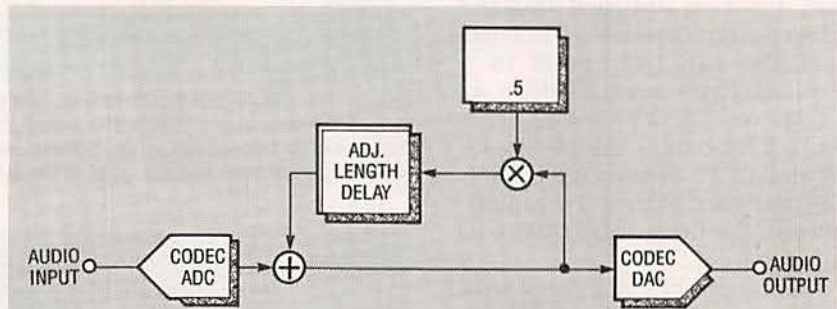


FIG. 5—ECHO-EFFECT BLOCK DIAGRAM. A digital implementation of an adjustable-length analog delay line is used.

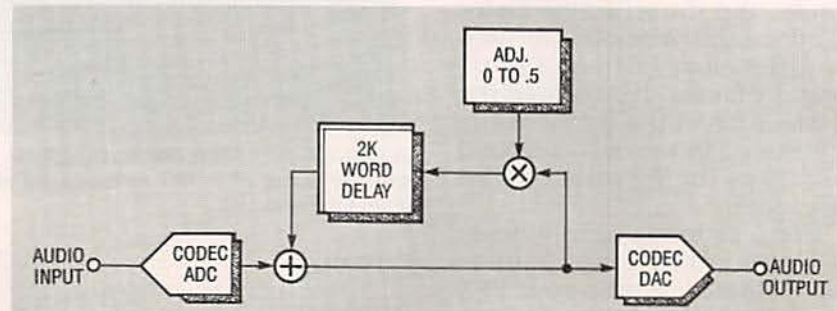


FIG. 6—REVERB EFFECT BLOCK DIAGRAM. The length of the delay line is fixed at 78 milliseconds, and the reflection factor is adjustable from 0% to 50%.

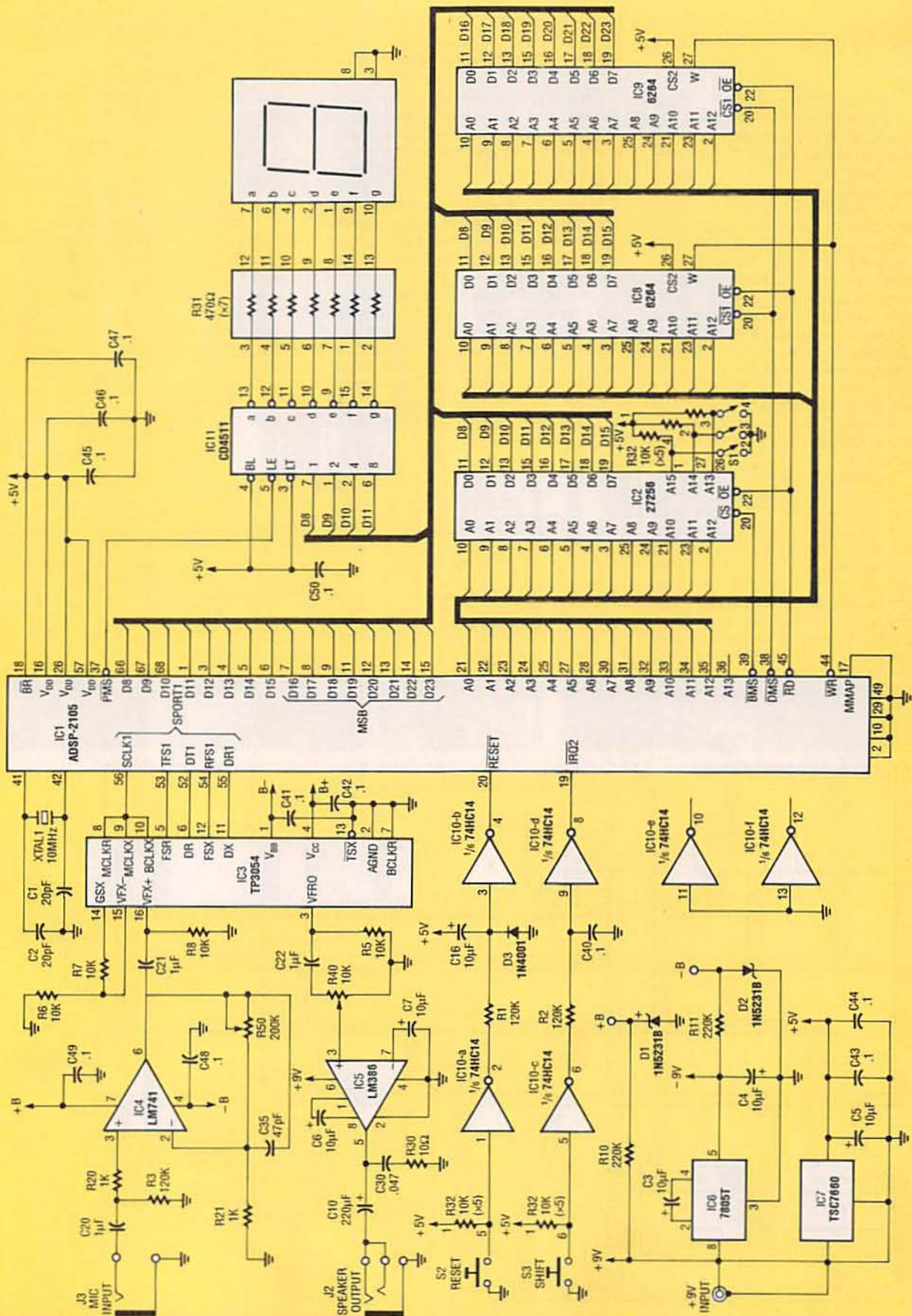


FIG. 7—VFX SCHEMATIC. The DSP microprocessor (IC1) has 1K × 24-bit words of fast program memory (PM) on chip. On power-up, the 2105 boots the program from the EPROM IC2 into the on-board memory.

THE ADSP-2105

The Analog Devices ADSP-2105 is the engine of the VFX processor. The ADSP-2105 is a second-generation digital signal processing (DSP) microcomputer based on the earlier ADSP-2100. It has significant architectural improvements over earlier generations (see block diagram in Fig. 10). The 2105 has built-in data memory RAM ($0.5K \times 16$ bits) and program memory RAM ($1K \times 24$ bits) so it really is a DSP microcomputer and not a microprocessor. Both of those memory banks are expandable with off-chip fast static RAM. That allows the program memory to be loaded, using the resident boot memory loader, from a slow PROM or EPROM (250 nanosecond access) and keeps high-speed data transfer inside the chip to reduce EMI and board-layout requirements.

The program and data memory can be easily expanded off-chip—as has been done with the VFX processor—when the internal data memory is not sufficient for the algorithms. The chip has resources built-in to simplify external memory hardware interfacing. They include separate selects for program memory, data memory, and boot memory, and a programmable wait-state generator to allow for slow external memories.

The 2105 incorporates several pe-

ripheral devices and their associated interrupts. There is a built-in 16-bit interval timer with programmable prescaler and interrupts. A high-speed synchronous serial interface (SPORT1) can interface to μ -law and A-law CODEC's using hardware companding as well as digital audio-oriented D/A and A/D converters. Additionally, the serial port can connect multiple 2105's together in parallel processing applications.

The ADSP-2105 also offers high performance by virtue of its instruction set. With a 100-nanosecond cycle time, multiple operations per cycle, and zero-overhead looping, the numerical performance of the chip is respectable. In addition, the 1-micron low-power CMOS processing holds power dissipation to

less than 1 watt; a powerdown mode reduces the power consumption to a mere 80 milliwatts.

The ADSP-2105 incorporates three execution units:

- Barrel shifter
- Arithmetic Logic Unit (ALU)
- Multiplier Accumulator (MAC)

The three units are optimized for their specific function, and are, therefore, very fast, completing any instruction in one cycle. Access to the three execution units is made via registers associated with each execution unit. For example, the ALU has the following 16-bit registers:

AX0, AX1, AY0, AY1, AR, and AF

The MAC has:

MX0, MX1, MY0, MY1, MR0, MR1, MR2,

LISTING 1

```

START:
        IO=buffer#1;           {Address of buffer#1 in DMD}
        MO=1;                 {Post modify value}
        I4=buffer#2;         {Address of buffer#2 in PMD}
        MO=1;                 {Post modify value}
        CNTR=2048;           {Number of words in buffer}
DO MOVE BUFFER UNTIL CE;
        AR=PM(I4, M4);
        DM(IO, MO)=AR;
MOV_BUFFER:                               {End of the loop}
    
```

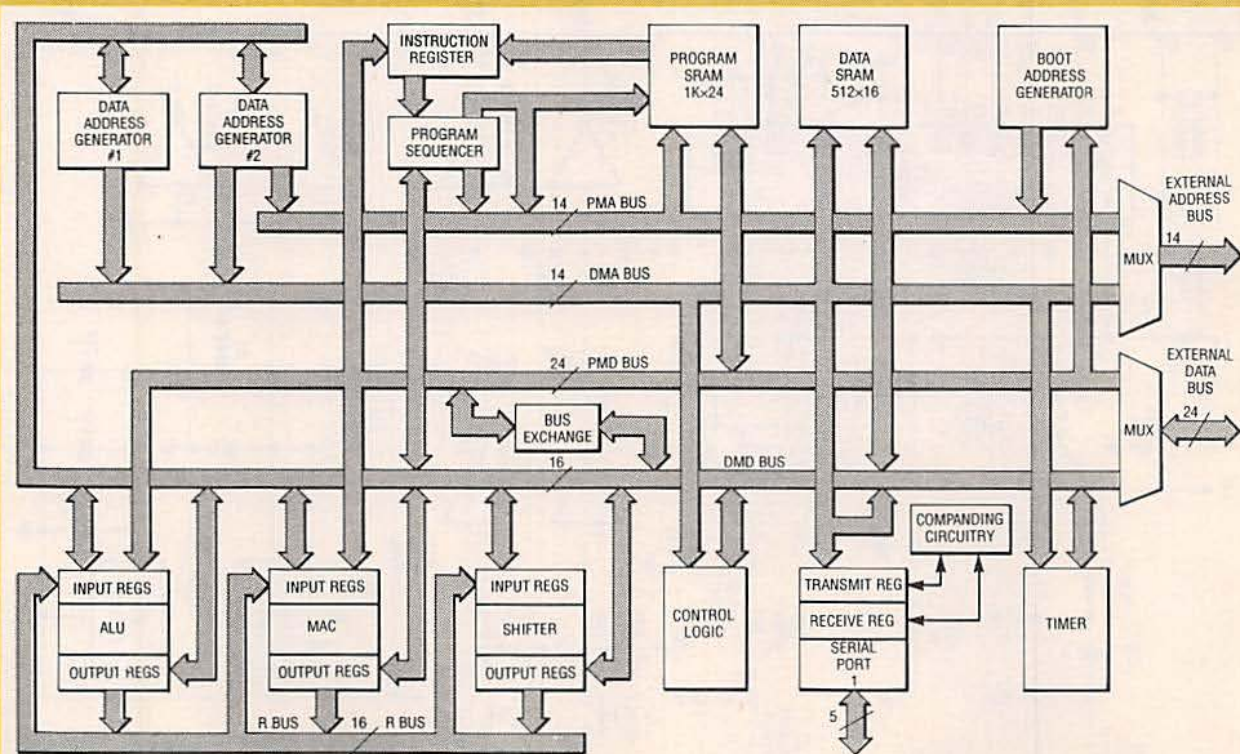


FIG. 10—ADSP-2105 BLOCK DIAGRAM. The 2105 has built-in data memory and program memory implemented in fast SRAM. That keeps high-speed data transfer inside the chip.

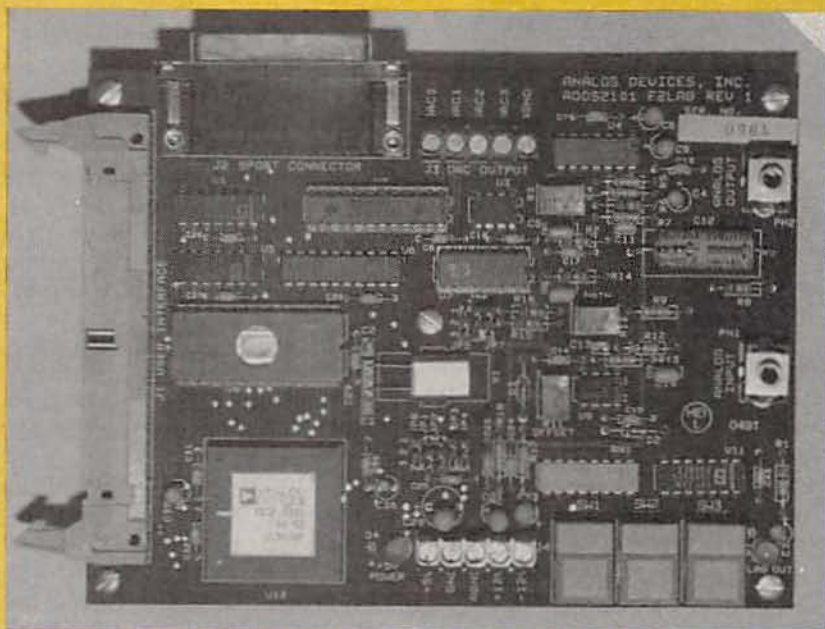


FIG. 11—THE EZ-LAB KIT includes a demo board, an ADSP-2101/5 family assembler, linker, and other miscellaneous development software. You can design and debug software for certain applications at minimal cost.

and MF

The barrel shifter has:

SB, SI, SE, SR1, and SR0

In addition, the ADSP-2105 incorporates two data address generators (DAG's), one of which can perform the bit reversing that is required for certain FFT algorithms. One DAG accesses program-memory data (PMD) and the other accesses data-memory data (DMD). The DAG's use a set of three registers to control indirect addressing and circular buffers. Those are the index registers (I0 to I7), the modify registers (M0 to M7), and the length registers (L0 to L7). For example, by setting up the registers so that I0 has the starting address, M0 has a value of 1, and L0 is zero, blocks of data can be moved from one buffer to another with very little programming (see Listing 1).

To be successful, any microcomputer, including a digital signal processor, must have readily available low-cost software tools. Analog Devices has supplied the ADSP-2105 with quality software tools at a reasonable price. The assembly language is algebraic and straightforward. Included is a powerful personal computer-based software simulator that allows software debugging without an expensive in-circuit emulator (ICE).

The ADSP-2105 has the same kind of interrupt handling capabilities as other microcomputers. The interrupts can be individually masked or enabled, edge-triggered or level sensitive. Interrupts are vectored to the program memory lo-

LISTING 2

IRQ2	0004h
SPORT0 (Transmit)	0008h
SPORT0 (Receive)	000Ch
SPORT1 (Transmit)	0010h
SPORT2 (Receive)	0014h
TIMER	0018h

cations shown in Listing 2. A second mirror set of Data registers can be enabled to facilitate fast context switching during its interrupt servicing. The device has on-chip clock generation circuitry and is packaged in a 68-lead plastic leaded chip carrier (PLCC).

The VFX processor described in this article was developed with Analog Devices' ADSP-2101 EZ-Lab Kit (see Fig. 11). The Analog Devices EZ-Lab kit includes an EZ-LAB demonstration board, an ADSP-2101/5 family assembler, linker and other miscellaneous development software, including the essential simulator. With this package one can design and debug software for certain applications with excellent results at minimal cost. Of course, an in-circuit emulator (ICE) will speed up the development process, although, of course, at a much higher price: the EZ-Lab kit sells for less than \$500 dollars, and an emulator costs more than \$2000 dollars. For people with limited capital resources and small to medium complexity algorithms, the kit is great. R-E

of on-board data memory (DM). Since that is not enough to perform the 128-point FFT and IFFT, two external static RAM's are also attached to the data bus, one for the high byte (IC9), and one for the low byte (IC8) of the memory. That 2x8K bytes of SRAM addressed by the 2105 is accessed when the DATA MEMORY SELECT (DMS) strobe is active.

The seven-segment LED display adds to the interactivity of the VFX processor, and is written to as if it was external program memory. The PROGRAM MEMORY SELECT (PMS) signal from the 2105 is activated to latch data from the bus into IC11 (the seven-segment BCD latch/decoder/driver), which then drives the seven segment display. No decoding is required for the selection of IC11 because there is no external program memory in the system.

The VFX processor uses a CODEC to digitize the audio input and convert it into a serial data stream. The CODEC interfaces directly with the 2105's synchronous serial port SPORT1, which includes pins 52-56. SPORT1 is configured for 8-bit synchronous data transfer with word-framing sync pulses and μ -law companding. The 2105 generates a 1.66-MHz serial clock (SCLK1) and 6.5-kHz framing pulses on TRANSMIT FRAME SYNC (TFS1) and RECEIVE FRAME SYNC (RFS1) to synchronize the data transfer.

The CODEC implements μ -law companding, which improves the dynamic range of the conversion by taking advantage of human perception of sound; that is, that the ear is much more sensitive to noise in low-level (volume) signals than in high-level signals. The CODEC receives and transmits 8 bits of data, and the digital signal processor has built-in companding hardware to convert it into a 14-bit number.

The other components of the VFX processor are the power supply and analog components. The VFX board accepts +9 volts DC and generates -9, +5, +5.1, and -5.1 volts DC. Voltage converter IC7 (a TSC7660)

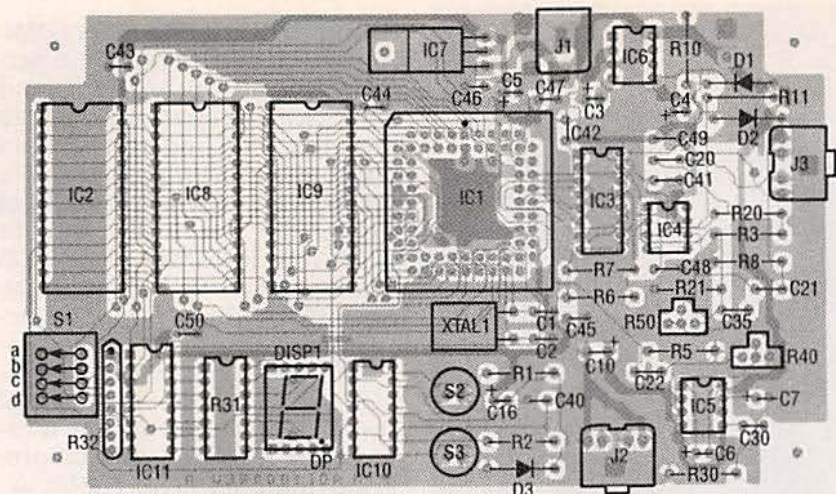


FIG. 8—PARTS-PLACEMENT DIAGRAM. Make sure that you install the mono jack at J1 and the stereo jack at J2.

PARTS LIST

All resistors are 1/4-watt, 5%, unless otherwise noted.

R1-R3—120,000 ohms
 R4, R9, R12-R19, R22-R29, R33-R39, R41-R49—not used
 R5-R8—10,000 ohms
 R10, R11—220,000 ohms
 R20, R21—1000 ohms
 R30—10 ohms
 R31—470 ohms ($\times 7$), 14-pin DIP
 R32—10,000 ohms ($\times 5$), 6-pin SIP
 R40—10,000 ohms, multiturn potentiometer
 R50—200,000 ohms, multiturn potentiometer

Capacitors

C1, C2—20 pF, 100 volts, ceramic
 C3-C7—10 μ F, 35 volts, electrolytic
 C8, C9, C11-C15, C17-C19, C23-C29, C31-C34, C36-C39—not used
 C10—220 μ F, 25 volts, electrolytic
 C16—10 μ F, 6.3 volts, Tantalum electrolytic
 C20-C22—1 μ F, 50 volts, ceramic
 C30—0.047 μ F, 100 volts, ceramic
 C35—47 pF, 100 volts, ceramic
 C40-C50—0.1 μ F, 100 volts, ceramic

Semiconductors

IC1—ADSP-2105KP40 DSP processor
 IC2—27256-25 32K \times 8 EPROM (256K)
 IC3—TP3054J CODEC
 IC4—LM741N op-amp
 IC5—LM386N-3 audio amplifier
 IC6—7660SCPA voltage converter

IC7—7805T 5-volt regulator
 IC8, IC9—6264-15 SRAM, 150 ns
 IC10—74HC14N hex Schmitt trigger inverter
 IC11—CD4511 7-segment decoder/driver
 D1, D2—1N5231B 5.1-volt Zener diode
 D3—1N4001 diode
 DISP1—LTS6780R 7-segment common cathode LED
Other components
 XTAL1—10-MHz crystal
 S1—4-position DIP switch
 S2, S3—momentary pushbutton, N.O.

J1—2mm DC power jack

J2—mini stereo jack

J3—mini mono jack

Miscellaneous: IC sockets, 9-volt DC wall transformer, microphone, headphones, PC board, solder, etc.

Note: The following items are available from American Distributors, Inc., 9 Whippany Road, Whippany, NJ 07981 (800) 877-0510:

- VFX kit (includes PC board and all PC-mounted components)—\$105

(plated through holes, solder masked and silkscreened)

- 9-volt wall transformer—\$12

- Headphones—\$15

- Microphone—\$16

Add \$5 shipping and handling. Check, MasterCard, or Visa.

generates the negative supply from the positive supply. A 5-volt DC regulator (IC7, a 7805) supplies +5 volts DC to the 2105 and all logic IC's, and two Zener regulators (D1 and D2)

generate the analog voltages of plus and minus 5.1 volts DC. Op-amp IC4 and audio amplifier IC5 condition and amplify the audio input and output, respectively.

Construction

The VFX processor is easy to build. All the necessary components including a double-sided PC board, all IC's, semiconductors, and passive components are available from the source given in the Parts List. A microphone, DC wall outlet transformer, and headphones are also available if you don't already have them. We've provided foil patterns in case you want to make your own PC board.

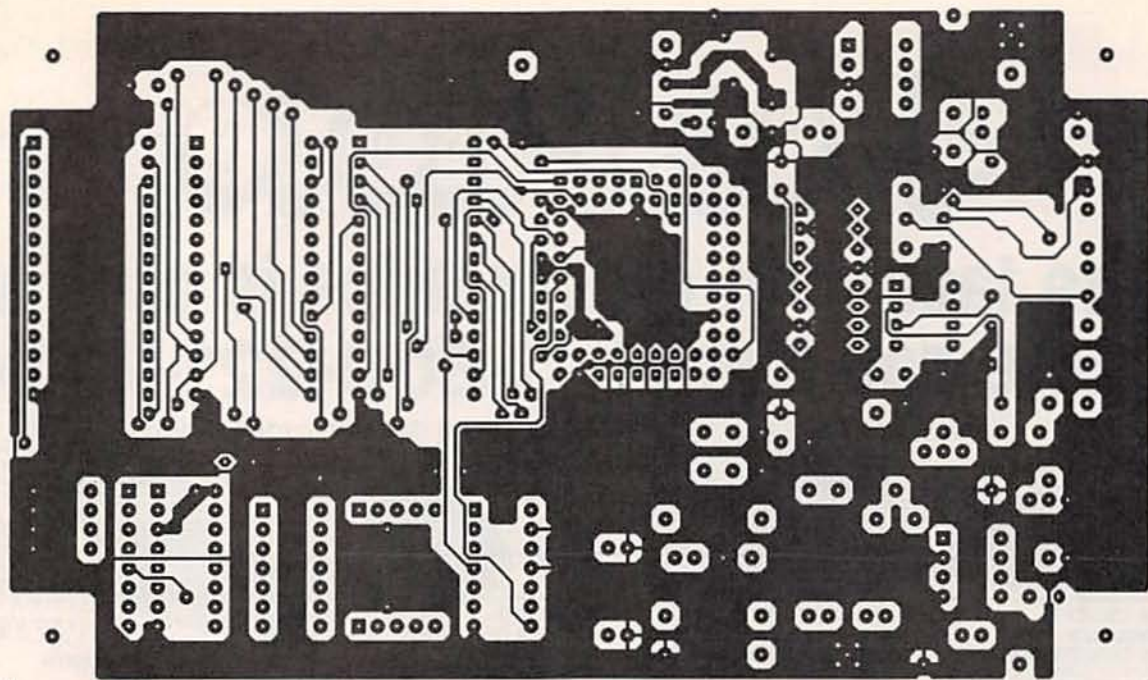
Following Fig. 8 as a guide, mount the components beginning with the resistors. Next install the capacitors, the crystal, switches, jacks, voltage regulator (IC7), and then all of the IC sockets. Make sure you don't install the input and output jacks in the wrong locations. The output jack has three terminals so that if you use headphones you'll hear sound from both sides. Be sure to orient the polarized capacitors correctly. Do not install the IC's yet and don't remove them from their packaging just yet either. When you've completed the soldering, carefully double check parts placement and look for solder splashes and bridging. The completed VFX card is shown in Fig. 9.

Hardware checkout

Now we will perform a hardware checkout, one IC at a time. Precautions against static discharge should be followed when handling the IC's. Electrostatic discharge can cause very subtle damage in the IC that can be hard to find—the kind that is

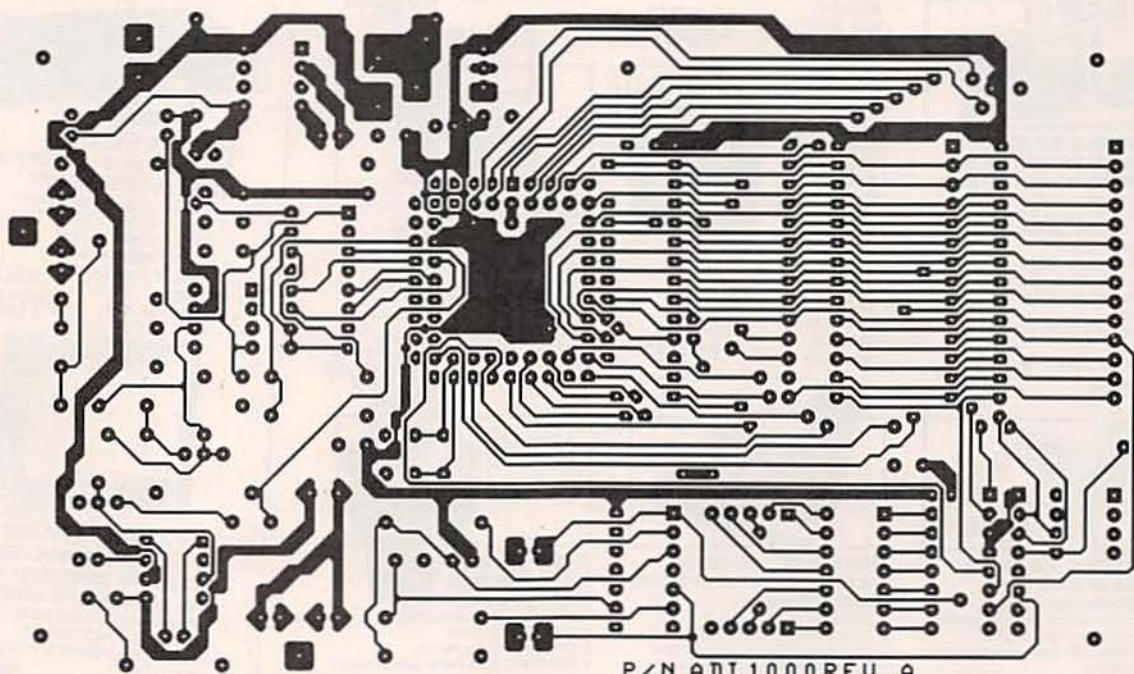
FILTER DESIGN SOFTWARE

The digital filter used in the echo and reverb effect was designed with the filter and digital analysis software (FDAS) from Momentum Data Systems software. The software was used to implement a finite impulse response (FIR) filter. The optional code generator wrote the source code for the filter, given its characteristics. The package also runs on the ADSP-2101 processor and other family members. The FDAS software can also implement other kinds of digital filters than FIR, including infinite impulse response (IIR) and some analog equivalents. **R-E**



6 INCHES

COMPONENT SIDE of the VFX board.



P/N ADI 1000REV. A

6 INCHES

SOLDER SIDE of the VFX board.

worth avoiding.

First apply 9-volt DC power to J1 and verify that there is 5 volts on the power pins of each IC socket. When verified, remove power from the board and plug in IC6, the negative-supply gen-

erator. Now reapply 9-volts DC to J1 and measure pin 5 of IC6; the voltage should be the negative of the voltage on IC6 pin 8 or -12 volts (whichever is less).

Next, check pins 1 and 4 of IC3 for -5 volts \pm 0.2 volt and +5.0 \pm 0.2 volt, respectively.

Install IC1, IC2, IC10, and IC11 in their respective sockets. For the RAM test, set all the S1 DIP switches to the "on" position and apply power to the board. The LED display should show the number "6." Press the SHIFT
continued on page 94

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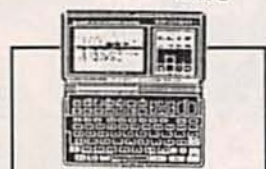


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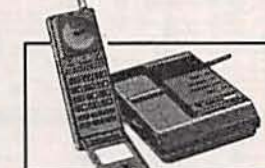
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FROM NotWorking To NETWORKING

Learn about basic and advanced equipment for troubleshooting LAN's.



GARY McCLELLAN

THIS IS PART 2 OF A THREE-PART SERIES on troubleshooting local-area networks (LAN's). In Part 1 we presented technical background on network technologies including cable types, topologies, signal schemes, and access protocols. This time we introduce the tools and test equipment necessary to service LAN's quickly and effectively. Next time we'll put our knowledge to work in diagnosing and solving easy and difficult network problems.

Experts say that cable faults cause more than 70% of all network failures. Cable faults may sound simple in theory but, in practice, diagnosing and locating them can bring strong men to tears. However, common sense, good test equipment, and intelligent substitution techniques can take you a long way toward rapid, inexpensive repair.

Common sense helps you localize the problem to avoid wasting time performing irrelevant tests. Good test instruments are your eyes and ears into the LAN; equipment can be as simple as a \$20 digital multimeter (DMM) or as complex as a time-domain reflectometer (TDR) costing thousands of dollars. (A TDR uses radar-like techniques to measure the distance to a cable fault. Typically a test instrument transmits a signal and measures the time it

takes for its reflection to return to the source.)

Gone are the days of mindlessly swapping computers, boards, and cables. Instead we use intelligent swapping to localize a problem, and then use appropriate test equipment to find the suspect part. Next we install a substitute, and if the LAN comes to life, that part remains. Otherwise, we will repeat the process until the fault disappears and the LAN comes on-line.

Some training firms claim that only a screwdriver is required to service a LAN. We won't go that far—but with the techniques discussed here, we'll come close.

Hand tools

Common hand tools are useful in servicing LAN's. Table 1 describes the basic requirements; you'll probably add other, more specialized tools to the list as time goes on.

One quick and easy way to get the tools you need is to buy a Jensen tool kit. For example, the reasonably priced JTK-5 tool kit contains all the essentials for servicing Ethernet LAN's. Also check with Jensen for tools and tool kits suitable for twisted-pair and Token Ring LAN's.

Probably the most common problem in LAN service is connectors. Sooner or later, you'll

have to replace a bad one. The best way to learn the proper techniques is to work with someone already skilled in the art. Failing that, there are other resources. Try a local electronic parts distributor for manufacturer's literature on connector installation. Or locate a copy of the *Radio Amateur's Handbook*, published by the American Radio Relay League. The Construction Practices chapter of that handbook describes the proper way to install BNC-type coaxial connectors. You might also contact AMP and other manufacturers to request assembly information on their crimp-on coax and RJ-xx series connectors. The sidebar lists several sources of information.

The DMM

No service technician in his right mind would be caught dead without a DMM; it is literally indispensable. You can use it to service LAN's, and also to check building AC-line power and repair electronic equipment of all types. DMM's are available with a dazzling variety of features. If you are shopping for a DMM, choose a 3½-digit unit, like the one shown in Fig. 1, that is easy to use, has the features you really need, and has a low price. Minimum LAN-specific requirements for a DMM include a 0 to 200 ohms range, a continuity beeper, a 0

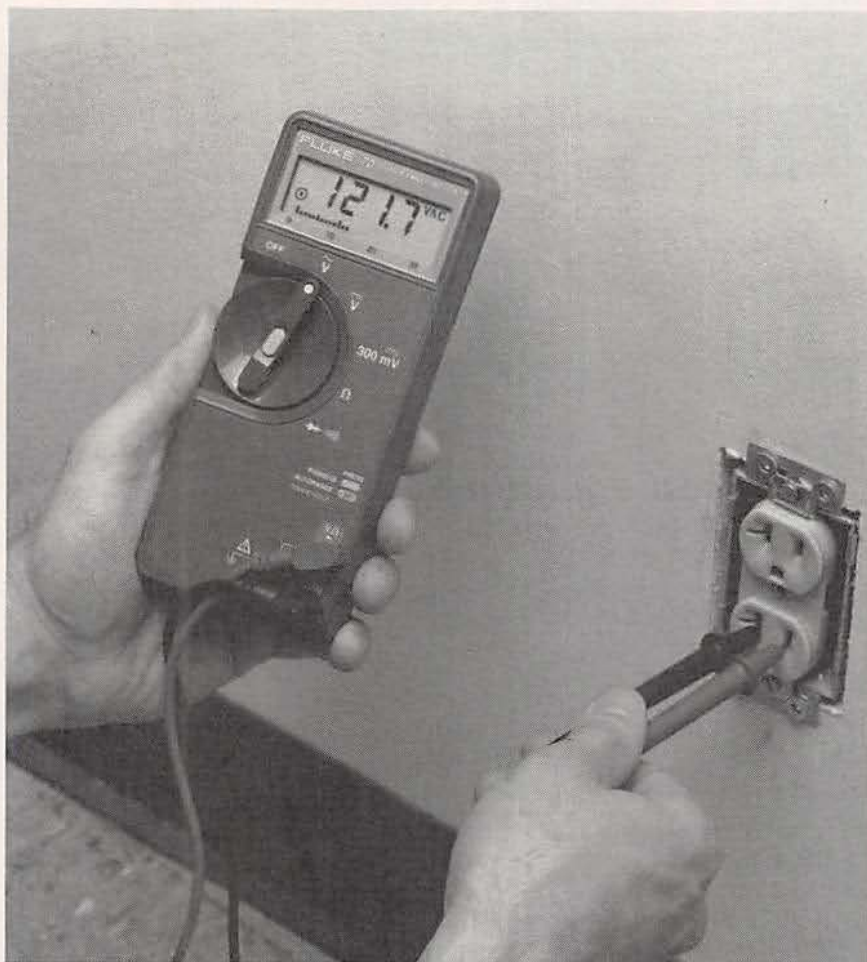


FIG. 1—A BASIC DMM, like the Fluke Model 70, is an indispensable tool for LAN troubleshooting.

to 20-volts DC range, and a 0 to 200-volts AC range. Most DMM's sold today meet those minimum specifications.

Let's discuss briefly how you can use a DMM for LAN servicing. Resistance and continuity are probably the most used functions in LAN servicing. Use the ohms function to measure the resistance of cables and terminator resistors, and to locate shorts or opens in cables and connectors. A low-end range of 0 to 200 ohms is important because coaxial cables typically measure less than 5.0 ohms end-to-end, and twisted pair less than 20.0 ohms. To make this type of measurement, first power down the network to avoid affecting LAN operation. Disconnect questionable cables before making measurements.

High-resistance cables can have partially severed wires or bad connectors. Test all terminators (connector bodies containing 50-, 91-, or 100-ohm

resistors) to ensure proper resistance. Use the continuity function to locate shorts and opens in cables and connectors. Audible beeps are especially useful when working in dark or tight places like plenums (dropped ceilings).

The DC function is useful as well. Ethernet LAN's carry 5-volt power and data to the transceivers attached to the backbone cable. Use the DMM to verify that power is present at the transceiver if it does not have a Power Good indicator. You can also use the DC volts function to verify voltages in emergency lights and uninterruptable power supplies (UPS's).

Last but not least, use the AC volts function to measure AC power outlets and noise levels on the LAN cables. It is not uncommon for power problems to cause trouble on a LAN, particularly when the file server or hub computer is affected. Then

the whole network may crash. Just check the outlet voltage with a DMM, and if it is outside the 105 to 125-volt AC operating range of most computers, call an electrician!

Noise problems can be a big headache, especially on LAN's with unshielded twisted-pair (UTP) cable. Noise causes random data errors and, in serious cases, can crash the network. Measure noise with a DMM by connecting it to one end of the cable, making sure the other end is terminated properly. The DMM reading for a good UTP cable can be in the range of 5 millivolts or less. A high reading can uncover unusual faults such as a coil of excess cable or cable routed too close to EMI sources such as fluorescent lighting fixtures. In fact, the author once determined that a 50-foot coil of excess UTP left on top of a light fixture by an installer was causing intermittent problems on a newly installed LAN. The problem drove everyone crazy for months! Using a DMM as a noise meter has limited utility because DMM's measure voltage in the kHz range, not in the 4 to 16-MHz range typical of most networks protocols.

Worse, DMM's don't measure impulse noise, which is especially disruptive to LAN operation. For that type of measurement, we must go to more specialized equipment such as that described in the following sections.

Microtest cable scanner

Microtest was the first company to provide specialized, all-in-one LAN test equipment such as the Microtest Cable Scanner. This handheld instrument contains everything you need to troubleshoot LAN cables, including ohmmeter, noise meter, time domain reflectometer (TDR), Ethernet activity monitor, and cable tracer. Best of all, the Cable Scanner is reasonably priced and readily available. Figure 2 shows the Cable Scanner and several other similar models.

Although optimized for Ethernet LAN's, the Cable Scanner also tests unshielded twisted



FIG. 2—MICROTEST'S HANDHELD LAN TESTERS combine most-needed features in easy-to-use, hand-held packages. Clockwise from upper left are the Cable Scanner, the Ring Scanner, the Pair Scanner, and the Quick Scanner.

pair (UTP), shielded twisted pair (STP), Token Ring, and RS-232 cables with simple adapters. In addition, Microtest offers specialized scanners specifically for testing unique features of other cable.

Key features of the Cable Scanner include resistance and continuity functions, a basic noise meter, and a TDR. The noise meter is a simple AC voltmeter that reads millivolt noise in the 1-kHz range; it has no capability for measuring impulse noise. Due to the shielding nature of coaxial cable, noise problems are less common in Ethernet systems—but

they do happen. The Cable Scanner is adept at sensing 60-Hz power-line noise that often appears in problematic coaxial cable systems.

The TDR function can locate shorts and opens in LAN cables. Operating it is as simple as pushing a button. The device then injects pulses into the cable where they travel until they strike a fault, and subsequently bounce back to the instrument. The Cable Scanner measures the travel time, calculates distance to the fault, and then displays the distance. All you have to do is inspect the cable at that distance and repair the fault.

Remember that for a TDR to work properly, all equipment must be turned off. Otherwise, data on the line could cause false distance readings—not to mention what it would do to on-line computers! You should also know that all TDRs have a blind spot, or dead zone, from where the instrument connects to some distance down the cable. The Cable Scanner cannot detect faults occurring within the first 25 feet of cable. If you suspect a fault in that section, inspect the cable manually, or make another measurement from the other end of the cable.

The Cable Scanner's Ethernet activity monitor is useful for spotting bad transceivers and other cases of network overload. Recall from Part 1 of this series that Ethernet works on a first-come, first-served basis, somewhat like an old-fashioned telephone party line. Whoever speaks first gets the line. Should something go wrong—for example, a transceiver that "jabbers" or talks all the time—traffic could soar to 100% usage. That, in turn, would prevent other computers on the network from exchanging data because their collision sense multiple access (CSMA) circuitry would force them to wait continually. The result is that LAN operation would come to a grinding halt.

The activity monitor counts the number of data packets (messages) sent between computers on the network over a set time period (for example, one second or one minute). Then it calculates percent usage. You then look up that value on a chart to determine whether there are problems. If so, you must troubleshoot to locate the cause of the fault.

The Cable Scanner also has an optional cable tracer that allows you to trace a specific cable as it runs through the building alongside others. This is a handy feature because LAN cables look alike, making it easy to waste time tracing the wrong cable. To operate the cable tracer, you must also purchase a cigarette-pack-size receiver. In operation, the Cable Scanner

sends a special signal over the cable under test. Then you hold the receiver next to each cable in turn; the one that produces a warble tone is the one you want.

Microtest also sells more specialized instruments for testing other kinds of cables. For UTP/STP cables there is the Pair Scanner, which addresses major twisted-pair concerns including impulse noise and signal loss through the cable. The Pair Scanner also has switching capabilities for selecting different transmit/receive pairs, as well as a hub computer test function. For Token Ring cabling there is the Ring Scanner, which isolates faulty multistation access units (MAU's), determines whether the ring maintains continuity, and monitors network traffic. Interestingly, it can simulate network faults, so you can perform "fire drills" on a good LAN and get a feel for symptoms before they occur. All Microtest products provide a serial output for logging data or printing hard copy reports.

Paladin Patch Check

Growing popularity of UTP-based LAN's has created a market for special test tools. One good example is a simple, low-cost cable tester from Paladin Corporation called Patch Check. Patch Check, shown in Fig. 3, identifies the most common faults in UTP systems, namely bad connectors, shorts, and opens.

Patch Check tests the full range of UTP systems, from single- to four-pair cables terminated in RJ-11 or RJ-45 connectors. Operation is simply a matter of snapping both ends of the cable into the unit, pushing the Test button, and watching the indicators. Bad connections or opens appear as one or more unilluminated LED's; shorts appear as multiple simultaneously lit indicators. Paladin also offers a remote indicator for situations where you can't get at both ends of the cable.

Patch Check can save lots of time. For example, in resolving one problem described in Part 3 of this series, the author check-

ed a cable with Patch Check in ten seconds, vs. five minutes on a DMM!



FIG. 3—PALADIN'S PATCH CHECK provides instant go/no-go testing of RJ-11 and RJ-45 telephone-style connectors, used for shielded and unshielded twisted-pair wiring.

Tektronix 1502C TDR

Of all the equipment discussed in these articles, the Tektronix 1502C TDR is oldest and best established. For finding tough problems it can't be beat. It can identify badly crimped connectors, crushed coaxial cables, wiring chewed by rodents, and more. It is sensitive enough to locate problems to within inches on the cable. The 1502C is a state-of-the-art version of a line of analog TDR's that goes back several decades.

The 1502C looks much like a benchtop oscilloscope, as shown in Fig. 4. However, instead of the usual cathode ray tube (CRT), the 1502C has a liquid crystal display (LCD) to reduce power consumption and weight. A removable reticle fits over the display, which shows cable impedance vs. distance. The operating controls are simple, and there are less of them than on an oscilloscope. An excellent operator's manual helps new or infrequent users operate the device.

Key features of the 1502C include a negative-going output pulse, which shuts down live

Ethernet transceivers, and a zoom feature that allows you to examine tiny faults which show up as impedance spikes on the display. Zoom helps you find problems like rusty connectors or bad crimps. In Part III we will show how we found an unauthorized cable tap using these features.

One important feature is the propagation-rate control. It's important because it determines the distance accuracy of the TDR. As you might recall from physics class, electrons travel at the speed of light in a vacuum. But in the real world of copper cabling, signals travel much slower. The speed reduction is due to insulation quality and conductor diameter. The propagation-rate control calibrates the equipment to compensate for the slower conduction in the cable, thereby providing correct distance indications.

RESOURCES

Following are addresses of manufacturers whose products were discussed in this article. Contact them for current pricing and more information.

- Paladin Corporation, 3543 Old Conejo Rd., Newbury Park, CA 92123, (800) 272-8665.
- Jensen Tools, Inc., 7815 S. 46th Street, Phoenix, AZ, 85044, (602) 968-6231.
- MicroTest, Inc., 3519 E. Shea Blvd. Suite 134, Phoenix, AZ 85028, (800) 526-9675.
- *Radio Amateur's Handbook*, American Radio Relay League, Newington, CT 06111.
- Tektronix, Inc., Redmond Division, 625 S. E. Salmon Dr., Redmond, OR 97756, (800) 833-9200.
- AMP, Inc., P.O. Box 3608, Harrisburg, PA 17105, (717) 561-6168.

Typically you set the propagation rate by consulting a chart published by the cable manufacturer or LAN equipment vendor. Values are usually expressed as a percentage of the speed of light, *c*. The higher the percentage, the faster the signals travel through the cable. Typical Ethernet backbone cable has a propagation rate of 0.76*c*. Some sources refer to propagation rate as the numer-



FIG. 4—TEKTRONIX' 1502C TIME DOMAIN REFLECTOMETER provides analog display of distance versus impedance. A knowledgeable technician can interpret the display to locate subtle LAN cable faults.

ical value of propagation (NVP) or velocity factor (VF). The terms all mean the same thing. Regardless of name, it is important to set the propagation rate control of your TDR if you want it to display meaningful, accurate readings.

Operating the 1502C is straightforward. You begin by powering down the LAN equipment on the questionable cable segment and removing any terminator resistors. (Terminators can trick a TDR into displaying fantastic cable lengths.) Then connect the TDR to the cable through an impedance adapter, install the correct display reticle, and apply power. Then adjust the controls, and you'll receive a visual indication of cable quality.

Tektronix makes several other TDRs. The 1503C analog TDR accommodates cables as long as 50,000 feet, and has an Ethernet option. The 1503C looks like a good choice for cable TV or aircraft carrier applications. Tektronix also makes the TMA-802, a moderately priced digital TDR and Ethernet ac-

tivity monitor.

Analog vs. digital

In this article, we have described two types of TDRs: digital (Microtest) and analog (Tektronix). Each type of TDR has its own advantages and disadvantages; both instruments are widely used in LAN servicing.

The major differences between the two are in information display and sensitivity to minor faults. Push a button on a digital TDR, and you'll read something like *Short 40 Ft* on the display. Digital TDRs are great for novice users because they make it easy to understand results. Their drawback, however, is that they report only major faults, missing minor ones that often cause the most frustrating problems.

Turn on an analog TDR and you'll see a oscilloscope-style wavy line over a black reticle calibrated in impedance vs. distance. Clearly the analog TDR is intended for more experienced users who can disregard the dead zone, interpret impedance

changes, and read distance from the reticle. Analog TDRs also have an amazing sensitivity to rusty contacts in connectors, water-logged cables, and other faults that can go undetected with less-sensitive instruments.

Network certification

Another issue is network certification, which is becoming increasingly important as corporations continue the downsizing trend. Downsizing involves using networks of PC's to perform mission-critical applications formerly run on mainframes. *Mission-critical* means that the health and competitiveness of the company depend critically on the computer systems that support the company. Without a reliable network, workers can't do their jobs, so goods and services are delivered to customers late. If customer dissatisfaction increases, the company suffers, and so do jobs. Clearly, we all have a vested interest in keeping our LAN networks running reliably.

In the past, LAN cables were often pulled by electrical or telephone wiring contractors who might not have had proper tools and expertise. As a result, Ethernet cables may exceed recommended lengths, excess UTP cable may be left coiled in plenums over fluorescent fixtures, and so on. Those problems decrease LAN performance and, even worse, can serve to reduce reliability.

In response, major LAN vendors have devised performance tests to help ensure that LANs meet standards for noise level, cable length, attenuation, and other factors that affect performance and robustness.

Without thinking out the problem the fanciest TDR in the world will be useless. Develop your ability to identify a problem and logically work your way through possible causes until it is solved.

Be sure to join us in Part III when we will roll up our sleeves and troubleshoot actual LANs with the equipment and tools described here.

The 555

A Versatile Timer

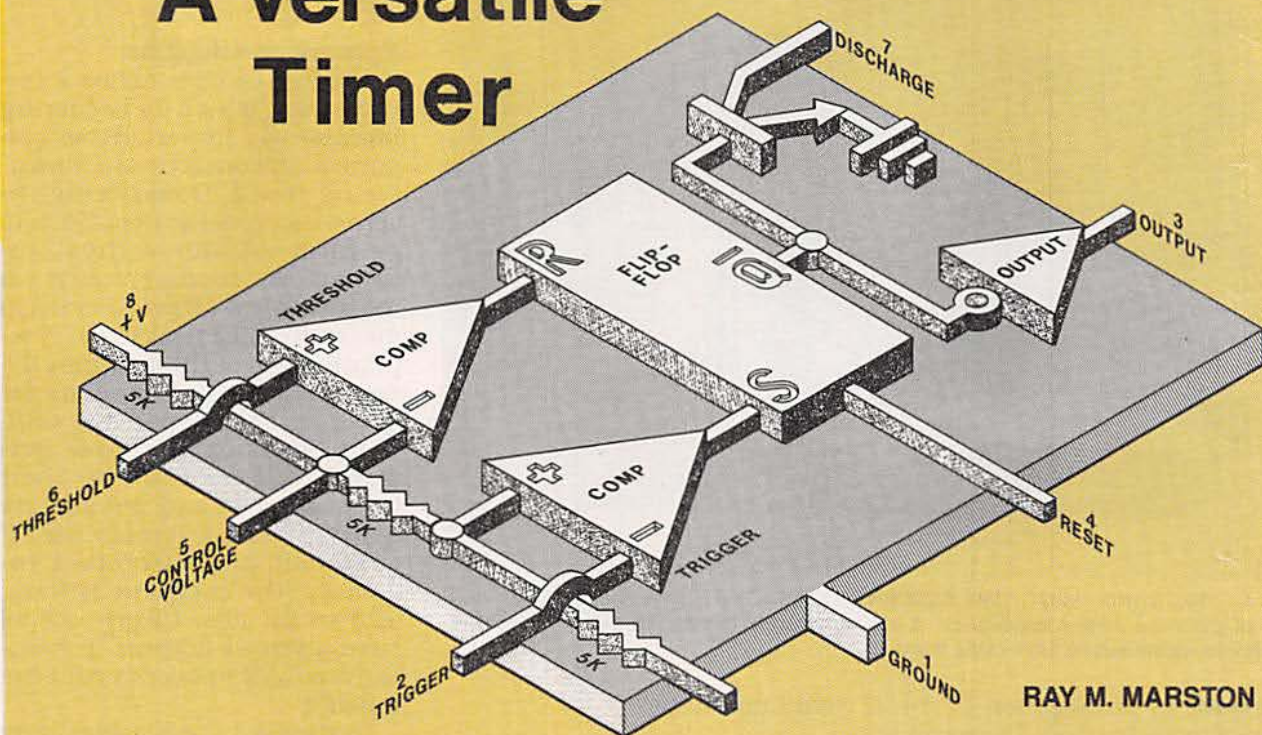


FIG. 1—FUNCTIONAL BLOCKS OF THE 555 TIMER with its pinout identified.

Learn to use the 555 and 556 timer IC in practical circuits to obtain accurate time delays and square waves

IN ANY ASSOCIATION TEST FOR those who know integrated circuits, the three digits 555 will summon up the instant response "timer IC." It's the short form generic designation for progeny of the NE555, a popular monolithic timer/oscillator IC first introduced by Signetics many years ago. Still widely second-sourced because of its versatility, the 555 ranks as a standard "building block."

The 555 and its derivatives can be found in thousands of different circuits, and its possibilities for further applications appear limitless. Although classed as a linear IC, it is often used in digital or "quasi-digital" applications because its inputs and outputs are essentially square waves

rather than sine or other complex waveforms. This article explains how the 555 works and shows you how to apply the IC in various practical control circuits.

A 555/556 overview

Figure 1 is a simplified block diagram of the 555 showing its principal functional blocks: threshold comparator, trigger comparator, R-S flip-flop, low-power complementary output stage, slave discharge transistor, and a voltage-reference potential divider. Both halves of a dual version of the 555 (two 555's on a single chip), the 556, have identical electrical characteristics. The 555/556 will run from 4.5 to 16 volts DC, although a typical

supply will be +12 volts DC or less.

The outstanding features of the 555/556 include:

- Timing adjustable from microseconds to hours
- Duty cycle adjustable
- Ability of output to source (supply) or sink (dissipate) 200-milliampere current
- Output can drive TTL logic circuits
- Temperature stability exceeds 0.005%/°C
- Normally "on" and normally "off" output

The 555 and 556 were designed for precision timing applications, with the timing interval controlled by an external resistor and capacitor (RC) network. The devices contain voltage dividers consisting of

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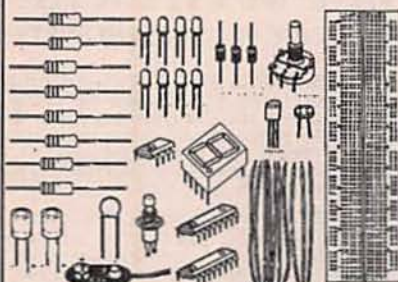


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\$179.⁰⁰

Reg. \$199.⁰⁰
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Microprocessor-based counter measures frequency from 10 Hz to 1.25GHz and period from 0.1µs to 100ms. Includes data hold, min/max/average readings and relative frequency measurements. Complete with 4 AA batteries, manual and 1-year warranty.



\$79.⁹⁵

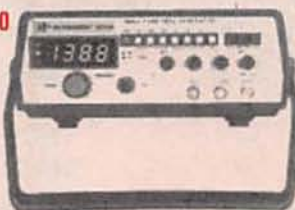
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Tool Kit

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\$55.⁰⁰

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Provides up to 6 on and 6 off settings per week with a minimum switch time as low as 1 minute. Plugs into 3-prong 110VAC outlet and has battery backup (AAA battery incl) to prevent programs from being cleared during power failure. Rated at 15amps. UL listed.



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SERVICE SPECIALIST TOOL KIT

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Panel layout is color-coded to identify functions easily. Sensitivity 1m/div. Complete with probes, operator's manual and 3-year warranty.

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Model ZP200

X10 OSCILLOSCOPE PROBE

200MHz monolithic probe provides superior performance with a risetime of less than 1.5ns and a sharp pulse response. Complete with sprung hook, trimmer tool, 6" ground line, BNC adapter, IC and insulating tip. Cable length is 1.2 meters.



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Model Z615 BK PRECISION HAND-HELD PARTS TESTER

This 2000 count, 3 1/2 digit LCD display meter tests capacitance (20mF), resistance (20MΩ), transistor hFE, SCRs, diodes, LEDs and batteries. Comes with 9V battery, manual, test leads and 1-year warranty.



\$24.⁰⁰

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AUDIBLE CONTINUITY TESTER

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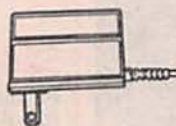
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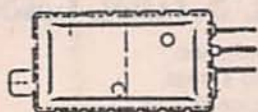
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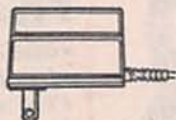
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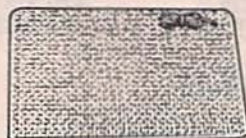


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Display	10 Digit LCD w/Function Annunciators	10 Digit LCD w/Function Annunciators	10 Digit LCD	10 Digit LCD	10 Digit LCD	8 Digit LED	8 Digit LED
RF Signal Strength Indicator	16 Segment Adjustable Bargraph	16 Segment Adjustable Bargraph	16 Segment Adjustable Bargraph
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7413	74159	2.09	74LS330	30	74LS243	.69	25LS2523	2.19	74HC151	59	74HCT194	79	4073	.34			LM748	.79	MC4001	4.00	2N4123	30
7414	74160	.89	74LS326	34	74LS244	.79	81LS996	1.19	74HC153	59	74HCT195	79	4075	.39			LM1014	2.69	MC4018	2.69	2N4124	30
7415	74161	.89	74LS333	40	74LS245	.79	81LS997	1.09	74HC154	1.69	74HCT237	89	4076	.69			LM150K	4.95	MC4024	4.00	2N4129	30
7416	74162	1.09	74LS334	40	74LS247	.89	81LS997	1.69	74HC157	59	74HCT237	89	4077	.38			LM207	5.00	MC4044	5.95	2N4220	1.00
7417	74163	.79	74LS338	40	74LS248	.89	81LS998	1.69	74HC158	59	74HCT240	89	4079	.45			MC1330	1.69	MC4156	1.39	2N4236	1.59
7418	74164	1.89	74LS340	34	74LS249	2.09	81LS998	1.69	74HC161	59	74HCT241	89	4081	.34			MC1349	2.09	MC4741	5.00	2N4240	1.00
7419	74165	5.95	74LS342	45	74LS251	.65	74S00	.39	74HC163	59	74HCT242	99	4082	.34			MC1350	1.29	ICL8038	2.19	2N4385	50
7420	74166	.69	74LS347	89	74LS252	.65	74S00	1.00	74HC164	59	74HCT243	99	4085	.79			LM301	.69	ICL7660	2.25	2N4401	30
7421	74167	.79	74LS348	89	74LS253	.65	74S00	1.00	74HC165	59	74HCT244	99	4086	.34			LM302	.69	MC1374	2.00	7107	8.95
7422	74168	.99	74LS349	89	74LS254	.65	74S00	1.00	74HC166	79	74HCT245	99	4093	.49			LM306	.87	MC1374	2.00	7107	8.95
7423	74169	.99	74LS351	30	74LS255	.65	74S00	1.00	74HC167	79	74HCT251	92	4094	1.39			LM309H	2.95	LM1414	1.69	7207	7.95
7424	74170	.99	74LS354	34	74LS256	.65	74S00	1.00	74HC168	79	74HCT252	92	4094	1.39			LM309K	1.50	MC1456	1.50	7208	20.00
7425	74171	.99	74LS354	34	74LS257	.65	74S00	1.00	74HC169	79	74HCT253	79	4098	1.19			LM310	1.99	MC1458	1.50	7209	20.00
7426	74172	.99	74LS354	34	74LS258	.65	74S00	1.00	74HC170	79	74HCT254	79	4098	1.19			LM312H	5.00	LM1488	65	75108	1.19
7427	74173	.99	74LS354	34	74LS259	.65	74S00	1.00	74HC171	79	74HCT255	79	4098	1.19			LM316	4.00	MC1496	99	75136	1.89
7428	74174	.99	74LS354	34	74LS260	.65	74S00	1.00	74HC172	79	74HCT256	79	4098	1.19			LM317	1.99	MC1500	3.50	75137	1.89
7429	74175	.99	74LS354	34	74LS261	.65	74S00	1.00	74HC173	79	74HCT257	79	4098	1.19			LM318	1.99	MC1500	3.50	75138	1.89
7430	74176	.99	74LS354	34	74LS262	.65	74S00	1.00	74HC174	79	74HCT258	79	4098	1.19			LM319	1.39	MC1500	3.50	75139	1.89
7431	74177	.99	74LS354	34	74LS263	.65	74S00	1.00	74HC175	79	74HCT259	79	4098	1.19			LM322	2.19	MC1500	3.50	75140	1.89
7432	74178	.99	74LS354	34	74LS264	.65	74S00	1.00	74HC176	79	74HCT260	79	4098	1.19			LM323K	3.99	LM1812	95	75365	1.69
7433	74179	.99	74LS354	34	74LS265	.65	74S00	1.00	74HC177	79	74HCT261	79	4098	1.19			LM324	4.95	LM1812	95	75365	1.69
7434	74180	.99	74LS354	34	74LS266	.65	74S00	1.00	74HC178	79	74HCT262	79	4098	1.19			LM325	4.95	LM1812	95	75365	1.69
7435	74181	.99	74LS354	34	74LS267	.65	74S00	1.00	74HC179	79	74HCT263	79	4098	1.19			LM326	4.95	LM1812	95	75365	1.69
7436	74182	.99	74LS354	34	74LS268	.65	74S00	1.00	74HC180	79	74HCT264	79	4098	1.19			LM327	4.95	LM1812	95	75365	1.69
7437	74183	.99	74LS354	34	74LS269	.65	74S00	1.00	74HC181	79	74HCT265	79	4098	1.19			LM328	4.95	LM1812	95	75365	1.69
7438	74184	.99	74LS354	34	74LS270	.65	74S00	1.00	74HC182	79	74HCT266	79	4098	1.19			LM329	4.95	LM1812	95	75365	1.69
7439	74185	.99	74LS354	34	74LS271	.65	74S00	1.00	74HC183	79	74HCT267	79	4098	1.19			LM330	4.95	LM1812	95	75365	1.69
7440	74186	.99	74LS354	34	74LS272	.65	74S00	1.00	74HC184	79	74HCT268	79	4098	1.19			LM331	4.95	LM1812	95	75365	1.69
7441	74187	.99	74LS354	34	74LS273	.65	74S00	1.00	74HC185	79	74HCT269	79	4098	1.19			LM332	4.95	LM1812	95	75365	1.69
7442	74188	.99	74LS354	34	74LS274	.65	74S00	1.00	74HC186	79	74HCT270	79	4098	1.19			LM333	4.95	LM1812	95	75365	1.69
7443	74189	.99	74LS354	34	74LS275	.65	74S00	1.00	74HC187	79	74HCT271	79	4098	1.19			LM334	4.95	LM1812	95	75365	1.69
7444	74190	.99	74LS354	34	74LS276	.65	74S00	1.00	74HC188	79	74HCT272	79	4098	1.19			LM335	4.95	LM1812	95	75365	1.69
7445	74191	.99	74LS354	34	74LS277	.65	74S00	1.00	74HC189	79	74HCT273	79	4098	1.19			LM336	4.95	LM1812	95	75365	1.69
7446	74192	.99	74LS354	34	74LS278	.65	74S00	1.00	74HC190	79	74HCT274	79	4098	1.19			LM337	4.95	LM1812	95	75365	1.69
7447	74193	.99	74LS354	34	74LS279	.65	74S00	1.00	74HC191	79	74HCT275	79	4098	1.19			LM338	4.95	LM1812	95	75365	1.69
7448	74194	.99	74LS354	34	74LS280	.65	74S00	1.00	74HC192	79	74HCT276	79	4098	1.19			LM339	4.95	LM1812	95	75365	1.69
7449	74195	.99	74LS354	34	74LS281	.65	74S00	1.00	74HC193	79	74HCT277	79	4098	1.19			LM340	4.95	LM1812	95	75365	1.69
7450	74196	.99	74LS354	34	74LS282	.65	74S00	1.00	74HC194	79	74HCT278	79	4098	1.19			LM341	4.95	LM1812	95		

RAMSEY ELECTRONICS



COM-3
\$2795.00

2 WAY RADIO SERVICE MONITOR

COM-3, the world's most popular low-cost service monitor. For shops big or small, the COM-3 delivers advanced capabilities for a fantastic price—and our new lease program allows you to own a COM-3 for less than \$3.00 a day. Features: ▶ Direct entry keyboard, with programmable memory ▶ Audio & transmitter frequency counter ▶ LED bar graph frequency deviation display ▶ 0.1-10,000 µV output levels ▶ High receive sensitivity, less than 5 µV ▶ 100 kHz to 999.9995 MHz ▶ Continuous frequency coverage ▶ Transient protection, up to 100 watts ▶ CTS tone encoder, 1 kHz and external modulation.



RSG-10
\$2495.00

SYNTHESIZED SIGNAL GENERATOR

Finally, a low-cost lab quality signal generator—a true alternative to the \$7,000 generators. The RSG-10 is a hard working, but easy to use generator ideal for the lab as well as for production test. Lease it for less than \$3.00 a day. Features: ▶ 100 kHz to 999 MHz ▶ 100 Hz resolution to 500 MHz, 200 Hz above ▶ -130 to +10 dBm output range ▶ 0.1 dB output resolution ▶ AM and FM modulation ▶ 20 programmable memories ▶ Output selection in volts, dB, dBm with instant conversion between units ▶ RF output reverse power protected ▶ LED display of all parameters—no analog guesswork!

• 2 METERS
• 223 MHz
• 440 MHz

FANTASTIC FM TRANSCEIVERS

SYNTHESIZED—NO CRYSTALS

Ramsey breaks the price barrier on FM rigs! The FX is ideal for shack, portable or mobile. The wide frequency coverage and programmable repeater splits makes the FX the perfect rig for Amateur, CAP or MARS applications. Packeteers really appreciate the dedicated packet port. "TRUE-FM" signal and almost instant T/R switching. High speed packet? No problem. Twelve diode programmed channels, 5W RF output, sensitive dual conversion receiver and proven EASY assembly. Why pay more for a used foreign rig when you can have one AMERICAN MADE (by you) for less. Comes complete less case and speaker mike. Order our matching case and knob set for that pro look.



\$149.95

FX-146 kit (2 Meters) \$149.95
FX-223 kit (1 1/2 Meters) \$149.95
FX-440 kit (3 1/2 Meters) \$169.95
CPX matching case set \$ 24.95

FREQUENCY COUNTERS

CT-70 7 DIGIT 525 MHz

CT-90 9 DIGIT 600 MHz

CT-125 9 DIGIT 1.2 GHz



Ramsey Electronics has been manufacturing electronic test gear for over 10 years and is recognized for its lab quality products at breakthrough prices. All of our counters carry a full one-year warranty on parts and labor. We take great pride in being the largest manufacturer of low-cost counters in the entire U.S.A. Compare specifications. Our counters are full-featured, from audio to UHF, with FET high impedance input, proper wave shaping circuitry, and durable high quality epoxy glass plated thru PC board construction. All units are 100% manufactured in the U.S.A. All counters feature 1.0 ppm accuracy.

NEW CT-250 2.5 GHz

ACCESSORIES FOR COUNTERS

Telescopic whip antenna—BNC plug, WA-10 \$11.95
High impedance probe, light loading, HP-1 \$16.95
Low-pass probe, audio use, LP-1 \$16.95
Direct probe, general purpose use, DC-1 \$16.95
Tilt bail, elevates counter for easy viewing, TB-70 \$9.95
Rechargeable internal battery pack, BP-4 \$8.95
CT-90 oven liresed, 0.1 ppm accuracy, OV-1 \$8.95

ALL COUNTERS ARE FULLY WIREB & TESTED

MODEL	FREQ. RANGE	SENSITIVITY	DIGITS	RESOLUTION	PRICE
CT-50	20 Hz-600 MHz	< 25 mV to 500 MHz	8	1 Hz, 10 Hz	\$189.95
CT-70	20 Hz-550 MHz	< 50 mV to 150 MHz	7	1 Hz, 10 Hz, 100 Hz	\$139.95
CT-90	10 Hz-600 MHz	< 10 mV to 150 MHz < 150 mV to 600 MHz	9	0.1 Hz, 10 Hz, 100 Hz	\$169.95
CT-125	10 Hz-1.25 GHz	< 25mV to 50 MHz < 15 mV to 500 MHz < 100 mV to 1 GHz	9	0.1 Hz, 1 Hz, 10 Hz	\$189.95
CT-250	10 Hz-2.5 GHz typically 3.0 GHz	< 25 mV to 50 MHz < 10 mV to 1 GHz < 50 mV to 2.5 GHz	9	0.1 Hz, 1 Hz, 10 Hz	\$249.95
PS10B Prescaler	10 MHz-1.5 GHz, divide by 1000	< 50 mV	Convert your existing counter to 1.5 GHz		\$69.95

SPEED RADAR \$89.95 complete kit SG-7

New low-cost microwave Doppler radar kit "blows" cars, planes, boats, bikes or anything else moving object. Operates at 2.6 GHz using up to 1/4 mile range LED optical readout displays speed in miles per hour. Kilometers per hour or feet per second. Electronic output allows for fastening to actual doppler shift. Uses two 1-1/2 cell cans for antenna (not included) and runs on 12 VDC. Easy to build—all microwave circuitry is PC stripline. ABS plastic case with speedy graphics for a professional look. A very useful and full-of-fun kit.

BROADBAND PREAMP

Boost those weak signals to your scanner, TV, shortwave radio or frequency counter. Flat 25 dB gain, 1 to 1000 MHz, 3 dB NF, BNC connectors. Runs on 12 VDC or 310 VAC. FR-2, wired, includes AC adapter. \$59.95

FM WIRELESS MIKE KITS

Pick the unit that's right for you. All units transmit stable signal in 88-108 MHz FM band up to 300' except for hi power FM-4 that goes up to 1/2 mile. FM-1, basic unit \$ 5.95
FM-2, as above but with added mike preamp \$ 7.95
FM-4, long range, high power with very sensitive audio section, picks up voices 10' away \$14.95

MC-1, miniature sensitive mike cartridge for FM-1, 2, 4 \$ 2.95

2M POWER AMP

Easy to build power amp has 8 times power gain, 1W in, 8W out, 2W in, 16W out, 5W is for 40W out. Same amp as featured in many ham magazine articles. Complete with all parts, less case and T-R relay. PA-1, 40W pwr amp kit \$34.95
TR-1, RF switched T-R relay kit \$11.95

PACKET RADIO

Two new versions are available for the Commodore 64 (P-64A) or the IBM-PC (P-IBM). Easy assembly "NO TUNING". Includes FREE disk software, PC Board and Full Documentation.
KIT P-64A \$59.95
P-IBM \$58.95
CASE CPK \$12.95

LO NOISE PREAMPS

Make that receiver come ALIVE! Small size for easy installation with Hi-Q tuned input for peak performance. Excellent gain and noise figure—guaranteed to improve reception! Specify band: 2M—PR-10, 220 MHz—PR-20, 440 MHz—PR-40. Each kit \$17.95

MICROWAVE INTRUSION ALARM

A real microwave Doppler sensor that will detect a human as far as 10 feet away. Operates on 1.3 GHz, and is not affected by heat, light, or vibrations. Drives up to 100 mA output, normally open or closed, runs on 12 VDC. Complete kit MD-3 \$19.95

MUSIC MACHINE

Next kit that will produce 25 different classical and popular tunes, plus 3 disc tone sounds. Lots of fun for doorbells, shop, or store entrance, car horn, music boxes, etc. Runs on 9V battery or will transform. Excellent speaker volume and adjustable tempo and pitch. Add our case set for a handsome finished look. Complete kit, MM-5 \$24.95
Case + knob set, CMM-5 \$12.95

PHONE TRANSMITTER

Mini-sized with professional performance. Self-powered from phone line, transmits in FM broadcast band up to 1/2 mile. Installable easily anywhere on phone line or inside phone. PB-1 kit \$14.95

LO NOISE PREAMPS

Make that receiver come ALIVE! Small size for easy installation with Hi-Q tuned input for peak performance. Excellent gain and noise figure—guaranteed to improve reception! Specify band: 2M—PR-10, 220 MHz—PR-20, 440 MHz—PR-40. Each kit \$17.95

TICKLE STIK

A shocking kit! Blinking LED attracts insects to pick up insect-looking can! You watch the fun! Ideal for office desks, parties, noisy know-it-alls. TS-4 kit \$9.95

VOICE ACTIVATED SWITCH

Voice activated switch kit provides switched output with current capability up to 100 mA. Can drive relays, lights, LED, or even a tape recorder motor. Runs on 9 VDC. VS-1 kit \$6.95

FM RADIO

Full-featured superhet, crystal-tuned sensitivity, IC detector and 10.7 MHz IF. Tuned Sid. FM broadcast band as well as large portions on each end. Ideal for "bug" receiver, hobby experiments or even as FM radio! FR-1 kit \$19.95

SUPER SLEUTH

A super sensitive amplifier which will pick up a pin drop at 15 feet! Great for monitoring baby's room or as general purpose amplifier. Full 2W rms output. Runs on 6 to 15 volts, uses 6-45 ohm speaker. BN-9 kit \$6.95

2 MTR & 220 BOOSTER AMP

Here's a great booster for any 2 meter or 220 MHz hand-held unit. These power boosters deliver over 30 watts of output, allowing you to hit the repeater's full cutting while the low noise preamp remarkably improves reception. Ramsey Electronics has sold thousands of 2 meter amp kits, but now we offer completely wired and tested 2 meter, as well as 220 MHz, units. Both have all the features of the high-priced booster as a fraction of the cost.
PA-10 2 MTR POWER BOOSTER (10 X power gain) Fully wired & tested \$69.95
PA-20 220 MHz POWER BOOSTER (8 X power gain) Fully wired & tested \$69.95



QRP TRANSMITTERS HAM RECEIVERS

20, 30, 40, 80M CW TRANSMITTERS

Join the fun on QRP! Thousands of these mini-rigs have been sold and lots of DX contacts have been made. Imagine working Eastern Europe with a 200 watt rig—that's ham radio at its best! These CW rigs are ideal mates to the receivers at right. They have two-position variable crystal control (one popular QRP XTAL included), one watt output and built-in antenna switch, Run/Stand 12VDC. Add our matching case and knob set for a handsome finished look. Your choice of bands: (Specify band: QRP-20, 30, 40 or 80) \$29.95
Matching case & knob set, CQRP \$12.95

20, 30, 40, 80M All Mode RECEIVERS

Build your own mini ham station. Sensitive all-mode AM, CW, SSB receivers use direct conversion design with N5COC IC as featured in QST and ARRL handbooks. Vary sensitive varactor tuned over entire band. Plenty of speaker volume. Runs on 9V battery. Very EASY to build, lots of fun and educational—ideal for beginner or old pro. New 30-page manual. Add the case set for well-fitted professional look. Your choice of bands: (Specify band: HR-20, HR-30, HR-40, HR-80) \$29.95
Matching case & knob set, CHR \$12.95

E-Z KEY CMOS KEYS

Send perfect CW within an hour of receiving this kit. Easy-to-build kit has sidetone oscillator, speed control and keys most any transmitter. Runs for months on a 9V battery. 28-page manual gives ideas on making your own key for extra savings. Add our matching case set for complete station look. CW-7 kit \$24.95
Matching case knob set, CCW \$12.95

2, 6, 10 MTR, 220 FM RECEIVERS

Keep an ear on the local repeater gang, monitor the cops, check out the weather or just plain listen around. These sensitive superhet receivers are just the ticket! They tune any 5 MHz portion of the band and have smooth varactor tuning, dual conversion with ceramic IF filters, AFC, adjustable squelch and plenty of speaker volume. Runs on 9V battery and performance that rivals the big rig! For a complete finished pro look, add our matching case and knob set with screened graphics. FM communications receiver kit \$29.95
Specify band: FR 146 (2m), FR6 (6m), FR10 (10m), FR-220 (220 MHz) \$12.95
Matching case & knob set, CFR \$12.95

ACTIVE ANTENNA

Cramped for space? Get longwire performance with this desktop antenna. Properly designed unit has dual HF and VHF circuitry and built-in whip antenna, as well as external jack, RF gain control and 9V operation makes unit ideal for SWLs, traveling hams or scanner buffs who need better reception. The matching case and knob set gives the unit a hundred dollar look! AA-7 Kit \$24.95
Matching case & knob set, CAA \$12.95

SPEECH SCRAMBLER

Communicate in total privacy over phone or radio. Kit features full duplex operation using frequency inversion. Both mike and speaker or line in/out connections. Easy hookup to any radio, and telephone use requires no direct connection! Easy to build 2 IC circuit. Can also be used to descramble many 2-way radio signals. Finish your kit off with the handsome case & knob set. SS-7 kit \$29.95
Matching case & knob set, CSS \$12.95

SHORTWAVE RECEIVER

Fantastic receiver that captures the world with just a 12" antenna! Can receive any 2 MHz portion from 4-11 MHz. True superhet has smooth varactor tuning, AGC, RF gain control, plenty of speaker volume and runs on a 9V battery. Fascinating Scout, school or club project provides hours of fun for even the most serious DXer. For the car, consider our shortwave converter. Two switchable bands (in 3-22 MHz range), each 1 MHz wide—tunable on your car radio dial. Add some interest to your drive home! Shortwave receiver kit, SRI \$29.95
Shortwave converter kit, SCV \$27.95
Matching case set for SRI, CSR \$12.95
Matching case set for SCV, CSR \$12.95

FM STEREO TRANSMITTER

Run your own stereo FM station! Transmit a stable signal in the standard FM broadcast band throughout the house, dorm or neighborhood. Connects easily to line outputs on CD player, tape decks, etc. Runs on 9V battery, has internal whip antenna and external antenna jack. Add our case set for a "station" look! FM-10 kit \$29.95
Matching case set, CFM \$12.95

AIRCRAFT RCVR

Hear exciting aircraft communications—pick up planes up to 100 miles away! Receives 110-136 MHz AM air band, smooth varactor tuning superhet with AGC, ceramic filter, adjustable squelch, excellent sensitivity and lots of speaker volume. Runs on 9V battery. Great for air shows or just hanging around the airport! New 30-page manual details pilot talk, too. Add case set for "pro" look. AP-1 kit \$24.95
Matching case set, CAR \$12.95

NEW

SPEAKER PHONE

Talk on the phone hands-free, great to put in shop or shack, press the button to answer—no actual phone needed. Works same as commercial units. Talk from anywhere in room, phone line powered—no battery needed. Super for hands-free intercom! Add our case set for a pro look. SP-1 \$29.95 Case-CSP \$12.95

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FAX 716-924-4555

RAMSEY ELECTRONICS, INC. 793 Canning Parkway, Victor, NY 14564

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XL - 103

550 MHZ - 86 Channel **\$89.95** each

TOP CHANNEL ROLLOVER,
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OPTIONAL

\$70.00 each - 5 Lot

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\$50.00 each - 100 Lot

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MXC-2520-525 MHZ remote volume
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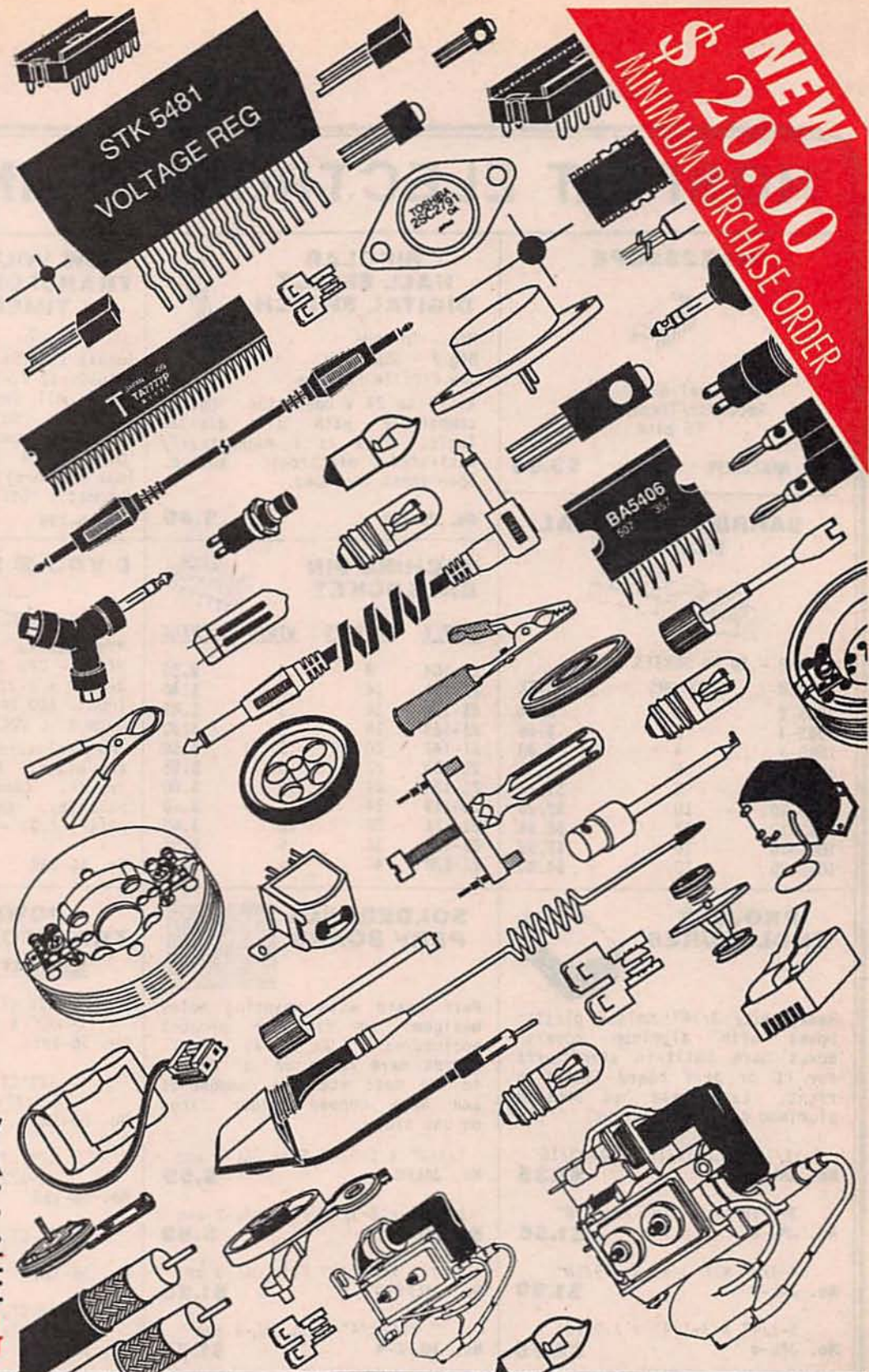
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MAX232CPE



Dual RS232
Receiver/Transmitter
16 pins

No. MAX232CPE **\$3.95**

BARRIER TERMINAL BLOCKS



10 AMP - 10 BS SERIES

NUMBER	SECTIONS	PRICE
10BS-2	2	\$.44
10BS-3	3	\$.66
10BS-4	4	\$.88
10BS-6	6	\$ 1.36
10BS-8	8	\$ 1.76
10BS-10	10	\$ 2.20
10BS-12	12	\$ 2.64
10BS-16	16	\$ 2.99
10BS-20	20	\$ 4.40

BIPOLAR HALL EFFECT DIGITAL SWITCH



Mfg - Sprague
Mfg # - UGN3030U
Low Profile Package

4.5 V to 24 V operation. Output compatible with all digital logic. This is a magnetically activated electronic switch. Spec sheet included.

No. 25-137 **\$.49**

LOW VOLTAGE TRANSFORMER TIMER



Input: 115/125 V, 60 Hz
Output: 12 V, 60 Hz, 72 VA (6 A)
Photo cell sensing 3 mode: Full automatic 'On' at dusk, 'Off' at dawn; Automatic 'On' at dusk, 'Off' at a predetermined time (max 12 hrs); Manual 'On' and automatic 'Off' at dawn.

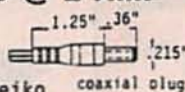
No. 56-199 **\$18.95**

MACHINE PIN DIP SOCKET



PART #	# PINS	WIDTH	PRICE
21-104	8	.3	\$.35
21-131	14	.3	\$.40
21-118	16	.3	\$.45
21-123	18	.3	\$.50
21-142	20	.3	\$.50
21-103	22	.4	\$.55
21-124	24	.3	\$.60
21-119	24	.6	\$.60
21-121	28	.6	\$.65
21-192	32	.6	\$.95
21-120	40	.6	\$.75

6 VDC @ 2 AMP



Mfg - Seiko
Mfg # - DPU-411-01
3-3/8" x 2-3/8"
Input: 120 VAC 60 Hz 30 W
Output: 6 VDC @ 2 amps

The enclosure and the 6 ft. wire are black. The wire has a white tracer. Center is negative for polarity. Coaxial plug: O.D. - .215", I.D. - .079".

No. 56-185 **\$7.95**

PROJECT ENCLOSURES



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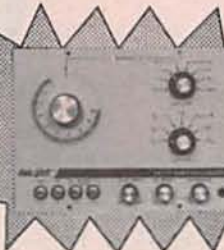
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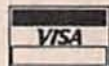
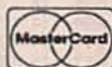
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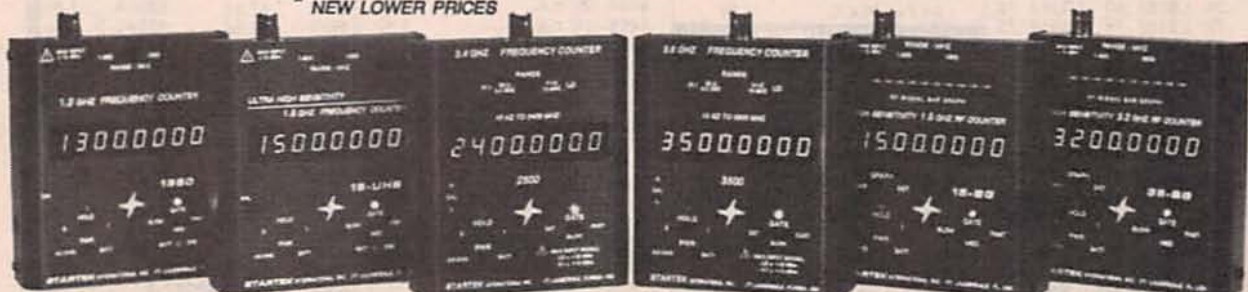
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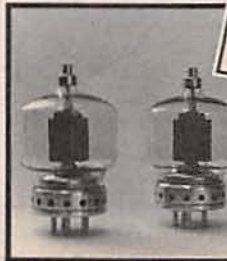
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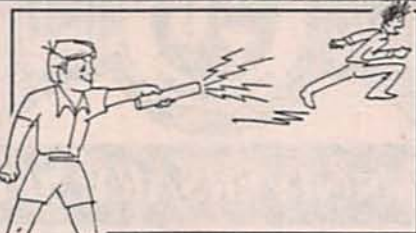
THE LARGEST ELECTRON TUBE INVENTORY IN THE WORLD

AMAZING * ELECTRONIC PRODUCTS and KITS

NEW CONCEPT! Mystery Levitating Device



Remember War of the Worlds? Objects float in air and move to the touch. Defies gravity, amazing gift, conversation piece, magic trick or great science project. ANT1K Easy to Assemble Kit / Plans \$19.50



NEW!
Amazing GlowTron!
Projects visible energy. Operates on safe, low voltage to produce spectacular lighting effects. Neon & fluorescents glow without wires! GTRON Ready to Use \$29.50

Combination Solid State Tesla Coil & Variable 100,000VDC Generator



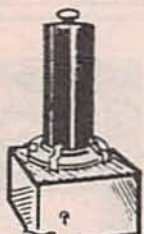
Experiments Using Tesla Coil:
• Plasma in a Jar/Tornado, Furnace
• Kirlian Photography
• Wireless Energy Transmission
• Induction Fields • Pyrotechnic Effects
• Corona and Brush Discharge
• Energizer for Neon Plasma Tubes

Experiments Using Hi Volts DC:
• Plasma Blaster Driller/Cutter
• Anti-Gravity/Force Fields
• Ion Reaction Motors
• Lightning Generation
• High Ion Source
• Ozone For Air Purification
• Electrification of People & Objects
• Particle Accelerators/Atom Smashing
• High Energy Capacity Charging

HVM7 Plans Complete System \$15.00
HVM7K Complete System Kit/Plans \$174.50
TCL4K Tesla Coil Only Kit/Plans \$99.50
115/19AC Wall Adapter for 115AC \$15.50

Table Top Tesla Coil

Spectacular - A Real Attention Getter!
• 250,000 Volts! • 7-10" Sparks!
Energy even passes through windows. Great for science projects, displays, advertising.



Highly spectacular devices produces visible, audible bolts of lightning appearing to flash in the air. Causes certain materials to burn from within and glow, lights bulbs without wires, produces induction fields, St Elmo's fire corona. Clearly demonstrates high frequency high voltages yet terminal may be touched by user during operation with a metal object. 115VAC operation only.
BTC3 Plans .. \$15.00 BTC3K Kit/Plans \$299.50
BTC30 Assembled and Tested \$399.50

Plasma Fire Saber

Produces the spectacular effect that captured the fantasy of millions of movie fans. Visible plasma field is controlled by grip pressure and adjusts saber length. Active energy field produces weird & bizarre effects. Excellent for special effects. Specify photon blue, neon red, phasor green, or starfire purple.
PFS2 Plans \$8.00 PFS2K Kit/Plans \$49.50
Special Offer PFS20 Assembled reg \$89⁹⁹, \$59.50

Solar Power Devices

Build a fence shocker, solar motor, light, bug zapper, bait charger, etc. SOL1 4", 2 Amp Cell w/Plans .. \$8.50
SOL2 6x12", 14 V Cell w/Plans \$7.50

Shocker Force Field / Vehicle Electrifier

Neat little device allows you to make hand and shock balls, shock wands and electrify objects, charge capacitors. Great pay back for those wise guys who have wronged you!
SHK1KM Easy To Assemble Electronic Kit . \$24.50

100,000V Intimidator / Shock Wand Module

Build an electrical device that is affective up to 20 feet. May be enclosed for handheld, portable field or laboratory applications.
ITM2KM Easy to Assemble Electronic Kit ... \$49.50
ITM2 Plans Only; Credit-able to Kit \$10.00

Ion Ray Gun

Projects charged ions that induce shocks in people & objects without any connection! Great science project as well as a high tech party prank.

IOG3 Plans \$10.00 IOG3K Kit/Plans \$69.50

Invisible Pain Field Generator

Shirt pocket size electronic device produces time variant complex shock waves of intense directional acoustic energy capable of warding off aggressive animals, etc.
IPG7 Plans \$8.00 IPG7K Kit / Plans \$49.50
IPG70 Assembled \$74.50

Homing / Tracking Transmitter

Beeper device, 3 mile range.
HOD1 Plans \$10.00 HOD1K Kit/Plans \$49.50

Listen Thru Walls, Floors

Highly sensitive stethoscope mike.
STETH1 Plans ... \$8.00 STETH1K Kit/Plans \$44.50

3 Mile FM Wireless Mike

Crystal clear, ultra-sensitive pickup transmits voices and sounds to FM radio. Excellent security system, warns of intrusion. Become your neighborhood disk jockey! Monitor children and invalids.
FMV1 Plans \$7.00 FMV1K Kit/Plans . \$39.50

Telephone Transmitter - 3 Miles!

Automatically transmits both sides of a telephone conversation to an FM radio. • Tunable Frequency
• Undetectable on Phone • Easy to Build & Use
• Up to 3 Mile Range • Only transmits during phone use
VWPM7 Plans \$7.00 VWPM7K Kit/Plans \$39.50

ElectroMagnetic Coil Gun

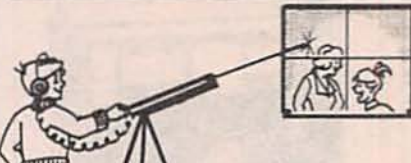
Projects a metal object over a considerable distance. Become part of and perhaps contribute to this exciting new concept of weaponry.
EML2 Plans \$8.00 EML2K Kit/Plans \$39.50



TV & FM Joker / Jammer - Shirt pocket device allows you to totally control and remotely disrupt TV or radio reception. Great gag to play on family or friends. Discretion required.
EJK1KM Easy to Assemble Electronic Kit . \$19.50

Visible Beam Laser

High brightness red HeNe laser visible for miles. Produce your own light show! Projects a beam or red lite clearly visible under most circumstances. Can be used to intimidate by projection of a red dot on target subject. Also may be used to "listen in" utilizing our laser window bounce method #LLIS1 below. Easy to Build Modules Produce A Working Visible Laser:
LAS1KM Kit w/1mw Laser Tube, Class II . \$69.50
LAS3KM Kit w/2.5mw Laser Tube, Class IIIA \$99.50



"Laser Bounce" Listener System

allows you to hear sounds from an area via a lite beam reflected from a window or other similar object. System uses our ready-to-use LATR1 Laser Terminator gun site as the transmitter. The receiver section is supplied as an easy-to-build kit, including our cushioned HS10 headsets. Order # LLIS20 System, includes our LATR1 Ready-to-Use Laser Gun Site, LLR1K Special Receiver Kit, and HS10 Headset, all for only \$299.50

5mw Visible Red Pocket Laser

Utilizes our touch power control!
VRL3KMX Kit / Plans \$119.50

See In The Dark Viewing

Device uses invisible infrared illumination for seeing in total darkness. Excellent for low cost night vision, along with observing lasers and other IR sources. Functional unit, many useful applications.
SD5 Plans \$10.00
SD5K Kit / Tube / Plans \$299.50
GPV10 Ready to Use Viewer \$499.50
6032A Tube / Plans to build your own ... \$99.50



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LIMITED TIME SPECIALS! ORDER TODAY!

Items stamped with this seal are compatible with X-10 Powerhouse, Leviton Decora Electronic Controls, Radio Shack Plug-n-Power, Sears Home Control, Stanley Lightmaker, GE Homeinuder, and most powerline carrier remote control systems.

HOME CONTROL CONCEPTS

Buy with confidence from HCC

- LOWEST PRICES GUARANTEED!
- DOUBLE MANUFACTURER'S WARRANTY!
- TECHNICAL SUPPORT SECOND TO NONE!
- IMMEDIATE SHIPPING!

Free Home Automation Mug

Get this exclusive gift with your order of \$149 or more! Great for drinking freshly brewed coffee from your module-controlled coffee maker. Order HCC-711M

Free Home Automation T-Shirt

Get this great gift with every order \$199 or more! Limited edition, available in S, M, L, XL. Order number HCC-711S.

Brand New! One-For-All 12 Lets You Control X10 and Infrared from one remote!

Universal Electronics has just unleashed their newest model remote control, the One-For-All 12. Billed as the most powerful universal remote in the world, the One-For-All 12 replaces 12 of your existing remotes for TVs, VCRs, Cable Boxes, CDs, Audio Products, Satellite Receivers and more! It can even control X10 modules!

The One-For-All 12 has a 32K memory which contains the world's largest library of infrared codes! In fact, the manufacturer is so confident that your component's infrared codes are contained in the One-For-All 12's memory that they're offering a **DOUBLE YOUR MONEY BACK GUARANTEE!** (call HCC Customer Service or Universal Electronics for further details)

Check out these great features:
Provides any device with a Sleep Timer function * Simple set-up * One Button System Control * Perfect replacement for lost or broken remotes * Toll-Free Consumer Help Line * Upgradable (by manufacturer, no charge) to match the latest advancements in IR remote control technology... won't become obsolete!

Built-in macros mean you can turn on a number of IR devices with the touch of one button! Complex

audio or video systems can be powered up with the touch of a single key! Saves time & convenience!

X10 Compatible! Combine with the HCC-3000 One-For-All Command Center for control of your home entertainment devices AND X10 devices! Just aim the remote at the HCC-3000 for instant control of your home's lights and appliances!



Attention PC hackers! The One-For-All 12 is even PC compatible with the addition of the HCC-PCIR PC to Infrared Interface! (see description lower right)

One-For-All 12 Universal Remote Control HCC-RC5 ONLY \$79.95!

One-For-All Infrared Command Center HCC-3000 ONLY \$29.95!

New! Supervised Wireless Security System

Installs in minutes - with no tools - and no wiring! URC8000 Console keeps track of 16 zones and displays status of each using LEDs. Because it's supervised you'll know if any door/window sensor is not working or has low battery. Add wireless door/window sensors to protect up to 16 different groups of doors and/or windows.

Add a motion detector to protect an area with more than one entry point. Console sounds loud 85 dB alarm and sends X-10 signals to flash all X-10 lights! Scares intruder and makes home visible to others (neighbors, police enroute, etc).

BONUS! Free HCC-574! When you order an HCC-8000 and One-For-All remote control!

Built-in infrared command center (see HCC-3000, above) for use with One-For-All remote! Console is also a receiver for the Stanley hand-held Mobile Control and the X-10 hand-held remote for controlling 16 X-10 devices!

Expand your system anytime by adding door/window sensors, motion detectors, or a plug-in Powerhorn siren!

- HCC-8000 Security Console ONLY \$69!
- HCC-574 Keychain alarm/disarm ONLY \$21.25
- HCC-534 Door/window Sensor ONLY \$14.00
- HCC-508 Powerhorn 110 DB Siren ONLY \$39.95
- HCC-554 Wireless Motion Detector ONLY \$49.95

Lamp Module

Stanley plug-in lamp module controls incandescent lights up to 300 Watt max. Off-white color. Only 650 modules reserved for this promo. Limit 16. HCC-2474. ONLY \$8.99

Mobile Control & Base

Stanley 8-button hand-held remote done in sleek 1990's styling. Transmits RF signal up to 100 ft. to plug-in base transceiver. Off-white color. HCC-2553. ONLY \$37.49
HCC-2554 Additional Mobile Control ONLY \$16.99

Stanley Home Control

Turns on/off up to eight X10 lights and appliances. Has illuminated ALL LIGHTS ON button. Also has DIM/BRIGHTEN and ALL UNITS OFF buttons. Off-white color. ONLY \$8.99
Limit 16. HCC-2551.

Motion Detector & Floods

Detects motion, turns on floodlights, and sends up to four X-10 ON signals to modules located inside or outside the house. OFF delay (10 sec. to 35 min.), dusk/dawn and sensitivity adjustments. Detects 40 ft. at 110° arc. Weatherproof. Bulbs not incl. By Stanley. Limit 12. HCC-2651. ONLY \$39.99

Heath Zenith Motion Switch

Senses motion & turns on light. Adjustable delay shut off. Great for hallways, basements, garages, laundry rooms, bathrooms, more. Photocell adjusts for night-only operation. HCC-6105. ONLY \$14.95

Wall Switch Module

Replaces existing wall switch. Controls incandescent lights up to 500 Watt max. Ivory color button. Only 830 modules reserved for this promo. So order now! By Stanley. Limit 16. HCC-2475. ONLY \$9.99
HCC-2476 3-Way Switch Set (pair) ONLY \$12.99

New Edition! Automation Book

"How to Automate Your Home" by David Gaddis. Excellent! Reviews in Popular Science & Radio Electronics, Circuit Cellar INK, & Electronic House. This superb book is now in its 2nd edition, expanded and improved! 150 pages and over 125 illustrations. Recommended Reg. \$29.95. ONLY \$26.95

Stanley Premier Home Control

Same features as Home Control (below); controls 16 devices. Handsome simulated woodgrain design with smoked flip-up keyboard dust cover. HCC-2549. ONLY \$17.49

X-10 Development Kit

Use to develop your own PC-based "smart" home automation system! Monitor status of home's lights & appliances and make intelligent decisions based on their on/off status. Develop a home control system with IF-THEN logic, even 1-button macros! Add Stanley motion detectors to give system input of room presence. Development software is interrupt based (does not use polling!) and includes compiled library routines and sample C-language source code.

Use with PC to Infrared Interface to develop a system which combines home automation and IR control; any X-10 controller can control infrared! With addition of Voice Master Key, voice control of the home becomes possible. Use X-10's Sundowner to give dusk/dawn input to your system. Add voice PC voice mail card for remote call-in control of X-10!

Requires IBM or compatible computer with parallel port. Includes TW523 module, adapter, interface cable, development software, demo program & technical info/data. HCC-523K ONLY \$69!

PC to Infrared Interface

Great for development of your own infrared home control system! Allows your PC to "push buttons" on remote control! Combine PC based home automation with infrared control of your TV (volume, channel, etc), stereo, VCR, and more! Add whole-house IR repeater such as X-10's Powermid. Use with Covox Voice Master Key for voice control of your entertainment system! Combine with X-10 Development Kit to allow any X-10 controller to control your infrared devices! Use with voice mail system for remote control of IR from any telephone. Possibilities are limitless!

Remote control links to PC's serial port. Use the SendIR program to transmit infrared signals (e.g. The dos command SendIR TV MUTE will mute the tv). Call SendIR from DOS batch files, your existing software program, or develop a program from scratch using sample source code. Complete with interface, cable, development software, sample C-language source code, technical info/data and documentation. Requires One-For-All or T-Control remote control and IBM or compatible computer with serial port. HCC-PCIR ONLY \$69!

Keychain control of anything!

Manufactured by Linear, this low cost RF link is ideal for wireless control of your own projects, your home and car alarm, car doorlocks, and even X-10 modules (with addition of HCC-284 X-10 Powerflash Module)! Set security code on transmitter and receiver, apply power to receiver board, and you're ready for wireless control!

TRANSMITTER: Tiny keychain transmitter is approx. half the height of a matchbox! Transmitter has two buttons corresponding to channels 1 and 2. Includes two Lithium batteries. Up to 100' range.

RECEIVER: Board level receiver measures approx 3" square! Requires power supply of 8 to 24 VDC or 12 to 18 VAC. Two outputs (channels 1 and 2) can each switch up to 300mA @ 18 VDC maximum to ground. Directly activate relays, drive bulbs, more.

HCC-RF1 RF Link set includes transmitter, receiver, documentation. ONLY \$39.99!
HCC-RFX Extra transmitter ONLY \$19.99!

HCC-284 Powerflash Module for X10 control. \$19.99

HACKER'S BONUS: Get a FREE extra transmitter with HCC-RF1 and total HCC purchase over \$249! Order number HCC-711R.

Decora Electronic Controls

Professional quality, X-10 compatible switches, receptacles, controllers, filters, signal bridges and test equipment by Leviton. Improved new design and styling; switches look IDENTICAL to Decora wide rocker switches, LED indicates ON/OFF status. In white, ivory and brown. PRICED BELOW TRADE (contractor/builder/electrician pricing)!

6291 Wall Switch Use to control fluorescent lighting, appliances, motors, etc. Rated 15A.

6381-U Ceiling Fan / Low Voltage Dimming Switch Module Dims low voltage lighting and controls motor speed (e.g. ceiling fans) using X10 DIM/BRIGHT! 500W incandescent, 500VA inductive. Call or write for free Leviton listing.

3-Prong Appliance Module

Plug-in appliance module rated 15A resistive, 500W lamps, 1/3HP motors. Off-white. 550 units reserved for promo. By Stanley. HCC-2550. ONLY \$9.99

Enerlogic ES1400e

Step up to Intelligent Home Control!

New ES1400e puts out 50% stronger X10 signal strength than original ES1400! Version 2 software & expansion port for future integrated products.

This intelligent X10 scheduler with 2-way interface monitors your powerline and allows IF-THEN control. Combine with Stanley motion detectors and have music and mood lighting follow you from room to room! Use X10 Sundowner to give your system dusk/dawn input. Great for setting up one-button macros! Once you've set up your home program, the on-line simulator allows you to test it completely! Once the ES1400e is set up, your PC may be powered down or used for other purposes!

The ES1400e is packed with features, including a battery back-up. Hayes Chronograph clock and calendar functions, programming samples, on-line help, complete documentation, 1 yr. warranty. HCC-1400. ONLY \$359

INFO, PRICING & CUSTOMER SERVICE **1-619-693-8887** WHOLESALE PRICES. \$100 MIN. PER ORDER.

TOLL-FREE ORDER LINE (ORDERS ONLY) **1-800-CONTROL**

TERMS: Most in-stock orders ship within 24 hours. Tax applies to Calif. orders for non-resale. Shipping & Handling charge will be added to order. COD orders add \$6.50 to shipping charge. Our standard shipping method is the Continental U.S. is by UPS ground service. Additional charge for UPS second day air, UPS Next Day Air, Federal Express or Airborne Express. Alaska and Hawaii orders are shipped by air service. International orders must be paid in U.S. funds by money order, cashiers check, or credit card. Returns merchandise subject to 15% restocking fee, before returning call for required RMA number. Certain merchandise (test equipment, software, books, etc) may not be returned for credit. Defective products will be repaired or replaced at our option. Double manufacturer's warranty on most items. We will match or beat any competitor's price. Not responsible for typographical errors. Limited time specials. Quantities may be limited. Phone our Customer Service Department between 8 a.m. and 5 p.m. Pacific Time for complete details.

VACUUM TUBE DEALER PRICE LIST Apr. '92



SOVTEK®, RUSSIA

5U4G	\$5.25 each	12 at \$4.75 each	25 at \$4.25 each
12AX7WA/7025	4.35	3.75	3.60
6922 (military 6DJ8)	6.75	5.90	5.20
EL84/6BQ5	2.90	2.60	2.25
EL84M/6BQ5WA	5.80	5.20	4.50
6V6GT	4.25	3.50	3.20
6L6GC	3.50	2.95	2.60
5881/6L6WGC	6.75	6.20	5.75

50 CALL FOR SPOT QUOTE
100 CALL FOR SPOT QUOTE

The 5881 is Russia's selected military 6L6WGC and is regarded as the very best 6L6 type in the world. Eric Clapton recently replaced the Philips/Sylvania 6L6 STR's in the custom Soldano amp which he uses live, with SOVTEK® 5881's because of their milky smooth sound. Discriminating musicians thruout the world are retubing with the SOVTEK® 5881/6L6WGC.

SINO, CHINA

5U4G	\$4.90 each	10 at \$4.25 each	25 at \$3.95 each	100 CALL FOR SPOT QUOTE
EL34	5.25	4.80	4.25	" " " " "
6L6GC	4.75	4.20	3.80	" " " " "
12AX7a	3.85	3.25	3.10	" " " " "
12AT7	3.90	3.55	3.40	" " " " "
6146B	11.50	10.60	9.80	" " " " "
6550	9.85	9.25	8.95	" " " " "
KT88	13.50	12.50	11.50	" " " " "

EI, YUGOSLAVIA

EL34/6CA7	\$5.10 each	10 at \$4.65 each	25 at \$4.10 each	100 CALL FOR SPOT QUOTE
KT90	23.90	21.50	19.90	" " " " "
6DJ8	3.15	2.75	2.35	" " " " "
12AU7/ECC82	3.15	2.75	2.35	" " " " "
12AX7/ECC83	2.70	2.40	2.15	" " " " "

SIEMENS, GERMANY

EL34	\$7.25 each	10 at \$6.75 each	25 at \$6.20 each	100 CALL FOR SPOT QUOTE
12AT7/ECC81	4.50	3.90	3.75	" " " " "

TESLA, CZECHOSLOVAKIA

EL34	\$7.25 each	10 at \$6.75 each	25 at \$6.20 each	100 CALL FOR SPOT QUOTE
EL34BL (COBALT BLUE)	7.95	7.45	6.90	" " " " "
E83CC/12AX7a	5.90	5.35	4.95	" " " " "

GE, USA

5U4GB	\$12.50 each	10 at \$11.60 each	6550a	\$19.95 each	10 at \$18.25 each
6CA7/EL34	15.75	14.25	7025	13.50	11.75
6L6GC	14.95	13.50	7027a	17.25	16.50
6LF6	19.25	17.50	7591a	15.50	13.75
12BH7a	9.95	8.75	7868	17.00	16.40
12AT7	6.85	6.30	8417	15.85	14.75

SOLID STATE RECTIFIER

Built into tube socket. Direct plug-in replacement for all 5Y3, 5U4 and 5AR4 types. \$6.25 each 10 at \$5.90

ODD BALL TUBES (MOSTLY USA STOCK)

4CX350A	\$69.00 each	6AX5	\$4.90 each	6J5	\$4.50 each	6X4	\$3.90 each	6189W	\$4.15 each
5AR4	7.95	6BA6	1.95	6J7	5.50	6X5	3.90	(12AU7W industrial)	
5V4GT	4.20	6BK11	6.90	6K11	6.90	6X8	2.90	6267/EF86	3.20
5Y3GT	3.95	6C4	3.50	6SC7	6.90	12AY7	5.95	6973	14.90
6AL5	2.40	6C10	6.90	6SG7	3.50	12AZ7	4.50	7199	17.80
6AN8	5.50	6CA4	3.90	6SJ7	4.50	12DW7	14.90	7247	14.90
6AQ5A	4.60	6CG7	6.90	6SK7	2.90	12FQ8	8.00	OA2	3.75
6AQ8	5.85	6EU7	11.80	6SL7	3.95	5749	2.90	OA3	2.25
6AS7	4.50	6FH8	12.50	6SN7	3.95	(6BA6W industrial)		OB2	2.25
6AU6	2.25	6GW8	6.90	6U10	4.90	5879	8.50	OC3	3.75

GIVE US A CALL ON ANY TOUGH-TO-GET TUBES. WE'LL FIND THEM FOR YOU!

MATCHING AVAILABLE ON ALL OCTAL POWER TUBES 65¢ extra per tube.

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TEST AND BURN-IN, ENSURING PREMIUM MATCH. PAIRS OR QUADS \$2.00 extra per tube.

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\$49 ea.

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AT 200 WATT SUPPLY

Factory Rebuilt
Fits full size AT case
only. 120/220V Input.



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3 1/2" FLOPPY DISK DRIVE

Matsushita JU-253
Includes two 3.5"
Face Plates (Gray & Beige).
Comes with separate
5 1/4" Mounting Kit



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Part No. 220-3418F

5 1/4" 1.2MB FLOPPY DISK DRIVE

Double Sided/
High Density
Hitachi/HFD516C12U
Mfg. for IBM #61X4618
Black Face Plate only!
Part No. 220-3421F



\$69 ea.

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OEM VERSION 3.30.01 Has an
Expanded Memory Manager for
above 640K on 80386 computers,
Print Spooler, Cache, & a file
Encryption Program.
Includes 5 1/4" & 3 1/2" disks,
and Manuals.



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An ideal getting started guide
for beginners. Complete with
Exploring The IBM Personal
Computer Software. Learn the basics:

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disk storage, dos, basic programming and
Furwriter a basic word processing package.

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(IBM #6280102) Retail ~~\$80.00~~ \$9.95 ea.



IBM PS/2 CARRY CASE

Genuine IBM Product
Designed for PS/2 Model 25
Also works great with Macintosh +, SE
Removable casters & feet. Heavy duty
padded Nylon construction.
Completely unzips for easy storage



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SUPER 8 REPEATER PROJECTOR

USED Portable Projector.
Includes a Super 8
Continuous Play Cassette.
8mm film can be replaced
with your own Super 8 films.
Has fold out 11-3/4" x 8-3/4"
Glass Screen. Bulb included.
Includes Padded Hard Sided
Carry Case 16-1/2" x 14" x 8"



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Part No. 650-0139F

ALARM BOARD

Great experimenting board. 24 lug and
6 lug terminal strips, 8 relays, 8 slide
switches, over 30 ICs, 4 heatsinks, 2ft.
four conductor telephone line cord and
many other parts.



\$3.95 ea.

Part No. 100-9990F

PLASTIC PARTS BOX

15"x14"x5"
Great for under
counter storage.



\$5 ea.

Part No. 580-9998F

SCHOOL BUS ALERT

Home Receiver to alert
Students as to the location of
their Bus. Receives Signal
from Bus equipped with
SIMON TRANSMITTER (below).
Mfg. TRANS ALERT 2000, INC.



Add up to
250 units

\$9.95 ea.

Part No. 660-9403F

SCHOOL BUS ALERT TRANSMITTER

Bus mounted Portable
Transmitter that announces
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SIMON TRANSMITTER
Mfg. TRANS ALERT 2000
Ideal for students with special needs.



\$49.95 ea.

Part No. 660-9404F

INFRARED REMOTE A/C SWITCH

Lets you turn on/off lamps,
appliances or other 120V
devices using an IR
transmitter. Turns units
on/off from up to 25' away.
2 prong non-polarized 15A.
Requires a 9V battery.



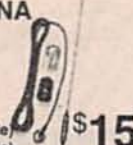
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Part No. 660-0021F

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UHF 445-470MHz
5dB Gain.
Complete with 14 ft.
of cable and PL-259



\$15.95 ea.

Part No. 110-0027F(3/4" Hole)
Part No. 110-0028F(3/8" Hole)

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Electronic flash.
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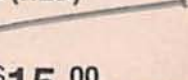


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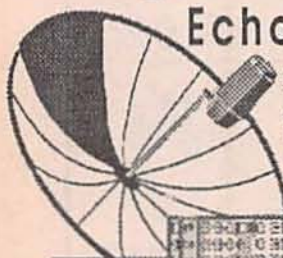
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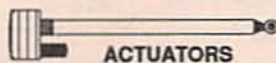
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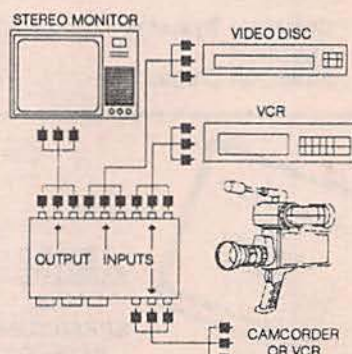
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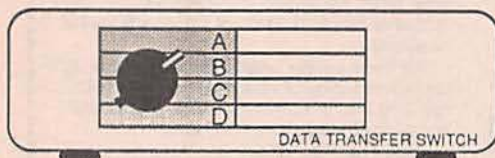
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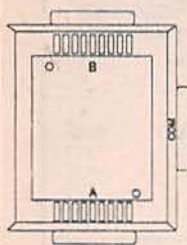
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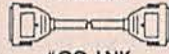
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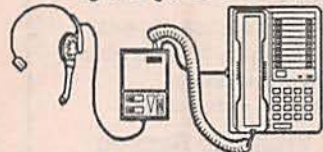
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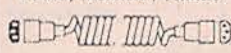
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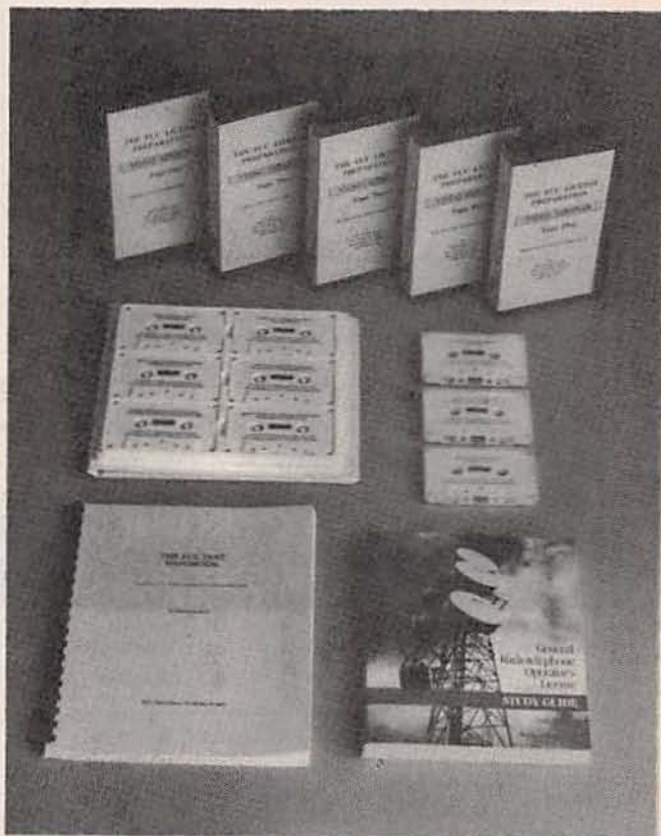
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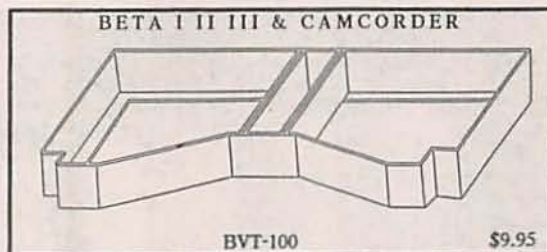
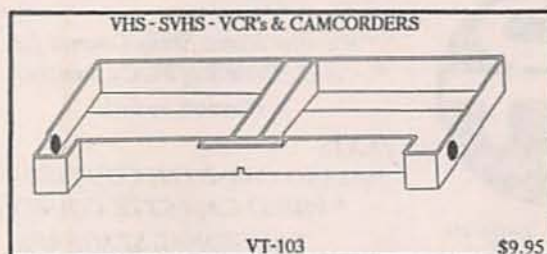
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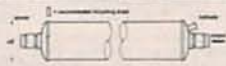
Parts list may vary depending on manufacturer.

GLOSSARY: mW = Milliwatts (light power output)
He-Ne = Helium Neon (red light)
ARGON = laser that emits a blue/green light
nm = Nano Meter (wavelength of light) (color)

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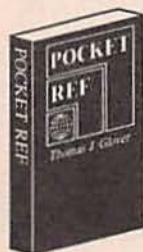
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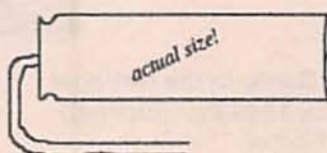
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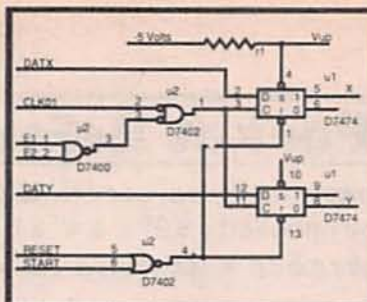
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The **TriField™** meter reads all three types of fields numerically and with a SAFE/BORDERLINE/HIGH SCALE, weighted proportional to effect on the body. Thresholds are based on epidemiological and laboratory studies. (While no absolute hazard thresholds have been established, reduction of relative exposure is prudent.)

The **TriField™** meter comes ready-to-use with battery, instructions, and one-year limited warranty. The cost is \$144 postpaid.

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PC BASED OSCILLOSCOPES OUTPERFORM STAND-ALONES IN COST AND FEATURES

CHASE SCIENTIFIC INTRODUCES 3 NEW PC-SCOPES

By Staff Writer -

Chase Scientific Company has currently introduced 3 new PC based Digital Storage Oscilloscope boards with useful bandwidths of 20, 40, and 60 MHz, and is expecting a 100MHz version by the end of the year. Each scope is completely self-contained on a *single mid-size (10") add-on board* at prices that will make the competition cry.

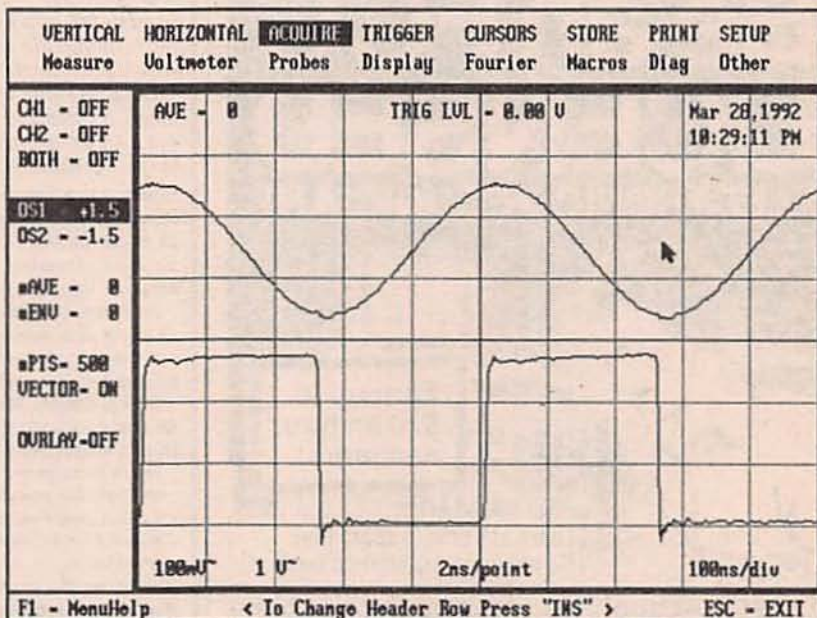
These boards have completely independent vertical channels, each with their own 25 or 40 megasample/sec 8-Bit A/D converter, 8K/32K static ram, and 10 vertical gain settings (in 1,2,5 steps) standard. This gives you the same high performance whether you are using one channel by itself or multiple channels simultaneously - not a common feature among other add-ons. Also, in addition to 27 timebase settings (in 1,2,5 steps), there is a user programmable mode for sweeps as slow as *1 year/div*.

Post and Pre-Triggering is available for time reconstructed waveforms as well as one-shot waveforms due to the board's ability to use *random interleaved sampling* down to 250ps.

These PC based scopes are designed with the latest in *Surface Mount Technology*, providing more performance and features than any other board its size on the market today.

SPECIAL FEATURES:

- Up to 40 Megasamples/sec one-shot digitizing rate.
- 8K Words/Channel standard (32K optional).
- Plot to any Epson or HP LaserJet compatible printer.
- Macro Language for Automated Testing.
- Store and Retrieve WaveForms from Disk.
- Built-in Functions include Ave, Freq, T_R, T_F, PW, Env, FFT
- Professional Scope Software works with virtually all CGA, EGA, VGA, or Hercules compatible monitors.



Actual Output from HP LaserJet IIP at 150dpi

COMPARISON CHART OF CHASE SCIENTIFIC PC-OSCILLOSCOPES

MODEL #	CS100-40*	CS60-25	CS40-25	CS20-25
PRICE (probes not incl.)	\$795	\$695	\$595	\$495
BANDWIDTH				
Repetitive (-3dB)	100 MHz	60 MHz	40MHz	20 MHz
Single-Shot (Sample Rate/4)	10 MHz	6.2 MHz	6.2 MHz	6.2 MHz
MAXIMUM DIGITIZING RATE (Two-Channel Simultaneous)	40 Ms/sec	25 Ms/sec	25Ms/sec	25 Ms/sec
NUMBER OF CHANNELS	2 (+ 1 external trigger/enable)			
TIME BASE RANGE **	20ns-2 sec/div	50ns-2 sec/div	50ns-2 sec/div	50ns-2 sec/div
MAXIMUM TIME RESOLUTION	250 ps	400 ps	400 ps	1 ns
VERTICAL RESOLUTION	+/- 0.4% (8-Bit A/D)			
MEMORY (Standard)***	8K words	8K words	8K words	8K words

* = Available 4th Qtr 92

** = Screen display can zoom up to 10X

*** = 32K option available

All scopes have 10mV/div - 10V/div input sensitivity in 1,2,5 steps (20pF, 1Mohm)

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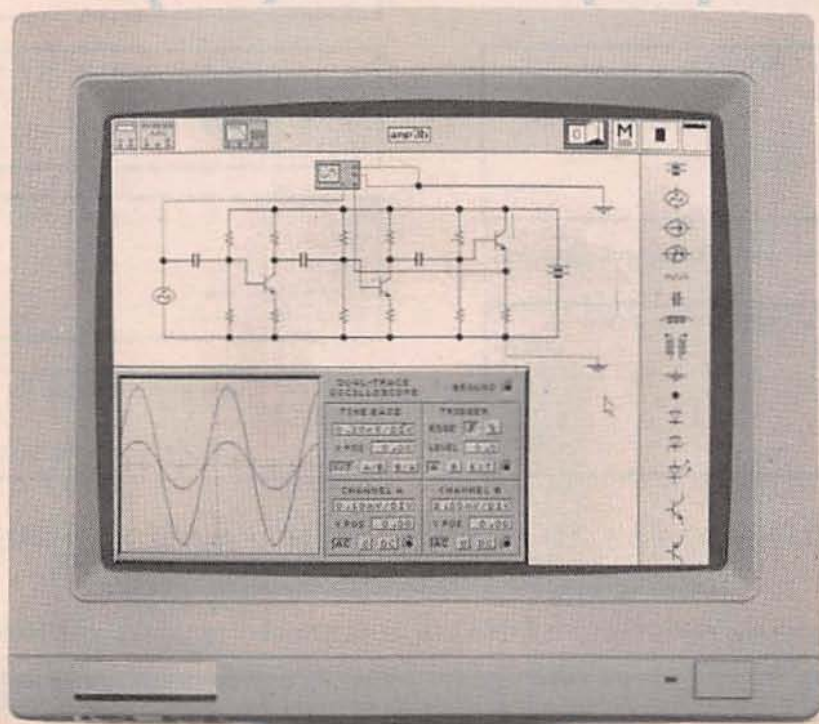
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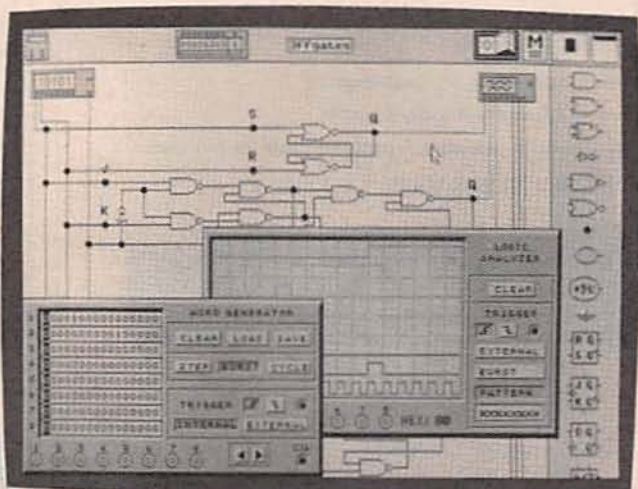
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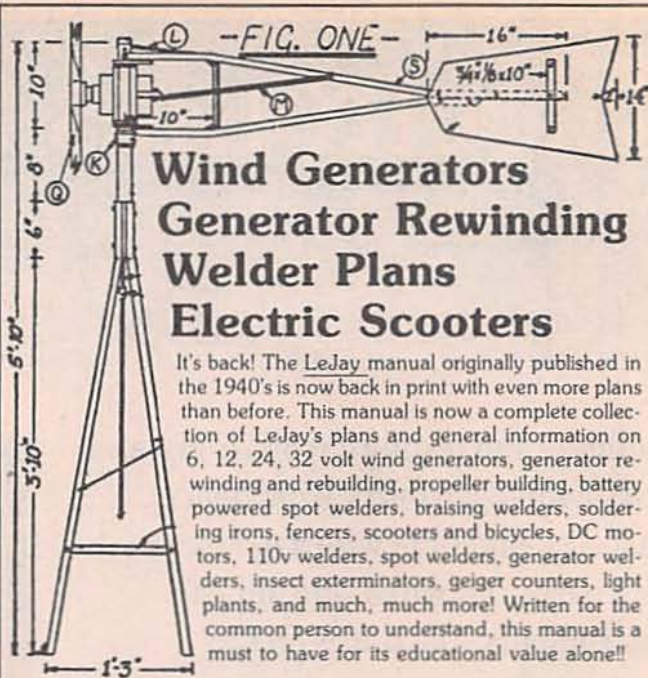


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Power output: 300W into 4 ohms (0.1% THD), 200W into 8 ohms (0.02% THD) • Frequency Response: 10 Hz - 20 KHz • Total Harmonic Distortion Less than 0.03% • Input Sensitivity and impedance at 1 KHz, IV 47k (1) • Load Impedance: 4 - 16 ohms • Power Requirements: ±55 to ±65V DC 8 A • (Each Channel) • Dimensions: 287 x 205 x 60 mm.

100W + 100W NEW CLASS A DC STEREO PRE AND MAIN AMP TA-1500 ▲▲▲



Kit: \$73.70
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Power output: 80 watts per channel into 8 ohms 100 watts per channel into 4 ohms • Total harmonic distortion: Less than 0.03% Frequency response: Aux input: 5 to 50,000 Hz + 0.2dB -2 dB • Frequency response: Power amplifier section: DC to 200 KHz • Sensitivity: Phono: 2.5 mV @ 47 K Aux: 150 mV @ 47 K Mic: 6 mV @ 10 K Output: Tape 150 mV @ 47 K Preamp: 1V @ 600 ohms • Power transformer: 26V to 32 V AC x 2 @ 6 A (Mark V Model 001) • P.C. Board Dimensions: 10.5" x 6.13" x 2.25" • Heat sink 5.13" x 2.63" x 3" (Each) Use rack mount cabinet LG 1924 or LG 1925

VIDEO AUDIO SURROUND SOUND PROCESSOR SM-333 ▲▲▲



Complete Kit: \$73.00
Assembled & Tested: \$85.00

Frequency response: 20 Hz to 20KHz • Total harmonic distortion: Front channel: 0.05% Rear channel: Less than 0.25% • Input signal voltage: 0.1 to 3.5V • Output: Front channel: 0.1 to 3.5V • Rear channel: 6.6V • Delay time: 5 to 50 milliseconds • Input impedance: 47 K • Power requirements: 100-120 VAC: 60Hz • Dimensions: 14.2" wide, 4.82" deep, 2.1" high

120 W MOSFET POWER AMPLIFIER (MONO) TA-477 ▲▲



Kit: \$68.80
Assembled & Tested: \$85.00

T.H.D.: Less Than 0.007% • Power output: 120 watts into 8 ohms RMS • Frequency response: 8 Hz to 20KHz + 0-0.4 dB 2.8 Hz to 65 KHz • 0-3dB • Sensitivity: 1V • Power requirements: 55 VDC @ 3 amps. May use Mark V Model 003 Transformer.

80W + 80W PURE DC STEREO MAIN POWER AMPLIFIER TA-802 ▲▲



Kit: \$45.94
Assembled & Tested: \$59.72

Power output: 80 watts per channel into 8 ohms Total harmonic distortion: Less than 0.05% at rated power. Intermodulation distortion: Less than 0.05% at rated power Frequency response: DC to 200 KHz -0 dB -3dB @ 1 watt Power requirements: 30 VAC x 2 @ 6 amp. May use Mark V model 001 transformer P.C. Board: 8-1/2" x 5-1/8" Heat sink: 5-1/8" x 2-5/8" x 3" (Each)

60W + 60W STEREO POWER AMPLIFIER (WITH MIC. INPUT) SM-302 ▲▲▲



Complete Kit: \$80.00
Assembled & Tested: \$95.00

Frequency response: 20Hz to 20 KHz • Total harmonic distortion: < 0.1% • Power output: 60W per channel into 4 ohm load • 33W per channel into 8 ohm load • Input sensitivity: Mic 10mv • Hi 380mv • Lo 640mv • Signal to noise ratio: Better than 70 db • Power consumption: 100W Dimension 360 mm x 75 mm x 200 mm

120W + 120W LOW TIM PRE-MAIN STEREO AMP. TA-800MKII ▲▲



Kit: \$63.92

Power Output: 120 watts each channel into 4 ohm load, 72 watts each channel into 8 ohm load. Frequency response: 10 to 20 KHz. Total harmonic distortion: Less than 0.1%. Tone control: Bass ± 12 dB Mid: ± 8 dB High: ± 8 dB Sensitivity: Phono input: 3mv into 47 K Line: 3 v into 47 K. Signal to noise ratio: 86 dB. Power requirement: DC: ± 40 VDC at 3.2 A, 8 ohm load DC: ± 40 VDC at 5.4 A, 4 ohm load AC: 28 VAC-0-28VAC at 6.5 A with 8 ohm load AC: 28 VAC-0-28VAC at 10.8 A with 4 ohm load.

120W + 120W AC/DC STEREO HI-FI & PRE-AMP. SM-720 ▲▲▲



Complete Kit: \$83.00
Assembled & Tested: \$98.00

Power Output: 120 W Peak music power output per channel. Input: Sensitivity: Tape 300 mv, Aux 300 mv, Phono 3 mv, Mic 3 mv. Tone control range: Treble ± 8 dB, Bass ± 8 dB. Frequency Response: 20 Hz to 20 KHz. Power Requirements: 110 VAC, 220 VAC, 50/60 Hz 12 to 16 VDC. Dimensions: 272 x 208 x 80 mm 10.5/8 x 8.1/8 x 3.1/8 inch.

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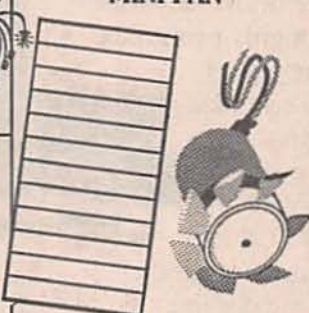
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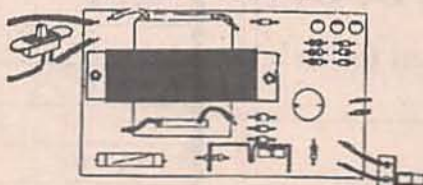
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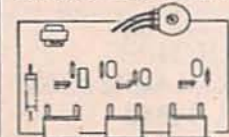
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Design your own power inductors! Easy to use software allows quick accurate designs. Includes databases for Ferrites, powdered iron, MPP, Koolu, E, pot and toroid cores. Calculates number of wire turns around core, to flux swing, copper losses, temperature rise and core losses, etc. Works with window like screens on a PC. For demo disk send \$2, refundable towards purchase.

Part No. ICAD5200 (5 1/4" disk) or ICAD3200 (3 1/2" disks) **\$139.95**

POWDERED IRON TOROID CORES

Micrometals 52 material - Good power inductor cores @ 100KHz. All of these cores are supported by INDUCTOCAD II. Call or write for our Catalog. Try our power core selection package, 6 pairs of the most useful cores you can turn into inductors. These cores are good from power levels of 100mW to 100Watts. Outer diameter from 0.265" to 1.3". Power core selection package Part No. PCSPS206 **\$12.95**

TOROIDAL POWER TRANSFORMERS

Low external field. Excellent regulation @ 10% from no load to full load. Ideal for construction of CAR BATTERY ELIMINATOR.

Primary	DC Output after Rect.	Height	Width	Price \$	Part No.
115VAC	15V/5A	3.8"	1.7"	46.95	TRON1505
115VAC	15V/10A	4.5"	2.8"	72.50	TRON1510
115VAC	15V/14A	5.2"	2.4"	79.25	TRON1514

Toroidal transformers for kits below. Allows 85-132 VAC operation of the kit regulators. **Essential** - Add an AC input filter and diode pack to adapt Power Supply kit to transformer. AC filter and diode pack Part No. FACTRSP9 **\$11.95**

Primary	VA	Matches kit Part No.	Price \$	Part No.
120/240	36	KIPS0503/KIPS0505	38.95	TRONPK36
120/240	45	KIPS1203/KIPS1303	41.50	TRONPK45
120/240	75	KIPS1205/1305/1503	46.95	TRONPK75
120/240	90	KIPS1505	49.50	TRONPK90

SWITCHING POWER SUPPLY KITS

Kits include: All components, PC board, Heat sink, Schematic, Assembly drawing, Inductor design, Assembly instructions, Test procedure. Complete board dimensions 3.3" x 2.3" x 1.3". Typical efficiency > 80%. Add a DC input filter to your boards for lower input noise. This is essential for Audio and Analog applications. DC filter Part No. FDCLNSP3 **\$6.00**

Input	Output	Price \$	Part No.
8-40VDC	5V/3A	37.95	KIPS0503
8-40VDC	5V/5A	39.95	KIPS0505
15-40VDC	12V/3A	37.95	KIPS1203
15-40VDC	12V/5A	39.95	KIPS1205
17-40VDC	13.8V/3A	37.95	KIPS1303
17-40VDC	13.8V/5A	39.95	KIPS1305
18-40VDC	15V/3A	37.95	KIPS1503
18-40VDC	15V/5A	39.95	KIPS1505

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Mt. View, CA 94040
Call (415) 964 2428 Fax (415) 969 9581

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Intel 386DX CPU on 8-slot motherboard with Phoenix BIOS, 2 MB RAM, in case with 250W power supply. New.

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ASCII Electronics

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Also works with Commodore computers. Smooth ball bearing action. Cable with DB9 connector included. (Dealer pricing available.)

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Use as-is or dismantle for a treasure trove of goodies such as: HEAVY snooker ball; 5 ball bearings; 2 optical encoder wheels. ICs are CD4011, CD4013, CD4030, CD4538 and CA339. Also 34 resistors, caps, 3 diodes and one transistor. New, unused.

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36 channel, channel 3 output. Used, working condition.

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Shown approx. 75% size.

6 for \$9.95

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With assembly instruction booklet. Convert ASCII terminal or computer into ham or shortwave AFSK RTTY.

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20,000 Tubes in Stock!

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- 8/16-bit 8088 or 286/386/486 compatible
- 640 x 480 in 16 colors
- 320 x 200 in 256 colors
- 256Kb video RAM

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- CP-30084 84Mb, 19ms IDE hard drive, 16-bit floppy/hard disk controller, cables and instructions

\$319

HOKIT80 \$319

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PART #	BRAND	CAP.	SPD.	TYPE	PRICE
CP-3000	Conner	42Mb	28ms	3.5" IDE	\$199
ST-351A	Seagate	42Mb	28ms	3.5" IDE	\$209
CP-30084	Conner	84Mb	19ms	3.5" IDE	\$299
CP-3096A	Seagate	88Mb	19ms	3.5" IDE	\$319
CP-30104	Conner	120Mb	19ms	3.5" IDE	\$379
ST-3144A	Seagate	131Mb	16ms	3.5" IDE	\$399
CP-3204F	Conner	212Mb	16ms	5.25" IDE	\$599

FLOPPY DRIVES

- FDD-1.44A 1.44Mb, 3.5", Beige \$79.95
 FDD-1.44X 1.44Mb, 3.5", Black \$79.95
 FDD-1.2 1.2Mb, 5.25", Beige \$89.95
 FDD-360 360Kb, 5.25", Black \$79.95

UNIVERSAL PROGRAMMER



- Programs EPROMs, EEPROMs, microprocessors, PROMs, PAL/GALs and other PLDs; tests logic & memory devices
- Optional adaptors available for PLCC, PGA, QFP and multiple DIP devices
- Includes host adaptor card and cable

MOD-EMUP \$699.00

EPROM PROGRAMMER



- Programs 24-32 pin EPROMs & EEPROMs from 16K-1024K
- Hex to OBJ converter
- Vpp 5, 12.5, 12.75, 13, 21 & 25V

\$119⁹⁵

MOD-MEP* \$119.95

MOD-MEP-4* 4-EPROM programmer unit \$169.95

MOD-MAC Host adaptor card & cable \$29.95

*Note: Requires host adaptor card

EPROM ERASER



- Quickly and simultaneously erases up to 4 standard EPROMs

\$39⁹⁵

DATASE II \$39.95

1024 X 768 NON-INTERLACED VGA PACKAGE

\$499⁹⁵

- 0.28mm dot pitch non-interlaced monitor & high-resolution VGA card
- Resolution up to 1024 x 768 in 256 colors*
- 512Kb video RAM expandable to 1Mb



VGA-PKG-1024N \$499.95

VGA-PKG-1024+ 1024x768 interlaced VGA pkg. \$469.95

VGA-PKG 640x480 interlaced VGA pkg. \$349.95

VGA-MON-1024 1024x768 interlaced monitor \$349.95

VGA-MON-1024N 1024x768 non-interlaced mon. \$389.95

*Note: Requires 1Mb RAM for 1024 x 768 in 256 colors

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\$49⁹⁵



BTC-5339 101/102-key enhanced layout \$49.95

3-BUTTON MOUSE

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- Accuracy 290-1450 DPI
- Opto-mechanical design
- Windows 3.0 compatible



JDR-MOUSE-3 \$14.95

MOUSE-PAD \$4.95

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PART #	SIZE	SPEED	TYPE	PRICE
41256-80	256K x 1	80ns	DIP	1.69
41256-60	256K x 1	60ns	DIP	2.39
414256-80	256K x 4	80ns	DIP	4.95
1M8-80	1M x 1	80ns	DIP	5.99
1M8-60	1M x 1	60ns	DIP	6.49
41256A98-80	256K x 9	80ns	SIMM	14.95
41256A98-60	256K x 9	60ns	SIMM	16.95
421000A98-10	1M x 9	100ns	SIMM	39.95
421000A98-80	1M x 9	80ns	SIMM	45.95
421000A98-60	1M x 9	60ns	SIMM	49.95
424000A98-80	4M x 9	80ns	SIMM	169.95
424000A98-60	4M x 9	60ns	SIMM	174.95

MATH CO-PROCESSORS



Each co-processor includes a manual, software guide and Intel's lifetime warranty.

PART #	SPEED	PRICE	PART #	SPEED	PRICE
8087	5MHz	89.95	80387-SXP	33MHz	199.95
8087-2	8MHz	129.95	80387-DXP	≤25MHz	119.95
80287-XL	12MHz	94.95	80487-SX	20MHz	499.95

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- Solderless breadboard with I/O, decode & timing circuitry
- PDS-601 8-bit card \$79.95
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WIRE-WRAP PROTOTYPE CARDS

- JDR-PR2 8-bit with I/O decode layout \$29.95
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 - Identifies unknown part numbers
- MOD-NIC \$129.95



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20MHz CACHE 486SX \$549

- 20MHz Intel 80486SX CPU • 64Kb cache memory on board (expandable to 256Kb) • Expandable to 32Mb on-board using 256Kb, 1Mb or 4Mb SIMMs* (OKB installed) • Includes Intel's "Vacuity" socket

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 MCT-M486-50 Mini-size 50MHz cache 486 \$1295.00
 MCT-M486-33 Mini-size 33MHz cache 486 \$895.00
 MCT-C386-40 Mini-size 40MHz cache 386 \$499.95
 MCT-C386-33 Mini-size 33MHz cache 386 \$449.95
 MCT-M386-25 Mini-size 25MHz 386 \$349.95
 MCT-M386SX-20 Mini-size 20MHz 386SX \$299.95
 MCT-M386SX Mini-size 16MHz 386SX \$249.95
 MCT-M286-16 Mini-size 16MHz 286 \$149.95
 MCT-M286-12 Mini-size 12MHz 286 \$129.95
 MCT-TURBO-10 Mini-size 10/4.77MHz 8088 \$69.95

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\$99⁹⁵

- Accommodates std. motherboards
- Mounts 3 floppy and 4 hard drives
- 2 digit LED display

- CASE-100A \$99.95
 PS-250TW 250W p. supply \$129.95
 PS-300TW 300W p. supply \$149.95
 CASE-50 Mini 286-style case \$59.95
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 CASE-120 \$199.95

Mini-upright case w/200W power supply

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 PS-200 286/386/486 200 watt \$89.95
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 PS-300 286/386/486 300 watt \$149.95



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- Incl. ProComm software

MCT-241 \$49.95

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7400	0.29	74LS02	0.25	74LS191	0.49
7402	0.29	74LS04	0.25	74LS192	0.59
7404	0.29	74LS10	0.25	74LS240	0.59
7406	0.35	74LS14	0.39	74LS241	0.69
7407	0.35	74LS20	0.25	74LS244	0.69
7408	0.35	74LS30	0.25	74LS245	0.69
7410	0.29	74LS32	0.25	74LS251	0.49
7414	0.49	74LS48	0.29	74LS253	0.49
7422	0.35	74LS42	0.39	74LS257	0.39
7427	1.19	74LS43	0.39	74LS273	0.49
7474	0.49	74LS51	0.25	74LS293	0.59
7475	0.49	74LS73	0.35	74LS367	0.39
7486	0.49	74LS74	0.29	74LS368	0.39
7490	0.29	74LS75	0.29	74LS373	0.49
7493	0.49	74LS83	0.49	74LS374	0.49
74116	1.99	74LS85	0.49	74LS482	1.99
74121	0.49	74LS86	0.25		
74123	0.49	74LS90	0.39	745	
74151	0.59	74LS93	0.39	74500	0.29
74153	0.59	74LS107	0.39	74502	0.29
74154	1.49	74LS112	0.35	74504	0.29
74157	0.59	74LS123	0.49	74508	0.29
74161	0.49	74LS125	0.39	74532	0.35
74163	0.49	74LS126	0.39	74538	0.39
74174	0.89	74LS138	0.39	74538	0.49
74175	0.89	74LS151	0.39	74531	0.59
74191	1.19	74LS153	0.39	745153	0.59
74221	1.29	74LS155	0.49	745157	0.79
74290	0.89	74LS157	0.39	745161	1.29
74293	1.49	74LS163	0.49	745163	0.59
		74LS173	0.39	745184	0.99
		74LS174	0.39	745373	0.99
74LS500	0.25	74LS175	0.39	745374	0.99

EPROMS

PART#	SIZE	SPEED	V _{pp}	PINS	PRICE
2732A	4096x8	250ns	31V	24	3.95
2764	8192x8	450ns	12.5V	28	3.95
2764-250	8192x8	250ns	12.5V	28	3.95
2764-200	8192x8	200ns	12.5V	28	4.49
27128A-200	16384x8	200ns	12.5V	28	4.95
27256	32768x8	250ns	12.5V	28	4.95
27C256	32768x8	250ns	12.5V	28	5.95
27312	65536x8	250ns	12.5V	28	5.95
27C101-20	131072x8	200ns	12.5V	32	8.95
27C101-15	131072x8	150ns	12.5V	32	9.95

STATIC RAM

PART#	SIZE	SPEED	PINS	CMOS	IP	PRICE
HM6116P-2	2048x8	120ns	24	Y	N	2.95
HM6116P-3	2048x8	200ns	24	Y	Y	2.95
HM6116P-4	2048x8	150ns	24	Y	Y	3.25
HM6116P-2	2048x8	120ns	24	Y	Y	3.95
HM6264P-15	8192x8	150ns	28	Y	Y	3.95
HM6264P-12	8192x8	120ns	28	Y	Y	4.95
HM6264P-10	8192x8	100ns	28	Y	Y	5.95
HM43256P-15	32768x8	150ns	28	Y	Y	4.95
HM43256P-12	32768x8	120ns	28	Y	Y	5.95
HM43256P-10	32768x8	100ns	28	Y	Y	6.95

PALS

PART#	SPEED	PINS	IN	OUT	I/O'S FUNCTIONS	PRICE
16A8	35ns	20	10	2	6 AND-OR INV	2.95
16A4	35ns	20	8	4	4 AND-OR INV	2.95
16A6	35ns	20	8	6	2 AND-OR INV	2.95
20A8	40ns	24	14	2	6 AND-OR INV	2.95
20A4A	25ns	24	12	4	2 AND-OR INV	3.49
20B6	40ns	24	12	6	2 AND-OR INV	2.95
20B8	40ns	24	12	8	AND-OR INV	2.95
20X8	50ns	24	10	8	2 AND-OR XOR INV	2.95
20L10	40ns	24	10	12	2 AND-OR INV	2.95

GALS

PART#	SPEED	PINS	REPLACES	IN	OUT	PRICE
16V8	35ns	20	10A8 TO 16AP8	8	8	2.49
16V8-15	35ns	20	10A8 TO 16AP8	8	8	2.95
20V8	35ns	24	14A8 TO 16AP8	20	8	3.49
20V8-15	35ns	24	14A8 TO 16AP8	20	8	4.95
22V10	35ns	24	PGM OUTPUTS	22	10	6.95
22V10-15	35ns	24	PGM OUTPUTS	22	10	19.95

8000 SERIES MICROPROCESSORS

PART#	PRICE	PART#	PRICE	PART#	PRICE
8155	3.95	8742	19.95	80484-33	599.00
8224	2.95	8748	8.95	8087	89.95
8237-5	4.49	8749	9.95	8087-2	129.95
8251A	3.49	8755	24.95	8087-1	189.95
8253-5	2.95	8088	4.95	80287-XL	94.95
8255-5	3.95	8088-1	9.95	80387-SXP	119.95
8257-5	3.49	80286-12	21.95	80387-OPX	199.95
8272	4.95	80286-16	49.95	80487-SX	499.95
8741	9.95	80386-33	299.95	ODP484-SX20	449.95

RS-232 BREAKOUT BOX \$34.95

- Ten bi-polar LEDs monitor TF, RD, RTS, CTS, DSR, CD, TC, RC, DTR and TC signals (2 spare)
 - 24 switches for breakout and patching
 - Includes jumper wires
 - Requires no battery
- BRBOX-80** \$34.95

SOLDER STATION \$59.95

- 60 watts thermostatically controlled heat from 200-900°F
 - Solder gun, gun-rest & cooling tray
- 168-3C** \$59.95

SOLDER/DESOLDER STATION

- Oil-free vacuum pump
 - Adjustable temperature (200°-900°F) and vacuum (0.60cm/Hg)
- XY9995D** \$399.95

VOLTAGE REGULATORS

PART#	PRICE	PART#	PRICE	PART#	PRICE
UA7850	1.95	7815K	1.39	7915T	0.59
78L05	0.49	7824T	0.49	7915K	1.49
7805T	0.49	7826K	1.39	7924T	0.59
7805K	1.39	7905	0.49	7926K	1.49
78M05C	0.29	7905T	0.59	LM317T	0.57
7806T	0.49	7905K	1.49	LM323K	3.60
7808T	0.49	7906T	0.59	LM337K	3.40
78L12	0.49	7908T	0.59	LM337T	0.87
7812T	0.49	79L12	0.49	LM338K	4.25
7812K	1.39	7912T	0.59	LM350K	4.25
78L15	0.49	7912K	1.49	LM350T	3.60
7815T	0.49	79L15	0.49	LM723	0.49

NEC V-20 SERIES

The NEC V-20 can improve performance by up to 30%! Pin compatible with the 8088.

- Uses superspeed of 8088 instructions
- High speed address calculation in hardware
- Low power CMOS design

PART#	PRICE
V20	6.95
V20-8	8.95
V20-10	10.95

LINEAR

PART#	PRICE	PART#	PRICE	PART#	PRICE
LM301	0.39	LM380	0.69	LM711	0.79
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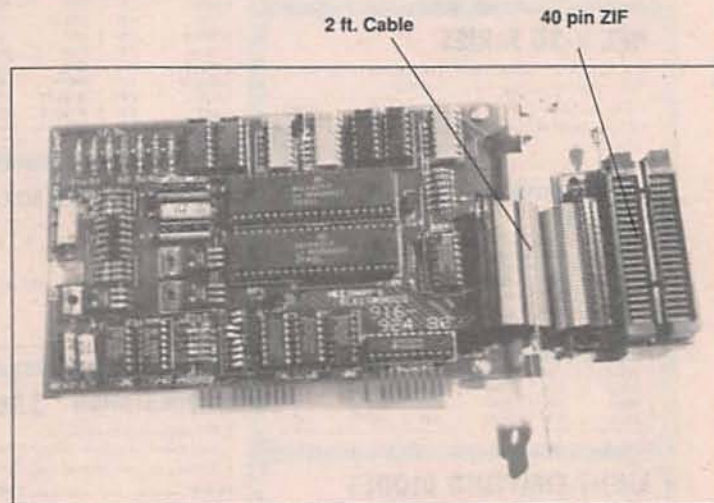
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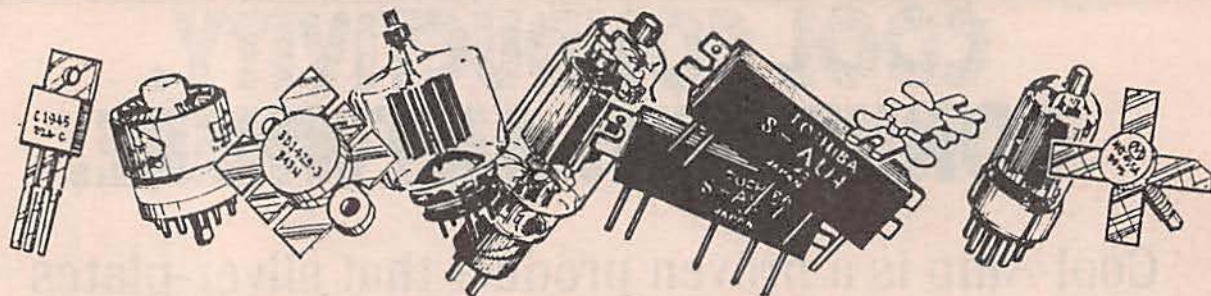
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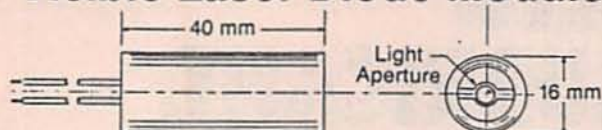
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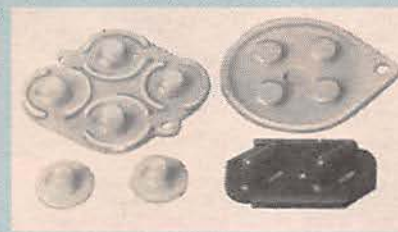
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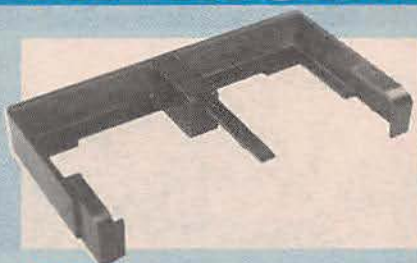
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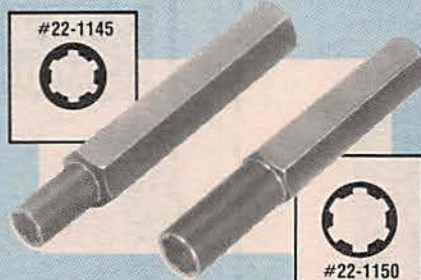
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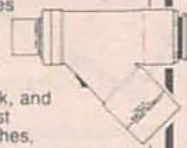
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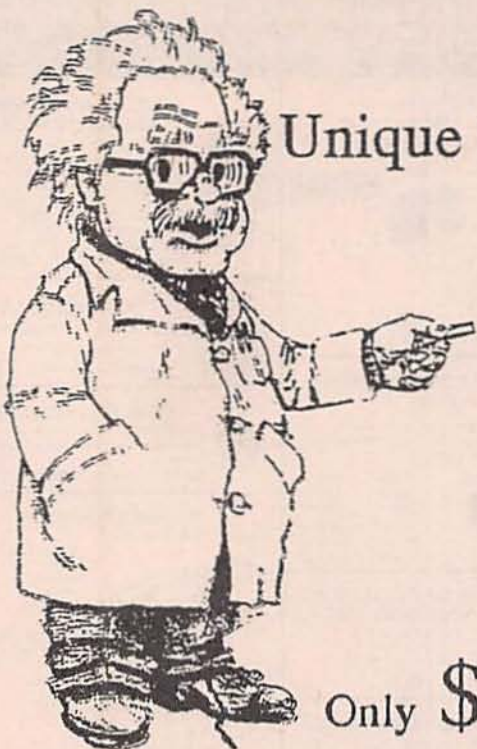
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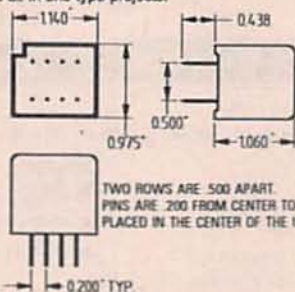
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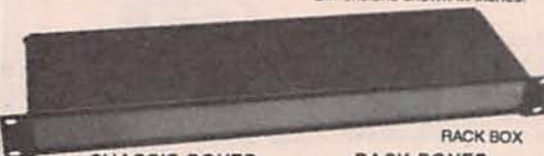
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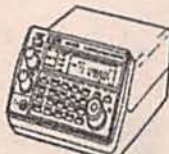
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Bearcat 590XLTX \$199.95 100 Channel 11 Band



Five banks of 20 channels each. Covers 29-54, 118-174, and 406-512MHz. Features scan, search, delay, priority, memory backup, lockout, service search, & keylock. Includes AC/DC cords, mtng brkt, antenna. Size: 7 3/8 x 6 15/16 x 1 5/8. Wt: 7.5lbs. Fax fact document #570.

Bearcat 560XLTZ \$99.95 16 Channel 10 Band



Compact, digital programmable unit covers 29-54, 136-174, and 406-512MHz. Features scan, WX search, delay, priority, memory backup, lockout, review, & auto delay. Includes AC/DC cords, mtng brkt, antenna. Size: 7 3/8 x 6 15/16 x 1 5/8. Wt: 2.5lbs. Fax fact document #560.

Trident TR-2C \$89.95



Scan/CB with optional radar detector
 Scans pre-programmed by state channels in low, high, UHF & T bands. Weather, 40 ch. CB receive plus mobile relay. Size: 7 3/8 x 6 15/16 x 1 5/8. Wt: 2.5lbs. Fax fact document #580.

Mag Mount Antenna. Easy to install whip antenna with 20' of coax & heavy duty magnet BNC MA 100 \$19.95
Base Antenna. 25 to 1000MHz coverage with 50' of coax. All mounting hardware included. BNC AS 300 \$59.95
External Speaker. Base or mobile mount. MS190 \$19.50
Wide Band Pre-Amp. Variable gain up to 20dB covers 100 KHz to 1500MHz. 9Vbatt included. BNC. GW-2 \$89.00
Interference Filter. Filters and eliminates common causes of interference to scanners. BNC. Model MP1F-1. \$59.00
Downconverter. Converts 800MHz freqs to 400MHz for 3 band scanners. Quartz locked, 9V batt. DC89 \$89.00
Extended Warranties & Service. Extended warranties available for most models. Call for quote. Out of warranty service by ex-Bearcat/Regency factory techs. Call for quote.

Hand Held Scanners

AOR 900 \$199.95 100 Channel 800 MHz Five scan banks 5 search banks. Covers 29-54, 118-174, 406-512 and 830-950 MHz (no cell lock). Features scan, search, delay, priority, memory backup, lockout, service search, & keylock. Includes AC/DC cords, mtng brkt, antenna. Size: 7 3/8 x 6 15/16 x 1 5/8. Wt: 7.5lbs. Fax fact document #650.



Bearcat 200XLTN \$239.95 200 Channels 800MHz Keyboard Programmable. Ten scan banks plus search. Covers 29-54, 118-174, 406-512 and 806 956MHz (with cell lock). Features scan, search, delay, 10 priorities, mem backup, lockout, WX search, & keylock. Includes NiCad & Chrg. Size: 1 3/8 x 2 11/16 x 7 1/2. Wt. 32 oz. Fax Facts # 450



Bearcat 100XLTN Now \$159.95 100 Channels, Keyboard Programmable. Similar to 200XLTN above without 800MHz. Fax facts #460

Bearcat 70XLTP Only \$139.95 20 Channels Keyboard Programmable. 10 Band Hand Held with Ni-Cads & Charger. Fax facts #470

Bearcat 55XLTR Now \$99.95! 10 Channels Keyboard Programmable. 10 Band with LCD. Requires 5AA's. Fax facts #480

Table Top Scanners

Bearcat 855XLTE Now \$179.95! 50 Channels Keyboard Programmable with 800MHz. LCD display, lock, priority, Search, WX. Fax facts #655

Bearcat 142XLM Only \$87.95 16 Channels with 10 bands. LED display, lockout, priority, WX scan, review key and memory backup. Fax facts #660.

Bearcat 147XLJ Now \$93.95 16 Channels with 10 bands. Track tuned, LED display, priority, WX search, review, memory backup. Fax facts #670.

Bearcat 172XLM Only \$124.95 16 Channels with 10 bands. Track tuned, LED display, priority, WX search, review, memory backup. Fax facts #680.

Bearcat 800XLX \$239.95



12 bands and 40 channels with 800MHz and nothing cut out. AC or DC. Fax facts #690.

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Grill Guides

Ball and socket type grill guides for attaching speaker grill to cabinet. To use, simply drill the appropriate size holes in cabinet and grill frame. 12 pair per package.



#RJ-260-367

\$1.80
Per Pkg

Triplet DMM

The Triplet model 2202 digital multimeter is a full function DMM with built-in transistor and battery testers. Large, easy to read LCD display. Rotary switch for easy one hand function selection. The test leads conveniently attach to meter so they are always in reach. Test leads, manual, and carrying case included.



Specifications:
DC Voltage: 200mV, 2V, 20V, 200V, 1000V
Resistance: 200 Ohm, 2k Ohm, 20k Ohm, 200k Ohm
Accuracy: ±0.5% at 200V, ±1% at other ranges
AC Voltage: Same as DC voltage
Frequency: 200mV, 2V, 20V, 200V, 1000V
Resistance: Same as DC voltage
DC Current: 1.2mA, 12mA, 120mA
DC Current: 200mA, 2A, 20A, 200A, 1000A
Resistance: 20 Ohm, 200 Ohm, 2k Ohm, 20k Ohm
Accuracy: ±0.5% at 200 Ohm, ±1% at other ranges

#RJ-390-140

\$47.00
Each

Pyle 15" Poly Woofer

15" poly woofer with a 60 oz. magnet and 2" voice coil. Mineral filled poly cone with poly foam surround. Poly cone provides proper internal damping to help control cone motion at high power excursion. Power handling: 100 watts RMS, 145 watts max. VAS= 10.9 cu ft., QTS= .53, fs= 30 Hz. Frequency response: 20-3,000 Hz. SPL= 98 dB/1M. Impedance: 4 ohm. Net weight: 9-1/2 lbs.



#RJ-292-070

\$64.80
Each

Pickering Headphones

We made a special buyout directly from the manufacturer on these super quality personal headphones. 1" dynamic high velocity element with strontium ferrite magnet. Adjustable headband with foam ear cushions. 5 ft. cord to 3.5 mm and 1/4" adaptor included.



#RJ-249-100

\$2.49
Each

10", Thruster Car Woofer

Heavy duty car woofer capable of handling 175 watts max (125 RMS). 4 ohm impedance. Polymerized paper cone with red poly foam surround. Resonant frequency: 26 Hz. VAS= 5.89, QMS= 4.6, QES= .27, QTS= .26. Frequency response: 30-2,000 Hz. Magnet weight: 38 oz. 2" voice coil. SPL= 92 dB 1W/1M. Net weight: 6 lbs.



#RJ-293-090

\$29.95
Each

Pyle 10" Poly Woofer

Long throw poly woofer with poly foam surround for superb low bass. Mineral filled poly cone assures low frequency sound that is smooth, tight, and low in distortion. 2" voice coil, power handling: 85 watts RMS, 130 watts max. fs= 43 Hz. Frequency response: 25-3,000 Hz. SPL= 95 dB 1W/1M. Impedance: 4 ohm. 40 oz magnet. VAS=1.8 cu ft., QTS= .34, QMS= 10.92, QES= .35. Net weight: 8 lbs.



#RJ-292-030

\$45.80
Each

The Loudspeaker Design Cookbook IV

This book describes the "science" of loudspeaker design, however applying it is an "art". Using the information in this book will yield hundreds of possible variations in speaker design, with some subtle and not-so-subtle differences. 1991 copyright, fourth edition. Author: Vance Dickason. 154 pages paperback.

#RJ-500-035

\$29.95
Each

Deluxe In-Wall Speakers

Perfect surround speakers. Customize your media room with these super quality, in-wall speaker pairs. Full size 6-1/2" woofer. Heavy duty 1" soft dome tweeter. Built-in crossover. Fits any standard 2 x 4 or larger wall. Retrofit design allows easy installation in new or existing walls. Response: 50-20,000 Hz. 8 ohm impedance. 40 watts RMS, 60 watts maximum. Includes provision for easy 70V/25V transformer mounting. Overall dimensions: 8-1/2" x 12".



#RJ-300-036

List
\$299.95

\$99.95
Pair

Right Angle 1/4" Phone Plug (Mono)



#RJ-099-020

65¢
Each

Honeycomb Tweeter

Unique tweeter with a square diaphragm of honeycomb material. Diaphragm is 1" square. Excellent dispersion. 13/16" voice coil. Frequency response: 2,000-20,000 Hz. Impedance: 8 ohm. Power handling: 25 watts RMS, 40 watts maximum. 4" x 3-1/4". Limited availability. Net weight: 1 lb.



#RJ-279-110

\$8.70
Each

High Voltage Cap Kit



This 85 piece kit contains a selection of 250, 350, and 450 volt electrolytic capacitors: 5 pieces each of 1, 2.2, 3.3, 4.7, 6.8, 10, 22uF and 2 pieces each of 33, and 47uF, 250V radial caps. 5 pieces each of 1, 2.2, 3.3, 4.7, 10uF and 2 pieces each of 22, 33uF, 350V radial caps. 5 pieces each of 1, 2.2, 4.7uF and 2 pieces of 10uF, 450V radial caps. Over \$62.00 wholesale cost if purchased individually. Net weight: 1 lb.

#RJ-020-950

\$49.95
Each

3" x 5" Speaker

Standard radio and TV speaker. 16 ohm impedance. 3 watts maximum power handling. Limited availability.



#RJ-299-115

\$1.95
Each

Large Input Terminal

Large input cup with push spring terminals and 4 lug terminal strip on rear. Flush mounted housing measures: 4" x 5-1/2" outside diameter. 4-5/8" x 3-1/16" mounting hole required. Limited availability.



#RJ-269-220

95¢
Each

Fluorescent Work Light



Handy light operates on 120VAC or 12VDC. Puts light where you need it. Extra bright 15 watt tube. 15 foot oil resistant power cord with wall adaptor and cigarette lighter plug. Two hooks provided for hanging. Net weight: 2 lbs.

#RJ-360-490

\$18.95
Each

5-1/4", 2-Way Pioneer

5-1/4" paper cone woofer with a 1" post mounted polymer tweeter. 4 ohm impedance. Response: 100-20,000 Hz. Power handling: 35 watts RMS, 50 watts maximum. 2-3/4" mounting depth. Limited availability. Net weight: 2-1/2 lbs.



#RJ-269-065

\$12.80
Each

Mini Super Tweeter

Super paper cone tweeter with silver mylar dust cap. Impedance: 8 ohm. Power handling capability: 2 watts RMS. 9-1/16" voice coil. 1-1/2" diameter cone with mounting tabs. Mounting holes: 1-7/8" on center. Limited availability.



#RJ-279-120

95¢
Each

Duracell "J" Battery

Popular TV/stereo remote control battery. Size "J", 6 volt alkaline. Duracell #7K67.



#RJ-140-090

\$3.40
Each

15" Thruster

Super duty, 15" car audio bass driver. Low 25 Hz resonant frequency. Weather resistant polymerized paper cone with red poly foam surround and two color printed dust cap. Power handling capability is 250 watts (170 watts RMS). 2" high temp voice coil with rear vented pole piece. 4 ohm impedance, 50 oz. magnet. Frequency response: 23-2,000 Hz. VAS= 19.04, QMS= 3.96, QES= .21, QTS= .20, SPL= 97.85 dB 1W/1M. Net weight: 11 lbs.

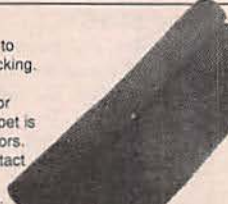


#RJ-293-150

\$59.95
Each

Cabinet Carpet

This high quality carpet conforms easily to sharp corners because it has no stiff backing. You can also stretch it to cover irregular shapes. This is the covering of choice for car, stages, and amplifier cabinets. Carpet is strong yet easy to cut with knife or scissors. Adhere with spray adhesive or latex contact cements. Provides protection and good looks. Sold by the linear yard. 54" wide.



#RJ-260-765 (Dark Charcoal)

#RJ-260-767 (Medium Grey)

#RJ-260-768 (Jet Black)

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Power Cord

Super duty power cord. 14 ga., 3 conductor. 4 ft. length. Limited availability. Black color.

#RJ-119-010 **\$1.50** Each

12VDC, 800mA Adaptor

Fisher Price battery charger. 120VAC input. 12VDC, 9.6W (800mA) output. 6 ft. cord with special connector. Limited availability.

#RJ-120-361 **\$4.95** Each

VCR Parts Assortment

Convenient assortment of clips, washers, springs, and screws. 10 pieces each of 4 sizes of "E" clips, 10 pieces of 2 sizes of retaining rings, 10 pieces of 14 sizes of washers, 2 each of 8 sizes of tension and compression springs and 24 assorted screws. Total of 246 pieces.

#RJ-430-315 **\$6.50** Each

Speaker Sealing Caulk

Special rubber compound quickly and easily seals speakers into cabinets. Eliminates vibration and air leaks. Sold in 1/4" x 36" strips. Strips are self-adhesive so they stick easily to speaker frame. Limited quantity.

#RJ-269-300 **75¢** Each

Replacement Antenna

Hinged 7 section antenna. 19" extended, 5-1/4" collapsed. 3/16" threaded base. Excellent antenna for portable radios, TVs, and more.

#RJ-210-200 **50¢** Each

Quality 30 Watt Iron

Economical 30 watt iron with replaceable tip. Blue plastic handle. 120VAC. A quality iron at a reasonable price. Display packaged.

#RJ-370-010 **\$4.90** Each

Soldering Stand

Convenient weighted soldering iron stand with cleaning sponge. Display boxed.

#RJ-370-020 **\$4.95** Each

Kester Pocket Pack

Perfect tool box solder supply. The wire feeds conveniently from the handy dispenser tube. Pocket clip attached. .031" diameter solder. .5 ounce (approximately 15 feet).

#RJ-370-050 **\$1.00** Each

Isotip Butane Soldering Iron

The ideal soldering iron for field repairs where no AC power is present. Operates for up to 100 minutes of continuous soldering per refill. Uses standard butane (not included) available at most stores. Tip temperature is adjustable up to 1067° F. Iron also comes with a torch attachment which easily screws on in place of the soldering tip. As a torch, one refill will provide up to 1 hour of continuous flame. Temperature is adjustable up to 2372° F. A protective cap with a built-in striker is included. Limited one year warranty.

#RJ-370-235 **\$24.95** Each

Cable Tie Mounts

Package of 10 adhesive back cable tie mounts for securing bundles of wire.

#RJ-080-515 **\$1.20** Pkg

Monitor Power Jack

Standard computer type monitor jack. Limited quantity.

#RJ-090-446 **85¢** Each

Spray Handle

Fits most paint and cleaner cans. Limited availability.

#RJ-340-371 **75¢** Each

Pull-Out Radio Carry Case

Super quality nylon bag for storing pull-out radios. Padded construction with adjustable carry strap. Storage pocket will hold up to 5 CD cases. Inside dimensions: 7-1/2" x 2-1/2" x 8".

#RJ-265-950 **\$10.80** Each

F-59 Deluxe Connector

Popular connector for cable TV systems. Full attached ferrule for hex crimp. Securely holds RG-59 cable.

#RJ-090-355 **17¢** (50-up)

Matching Transformer

Adapts 75 ohm coax to 300 ohm twin lead (or vice-versa) at antenna or television. 5-90 MHz UHF/VHF. 3 capacitor, PC board type.

#RJ-180-010 **49¢** Each

Belt Camcorder Battery Pack

Very high current power pack. Will run most camcorders up to 10 times longer than clip-on batteries. 12V, 6.5AH sealed lead acid type battery. Fuse protected with cigarette lighter output. Comes in padded case with quick release belt and UL approved charger. Net weight: 6 lbs.

#RJ-140-603 **\$48.80** Each

TNC Male Crimp-On

(For RG-59 and RG-62).

#RJ-090-1000 **\$1.45** Each

Technician's Turntable

Turntable to speed repair of VCRs, TVs and more. Lets technician easily turn unit for convenient repair. 20" diameter. White color. Net weight: 5 lbs.

#RJ-360-425 **\$19.95** Each

Outdoor Phone Jack

Heavy duty, diecast aluminum housing withstands the harsh conditions associated with outdoor use. Form gasket under snap shut lid prevents water leakage. Complete with mounting screws. Limited availability.

#RJ-150-030 **\$2.95** Each

Universal Video Cable

6 ft. RG-59 cable with a push-on "F" connector to a combination 75 and 300 ohm balun (switchable between 75 and 300 ohm).

#RJ-180-126 **\$2.75** Each

AGC Fuses

San-O brand fuses. Sold in boxes of 100 pieces. Special buyout price. Limited availability and values.

#RJ-070-421 (.5A) **\$3.95**

#RJ-070-429 (2.5A) **Per 100**

Mini Headphone Extension

Add 6 feet to your mini headphones. Gives the user added mobility when listening to personal cassette players.

#RJ-240-090 **\$1.65** Each

Unfinished 6" x 9" Cabinets

You can paint or finish to your liking. Deep enough for extra large magnet speakers. Flush mount design for rear deck baffle applications. Dimensions: 11-3/4" x 8-1/2" x 6-3/4" x 5" (tapered back). Sold in pairs. Net weight: 9 lbs. per pair.

#RJ-260-450 **\$12.50** Pair

8 Position Dip Switch

Switch type (IE: rocker, slide, toggle) may vary, call.

#RJ-060-134 **60¢** Each

12V, 2.3AH Camcorder Battery

Popular battery for use with Canon, Chinon, Curtis Mathes, G.E., Magnavox, Minolta, Olympus, Panasonic, J.C. Penny, Pentax, Philco, Quasar, Sears, Sylvania, Teknika and other miscellaneous manufacturers. Dimensions: 7.17" (L) x .94" (W) x 2.42" (H). Weight: 1-1/2 lb.

#RJ-140-541 **\$41.95** Each

Velcro Type Fasteners

2, 1" x 2" hook and loop fasteners for attaching almost anything. Great for securing radar detectors to your dash. Each piece has a self adhesive back. Thousands of uses.

#RJ-265-900 **48¢** Pkg

Pressfit Speaker Terminal

Spring loaded, pushbutton speaker terminal in a round housing. No screws required to fasten; simply drill a hole, apply glue, and press into place.

#RJ-260-295 **95¢** Each

3.5 Amp DC Power Supply

A quality, compact 12VDC power supply. Perfect for testing car stereos, CB equipment, radar detectors and other 12VDC items. Regulated 13.8VDC, 3.5 amp continuous, 5 amp surge. LED power indicator. Binding post outputs. Net weight: 4 lbs.

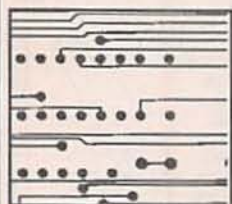
#RJ-120-500 **\$23.80** Each

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TO DISK |
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XST500(E-Z) E-Z Kit \$39.95



The Use of surface mount technology makes this the smallest telephone transmitter you can buy. Powered by the phone line, it can transmit a phone conversation up to 1/4 mile. Our E-Z kit has all the surface mount parts pre-assembled to the circuit board.
XSP250(E-Z) E-Z Kit \$29.95



The XTR100 Tracking Transmitter transmits a continuously beeping tone that can be received by any FM receiver. Can be used for games, contests, or as an anti-theft device.
XTR100(C) Kit \$39.95



The XFM100 FM transmitter has a range of up to 1 mile. It works with any standard FM receiver. It contains a built in high gain two stage audio amplifier for maximum sensitivity.
XFM100(C) Kit \$35.95



The XTT100 is a battery powered phone transmitter with a range of up to one mile. It only transmits when the phone is being used in order to conserve battery life.
XTT100(C) Kit \$35.95



The XBD200 quickly locates hidden transmitters from 1 to 2000 MHz by emitting an audio output proportional to the transmit level.
XBD200(C) Kit \$44.95



Use the XPS100 to call your home from any other phone and listen in using the built in microphone and amplifier.
XPS100(C) Kit \$45.95



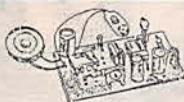
The XPB1 is a telephone transmitter capable of transmitting to any FM receiver up to a 1/4 mile away. Powered by the telephone line it requires no batteries.
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RADAR SIGNAL DETECTOR

If you think that a sensitive radar detector is a complicated piece of equipment, take a look at this new kit. This simple, yet effective, detector circuit can be built in less than an hour and can be tuned to respond to signals between 50MHz to 500GHz. It's a fun kit to build and play with. A cigarette lighter plug is included. Size 1" x 3/4" operates on 9 to 15v DC.

KIT RSD-1 \$12.95

STROBE LIGHT

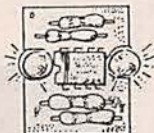
If you need an attention getter, or warning light, you need the strobe light kit. Use it for emergency light for autos, for model planes or radio towers. Even use it on your bicycle. Operates on 6 or 12v DC and has a variable strobe rate.

KIT ST-1 \$8.95

DIGITAL THERMOMETER

Have you ever wanted to tell temperature changes fast & accurately? The DT-1 kit will turn your digital volt meter into an accurate digital thermometer with .1 degree resolution. It gives you a 250 degree window with a range from -40F to 300F degrees. It has a remote sensor .25" sq. that can be mounted many feet from the meter if need be.

KIT DT-1 \$8.95



BLINKY LIGHTS

Want to attract attention? These kits are perfect for decorating name tags, lighting up your hat, or flashing lights for your model trains. Some people use them to simulate a burglar alarm for autos. Put it in a box, set it on your dash and it looks like the real thing. Each kit contains two LEDs that alternates flashing. Operates on a 9v battery. Size .5" x .5"

KIT RB-2 \$3.45

CAPACITANCE METER

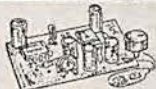
This easy to build kit will turn your digital volt meter into a CAPACITOR METER. Turn that junk box of unmarked capacitors into a fortune. Measures capacitors from 2pF to 2.2uF. Operates on a 9v battery. Size 1.75" x 2"

KIT CA-2 \$12.95

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Small but mighty .8"x1" PCB, will really stomp out a signal well over 400 yds. This is a buffered wireless mike that operates on 80 to 120 MHz FM. Comes complete with a microphone, and 9V battery connector. Operates on 6 to 12v DC.

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KIT AA-1 \$10.95



AC LINE MONITOR

This is something every computer user, photographer, or anyone that must maintain a safe usable AC line voltage should have handy. Monitor the voltage of your motor home's 110v AC generator inside the motor home. Every technician's bench needs this item. The AC line monitor will indicate, with multi-color LEDs, what voltage is being distributed to your equipment at that particular outlet.

KIT LM-110 \$10.95



12V BATTERY MONITOR

Have you ever been in your car, boat, or camper — you try to start your motor but the battery is dead? The BATTERY MONITOR kit uses the cigarette lighter plug outlet to monitor the true battery voltage. Multi-color LEDs indicate the voltage in 1v steps from 11v to 15v, green means great, yellow is good, and red — call the tow truck or get out the oars. Size 1.2" x 1.75"

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KIT TEL-B1 \$10.95



PHONE RECORDING SWITCH

This telephone line powered switch is small enough to install anywhere only .9" x .6". Every time someone picks up the phone the tape recorder will record both sides of the conversation automatically. Use it in your office to record all phone conversations so you don't lose that important address you wrote on the back of an envelope.

KIT TEL-SW 1 \$10.95

BUSY PHONE LIGHT

Add this little kit to any or all of your phones. When any extensions are in use the LED will light. Uses a 9v battery. P.C. Board 1" x 1/2". Complete with etched & drilled PCB, all parts and schematics.

KIT TEL-LIT-1 \$9.95



VOICE ACTIVATED SWITCH

This vox can be used to operate a tape recorder, ham radio, CB radio. Use it to turn on an alarm. The output can operate a load up to 100ma. It will operate a relay, lights, motor, or LEDs. What could you do with a sound activated switch? Size 1.5" x 1.25"

KIT VOX-1 \$6.95

LIE DETECTOR

This kit can be great fun at parties. Lie and an audible tone will change, the more you lie the more the tone changes. When you lie your palms & forehead sweat. This kit allows you to measure these changes. Only a very slight amount of change will cause the tone to increase in frequency. Operates on 6 to 12v DC. Size

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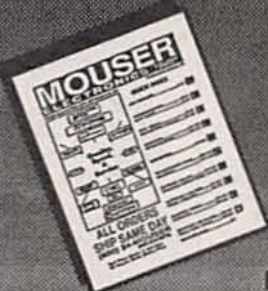
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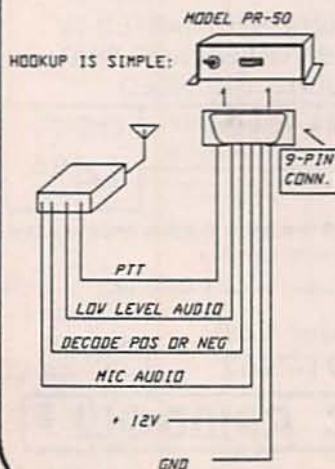
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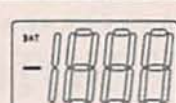
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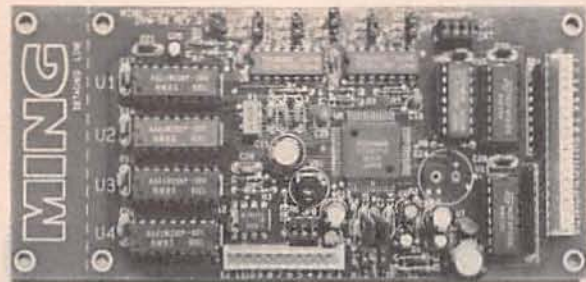


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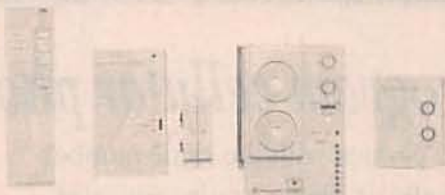
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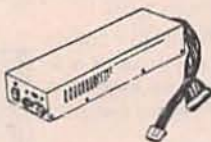
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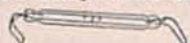
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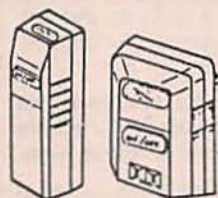
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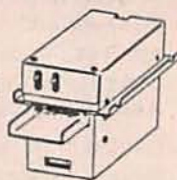
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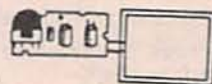
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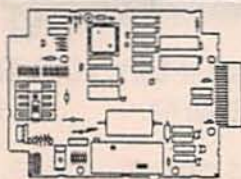
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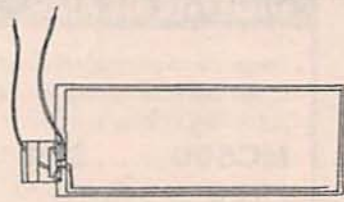
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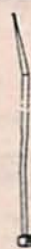
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TR-600B	6"	30 lbs	black	1 1/2"	.50	\$4.00	\$30.00
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6 Vdc	300 ma.	2.1 mm co-ax	positive	DCTX-632	\$2.75	C
7.5 Vdc	400 ma.	1.3 mm co-ax	negative	DCTX-754	\$3.25	C
8.3 Vdc	10 ma.	battery snap		DCTX-8310	\$1.50	C
9 Vdc	200 ma.	2.1mm co-ax	positive	DCTX-920	\$2.75	C
9 Vdc	300 ma.	2.1 mm co-ax	positive	DCTX-932	\$3.00	C
9 Vdc	300 ma.	2.5mm co-ax	negative	DCTX-931	\$3.00	C
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12 Vdc	100 ma.	2.1mm co-ax	negative	DCTX-1210	\$2.50	C
12 Vdc	500 ma.	2.1mm co-ax	negative	DCTX-125	\$4.50	C
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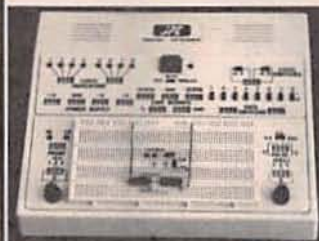
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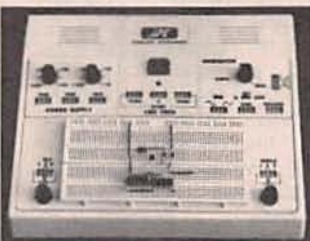
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BB840	840	0	no	\$ 5 ⁴⁹
BP605	1,620	4	yes	\$19 ⁹⁹
BP610	2,230	4	yes	\$24 ⁹⁹



BP605



BB100



BB640



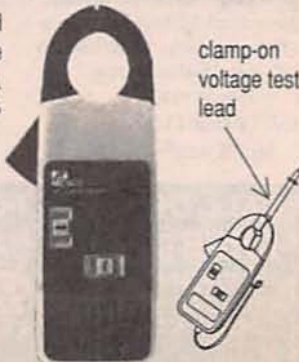
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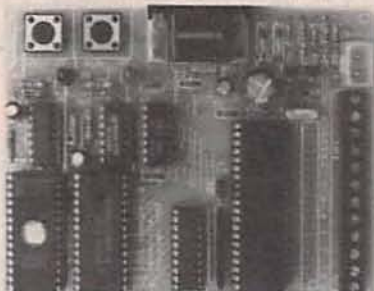
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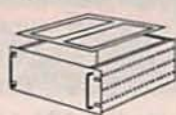
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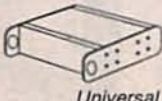


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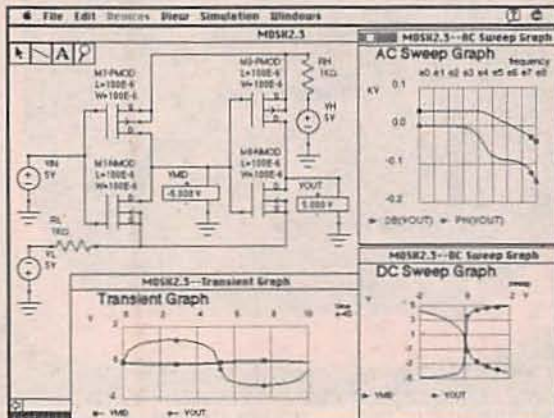
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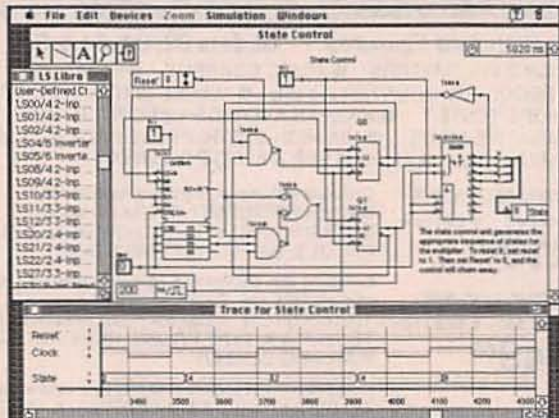
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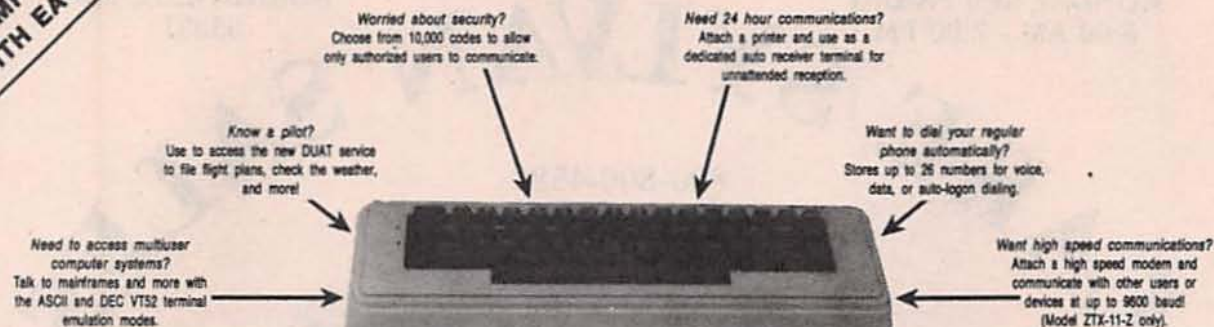
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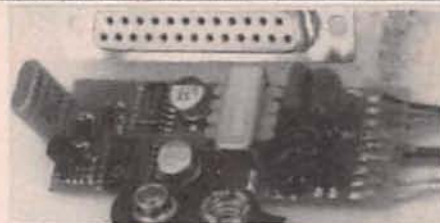
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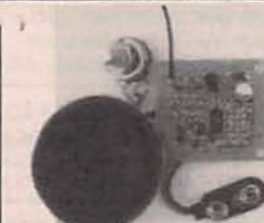
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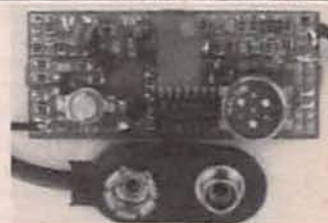


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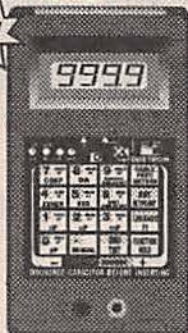
* Hold function forces display in most modes

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* identifies transistors (PNP/NPN) and their leads (EBC etc.)

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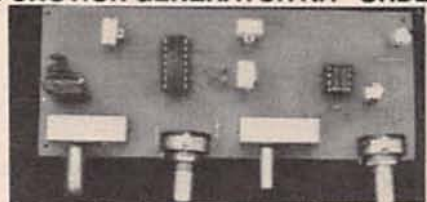
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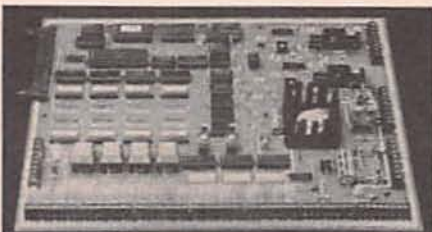
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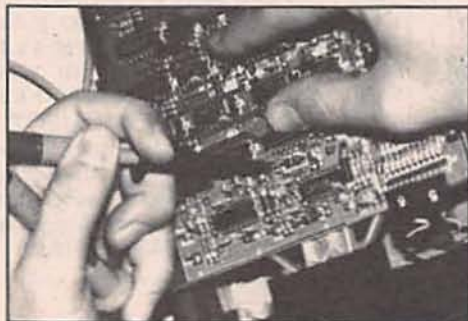
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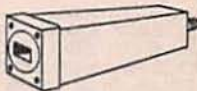
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HSC#13123

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Pocket-sized Ku-Band LNB...

...Not that you'd receive many satellite signals in your pocket, but this techno-marvel is that small! Measures only 4.5" overall length, with 1.5" square face. Noise figure of 1.2dB. Gain of 58dB, ready to attach to .75" x .375" rectangular waveguide for Ku-Band downlinks. We don't know operating voltage yet, but this info should be available. Manufactured by Norsat, Model# BSCA83H02



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HSC #KU-LNB

\$49.95

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These units are to be used at work stations where static charges are a concern (i.e. CMOS circuit assembly). They produce a tone whenever one of three selectable levels of static charge is present in their monitoring area, allowing you to take preventive action. Only 4" tall and comes with its own 9VDC 300mA adaptor, or will run off internal 9V battery (not included). Prevent those shocking developments!

HSC#12846

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1K 10 Watt Resistor	7874	.25	.20	.18	.15
75 Ohm 5 Watt Resistor	5344	.25	.20	.18	.15
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Perestroika Fallout...Soviet Science Collector's Item!

History on the march! Empires crumbling! Eager young scientists being trained for the new world order! We took advantage of the changing world scene to bring to you these unique items that also represent great value...Russian (formerly Soviet) microscope! The manual calls them training microscopes, we would probably call them student-grade instruments, although they are not toys. They are biological (illuminated from below via mirror) microscopes with two objective lenses (8x, 20x) and three eyepieces (7x, 10x, 15x). The optical quality and workmanship are surprisingly good, given the stories we've heard of Soviet labor woes. The base and ringed armature are handsome painted cast aluminum, and the objective turret and lens bodies are chrome-plated brass. The only assembly required is to screw the eyepiece tube into the frame, and drop in your choice of eyepiece. These units are new, liberally greased (l), packed with a large sachet of dessicant in styrofoam & cardboard, and bed with string! The 50-page manual is in fair English, and is duty rubber-stamped with several acceptance dates (1988) and certification numbers on the back. You can think of it as a piece of history, or just a decent, inexpensive microscope, only \$69.95! Hurry, limited quantities!



HSC #13065

\$69.95

Teeny Tiny Tuner Modules



The unusual item at left is a MITSUBISHI CRTV9-AC55F 83 Channel Reverse Converter - the opposite of a tuner - input IF signal (45.75 MHz) converted to one of 83 CATV signal frequencies (55.25MHz to 547.25MHz) selected by voltage input to varactor diode (3-24VDC). Requires +12-5VDC - Pinout, Spec. Sheet & Block Diagram included. Body Measures 3.75"x2"x.75". Useful for Amateur TV? Hams?

HSC #13120 \$14.95



Here is a little module that you won't find anywhere else! This tiny (only 1" x 1.75" x .5") PC mount package is a varactor tuned FM tuner! Made by Toko (Model #TMC103A) for use on the PC FM Subcarrier adaptors at right. Uses 8 - 12VDC, tunes from 88.3 to 108.1 MHz from 75 ohm antenna input, has 10.7 MHz IF output with Vcc output for control feedback to tuning circuitry. We provide a schematic of a suggested application showing pinout of this module with related tuning circuit.

HSC #13101 \$4.95 ea. or 10/\$39.95

FM Computer Network Gear...

Just in...and it goes to show you what things you will find in Silicon Valley's surplus! We have come across a large quantity of components of a nationwide subscription computer network system...software, data and E-mail was sent by means of Broadcast FM Subcarrier and satellite! Perhaps another idea that was ahead of its time, who knows? Anyway, here is a rundown of the pieces, maybe you will think of something to do with them...Note: please don't contact the manufacturer, as they have moved on to other things!



A. "PIN-Desk" IBM/FM Subcarrier Receiver Board. Made by Indesys (similar to illustration). Full length XT style board has shielded box with FM tuner (frequency selected by software), piggyback board with either a 80C31 or two CY2901's. Comes with dipole antenna (see "B" at left) and two diskettes, one marked "Send" and one marked "Receive". This is intended to be part of an FM subcarrier subscription "network" for sending and receiving messages, files and data anywhere in the country! A hacker's bonanza with (depending on revision) NVSRAM's, MAX231, 80C800, Synthesized FM tuner, RF Parts, etc.!

HSC #13084 \$24.95

B. "PIN-Mail" Receiver SA-287A, also made by Indesys. This was part of their "PIN" system, and you were supposed to be able to receive E-mail, unattended, via FM Subcarrier with just this box, an antenna (included) and a printer! Or it could be hooked up to a computer via parallel port. Box has numeric keypad on top, plus connectors on back for power, printer, computer and antenna. No diskettes (software is in ROM), just the receiver unit, dipole antenna and power supply.

HSC #13085 \$24.95

C. Satellite Data Receiver ST-189, by Indesys. Extentally similar to "C" above, but very different inside, unit was designed to be hooked to a small dish antenna and LNB (not included, and we don't have any) for satellite reception of data and E-mail. Power Supply provided. Many interesting parts inside, including Z-80, NVSRAM, RF Linear parts, 80C31, Sierra Semi SC74008, high frequency varactor tuner, etc. Experimenter's delight!

HSC #13100 \$24.95

Broadcast FM Antennas

A. Winegard SR-8108 Yagi-type FM/VHF Antenna. Small mast-mount antenna appears to have been designed for attic or drop-ceiling applications, but we can't see any reason not to use it outdoors. 22.5" boom, longest element is 67". It was intended for the data receivers at right in fringe reception areas, but will of course work fine for FM Broadcast reception with your stereo, as well as VHF/TV reception! New with assembly and mounting instructions.

HSC #13086

\$19.95



B. Dipole antenna (not shown). Typical 300-ohm stereo FM-type dipole antenna with built-in balun for 75-ohm coax, plus a six-foot coax cable with F-connectors. Works great with FM stereos, VHF TVs, or the units at right!

HSC #13087 \$1.95ea. or 10/\$15.00

C. FM "Rubber Ducky" Antenna...18" long with pivot joint on mounting box, 75-ohm coax cable (6 foot) with "F" connector. Could be used in place of "D" above.

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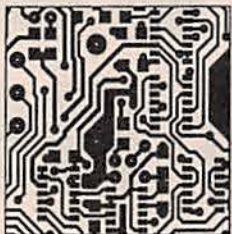
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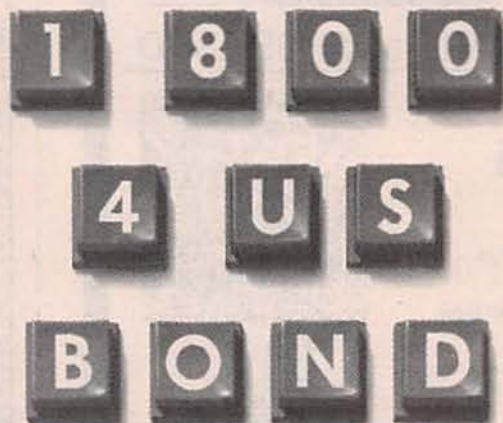
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three 5000-ohm resistors in series between the supply voltage and ground so that one-third of the supply voltage is developed across each resistor. The internal flip-flop circuit provides a definite "on" or "off" response. Its timing intervals are independent of the supply voltage.

The 555 has two basic operating modes: *monostable* (one-shot—a single pulse is emitted), and *astable* (a stream of output pulses is generated). In the monostable mode when functioning as timers, time is precisely controlled by the external RC network. In that mode the 555 produces output pulses with rise and fall times measured in microseconds.

In the astable mode, the 555 can be an oscillator. It can maintain an accurately controlled free-running frequency and duty cycle with only two external resistors and one capacitor. In either monostable or astable modes, timing accuracy is essentially independent of variations in supply voltage or ambient temperature. The device can be triggered and reset on falling waveforms.

Typical applications for the 555 include precision and sequential timing, pulse generation, pulse-width and pulse-position modulation, and linear ramp generation. Moreover, it can directly drive loads such as relays, solenoids, low-power lamps, and high-impedance speakers.

The 555 is packaged in plas-

tic and metal DIP's and 8-pin metal cans for operation in the commercial temperature range of 0 °C to +70°C. Some plastic DIPs can operate in the -40°C to +85°C extended temperature range.

Alternate-sourced 555's can usually be identified by the inclusion of the numbers 55 or 555 in their designations. Examples include Harris' CA555, Motorola's MC1455, and National Semiconductors' LM555C. Other sources include Exar, Goldstar, Raytheon, Samsung, SGS-Thomson, and Sharp Electronics. CMOS versions of the 555, such as Texas Instruments' TLC555 are also available. In addition to their low power consumption compared to standard 555's, their outputs are compatible with CMOS as well as TTL.

Table 1 presents some basic electrical characteristics for the 555. The 556 is housed in a 14-pin DIP package but the block diagram of each circuit is identical to that of the 555 shown in Fig. 1. The 556 is also alternate-sourced by many of the same firms that offer the 555. Examples are Motorola's MC3556 and Texas Instruments' TLC7556.

How the 555 works.

Figure 2 is a representative circuit schematic for the 555. It contains 21 transistors, 4 diodes, and 15 resistors. The voltage divider consisting of three 5000-ohm resistors (shown in Fig. 1) appears to the right of

Q10 in the trigger comparator. It applies one-third of the supply voltage to the non-inverting input terminal of the trigger comparator and two-thirds of the supply voltage to the inverting input of the IC's threshold comparator.

The output of the two comparators controls the R-S flip-flop, which in turn controls the states of the complementary output stage and the slave transistor Q6. The flip-flop's state can also be set by signals at RESET pin 4.

When organized as a monostable timer, the TRIGGER pin 2 is held high by external resistor R_T in series with the DC supply voltage. Under that condition, Q6 is saturated, shorting external timing capacitor C_D to ground, and OUTPUT pin 3 is driven low. Timer action is started by applying a negative-going trigger pulse to pin 2. As this pulse falls below one-third of the DC supply voltage, the output of the trigger comparator changes state. That causes the R-S flip-flop to switch, turning Q6 off, and driving OUTPUT pin 3 high.

As Q6 turns off, the short is removed from the external capacitor C_D . The capacitor charges through the external resistor R_D until the voltage across C_D rises to two-thirds of the supply voltage. Then the threshold comparator changes state and switches the R-S flip-flop back to its original state, turning Q6 "on" and rapidly discharging C_D . At the same time, OUTPUT pin 3 reverts to its low state. The *timing cycle* is then complete.

A characteristic of the 555 is that, once triggered, it cannot respond to additional triggering until the timing sequence is complete. However, the sequence can be aborted at any time by feeding a negative-going pulse to RESET pin 4.

The output pulse is a square wave whose duration (time delay) depends on the values of R and C. The formula for this is: t_D (time delay) = 1.1 (value of R × value of C)

Simply stated, time delay is directly proportional to the

TABLE 1—ELECTRICAL CHARACTERISTICS

Characteristics	Symbol	Min.	Typ.	Max.	Unit
DC Supply Voltage	V_{CC}	4.5	—	16	V
DC Supply Current ($V_+ = 5V$)	I_{CC}	—	3	6	mA
($V_+ = 15V$)		—	10	15	mA
Power Dissipation		—	—	600	mW
Threshold Voltage	V_{TH}	—	$\frac{2}{3}$	—	V
Trigger Voltage ($V_+ = 5V$)	V_T	—	1.67	—	V
($V_+ = 15V$)		—	5	—	V
Reset Voltage	V_R	0.4	0.7	1.0	V
Reset Current	I_R	—	0.1	—	mA
Timing Error (Monostable)		—	1	—	%
Frequency Drift with Temperature		—	50	—	ppm/°C
Drift with Supply Voltage		—	0.1	—	%/V
Output Rise Time	t_r	—	100	—	ns
Output Fall Time	t_f	—	100	—	ns

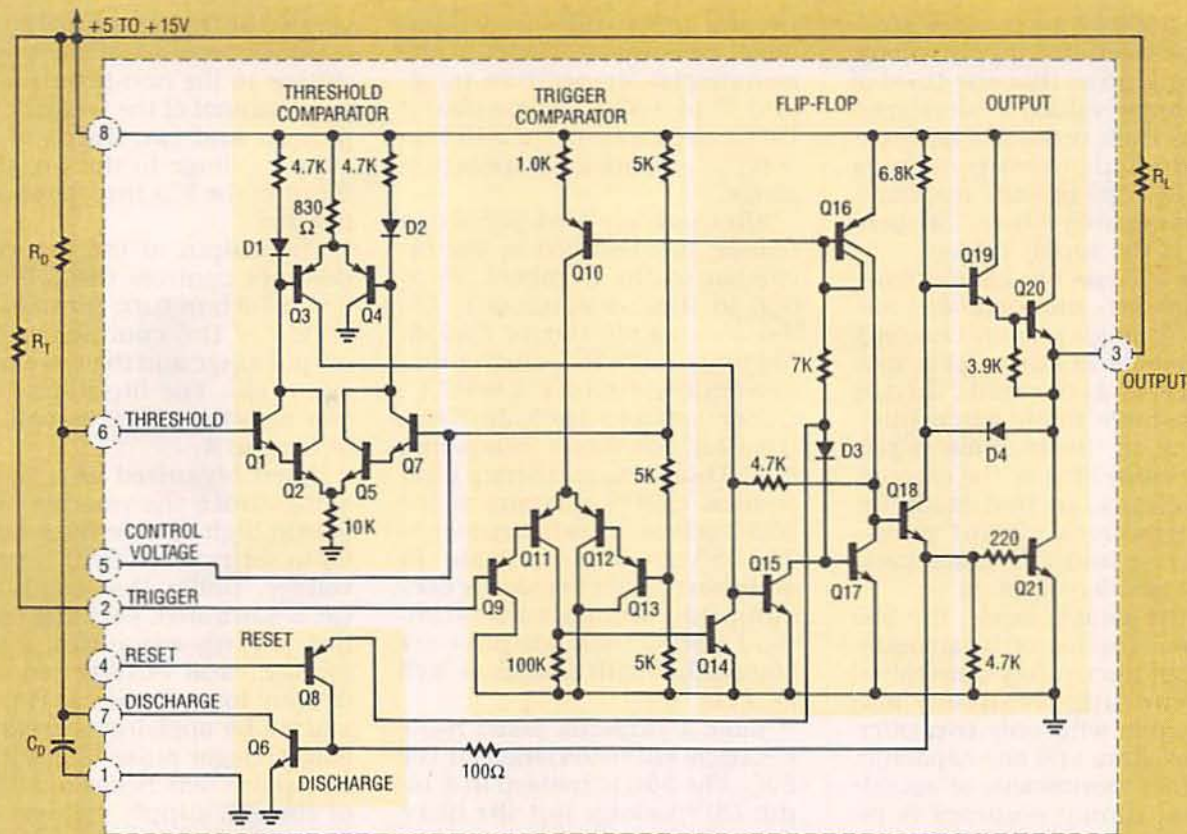


FIG. 2—REPRESENTATIVE CIRCUIT SCHEMATIC FOR A 555 timer with external resistive and capacitive components.

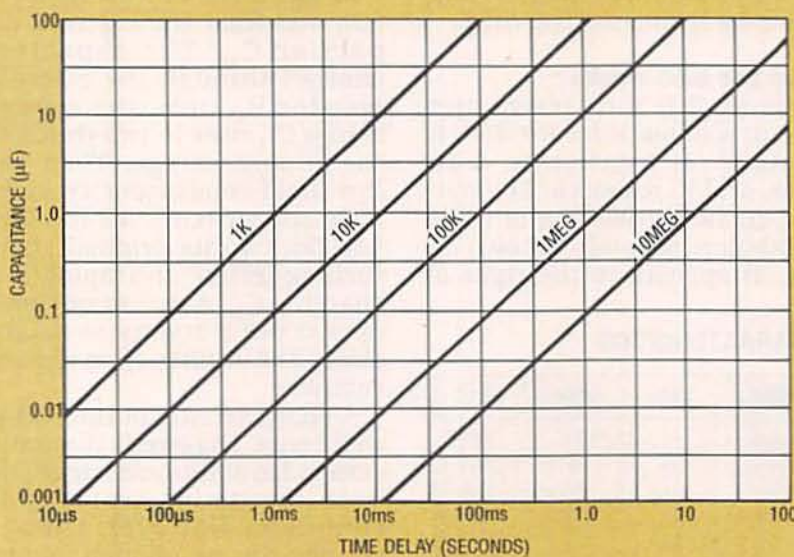


FIG. 3—COMBINATIONS OF RESISTANCE AND CAPACITANCE yield a range of time delays. The trigger pulse width must be less than the timing period.

product of R and C . Figure 3 is a plot of time delay vs. resistance and capacitance based upon the time-delay formula where t_D is in milliseconds, R is in thousands of ohms, and C is in microfarads. Figure 3 gives a

family of time delay curves with variations in R_T and C_T . Delays from 10 microseconds to 100 seconds can be obtained by selecting suitable values of low-leakage capacitors from 0.001 μF to 100 μF and resistors from

1 thousand ohms to 10 megohms.

Figure 4-a is a simple fixed-period (approximately 50-second) manually-triggered time delay circuit, and Fig. 4-b shows the waveforms as they would appear on an oscilloscope. The sequence of events in Fig. 4-b is initiated by grounding TRIGGER pin 2 with momentary START switch S1. The CONTROL VOLTAGE pin 5 is decoupled by C2, and the output state can be determined by observing whether LED1 is illuminated or not. A square output pulse (whose fixed-period is determined by R_1 and C_1) appears at OUTPUT pin 3, while an exponential sawtooth (with the same period as the square wave) appears at DISCHARGE pin 7.

The fixed-period output of the circuit in Fig. 4 can vary from 1.1 to 120 seconds by making the changes shown in Fig. 5. Resistor R_1 is replaced with a 10K fixed resistor and 1-megohm potentiometer R_5 in series, as shown. A reset feature can be added by installing RESET switch S2, permitting

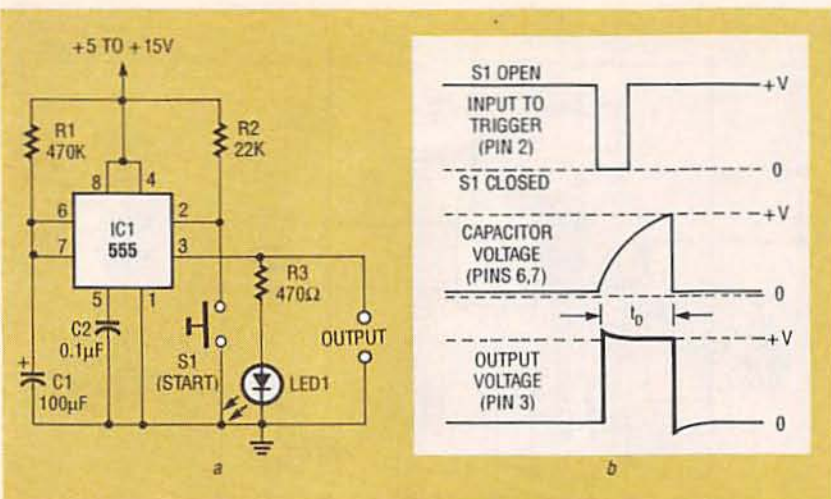


FIG. 4—FIXED-PERIOD TIMER produces a 50-second time delay (a). The waveforms at three pins are shown (b + a).

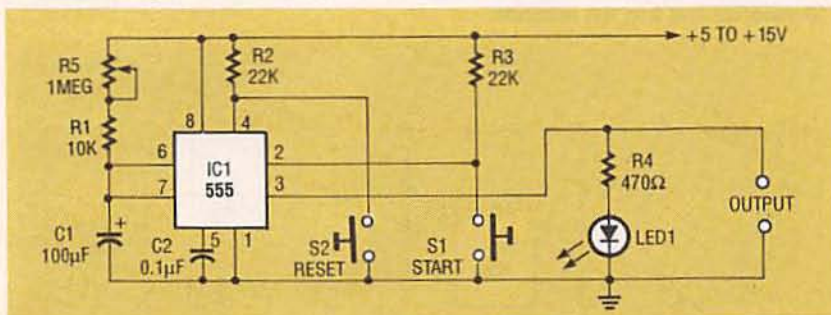


FIG. 5—VARIABLE-PERIOD TIMER CIRCUIT with reset capability produces time delays from 1.1 to 120 seconds.

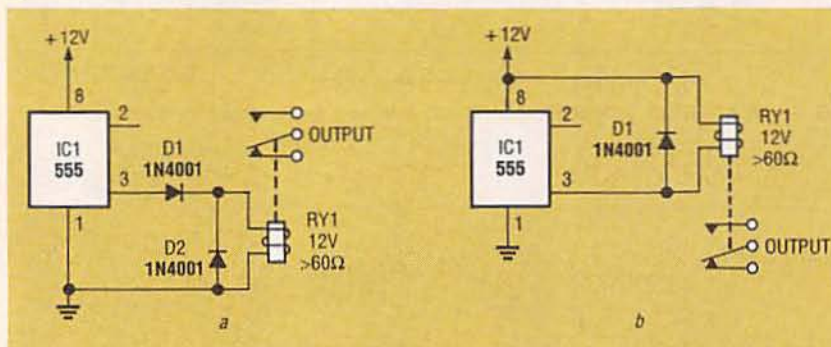


FIG. 6—ALTERNATE METHODS FOR ENERGIZING a relay from the output of a 555.

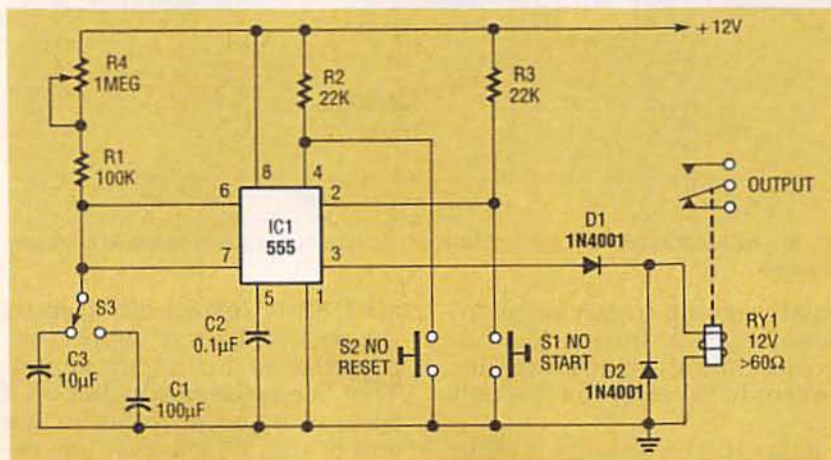


FIG. 7—TIMER WITH A RELAY OUTPUT provides time delays of 1.1 to 120 seconds.

premature termination of the timing period.

The 555 timer can drive non-inductive loads directly from pin 3 with currents as large as 200 milliamperes. However, if the circuit contains an inductive relay load, either of the schematics shown in Fig. 6 apply. In Fig. 6-a, the relay RY1 is normally off, but it goes on only when OUTPUT pin 3 goes high during the timing interval; in Fig. 6-b, RY1 is normally on, but it turns off during the timing interval. Diode D1 in both circuits protects the 555 against inductive-switching damage. The contacts of relay RY1 can control external circuits.

Figure 7 shows how a relay and a 555 can form a simple 1.1- to 120-second timer in two switch-selected decades. However, the general-purpose circuit has several drawbacks. First, it draws current continuously, even when the timer is off. Second, because of the wide tolerance variations in the electrolytic timing capacitors C1 and C2, potentiometer R4 needs two custom calibrated scales.

The schematic in Fig. 8 shows how to overcome these drawbacks. The RESET switch S2 and the set of relay contacts in parallel with the START switch S1, which are both normally open (N.O.) keep the circuit off so there is no current drain. The timing cycle is started by pressing momentary pushbutton switch S1, which connects power to the 555. At the instant of S1 closure, C3 is fully discharged. It therefore sends a start pulse to TRIGGER pin 2 through R4 and initiates a timing cycle.

As the timing cycle starts, RY1 is energized. The contacts in parallel with S1 close and keep the 555 powered even when S2 is released. At the end of the timing cycle RY1 is de-energized and its contacts re-open, disconnecting power from the 555.

The timing of the circuit in Fig. 8 is principally controlled by the values of resistor R1 and potentiometer R5, and either C1 or C2, which are switch-selected by S3-a. Note, however,

that timing is also influenced by the setting of potentiometers R6 and R7. They are selected with switch S3-b and connected to CONTROL voltage pin 5 of the IC. Those potentiometers effectively shunt the internal voltage of the 555, thereby altering timing periods.

That feature allows the circuit to produce precise timing periods even when capacitors with loose-tolerance values are in the circuit. It also allows a single calibrated timing scale to cover the two switch-selected timing ranges.

To set up the Fig. 8 circuit, first set potentiometer R5 to its maximum value, set switch S3 to position 1 and push START button S1. Then adjust potentiometer R6 for a precise period of 10 seconds. Next, set 3 to position 2, push START switch S1, and adjust potentiometer R7 for a precise period of 100 seconds. With those adjustments complete, the timing scale can be calibrated over its full 100-second range.

Timers for car lights

Figure 9 is a circuit that automatically delays the turn-off of an automobile's headlights, permitting them to function as safety lights at night after the ignition switch is turned off. It is a useful circuit if you want your car's headlights to remain on for 50 seconds after you have parked, turned off the ignition, locked the doors, and walked away. The headlights will stay on long enough to illuminate your route until you can reach the safety of your home. The circuit does not interfere with normal headlight operation.

When the car's ignition switch S2 is turned "on," RY1 is energized (through diode D3) closing its contacts and connecting the 12-volt battery to the 555 and headlights switch S1. In this state the headlights operate normally. However, because both sides of capacitor C2 are connected to the positive supply, it is fully discharged.

When S2 is turned "off," the voltage across R3 goes to zero, de-energizing the relay. However, at that time C3 applies a

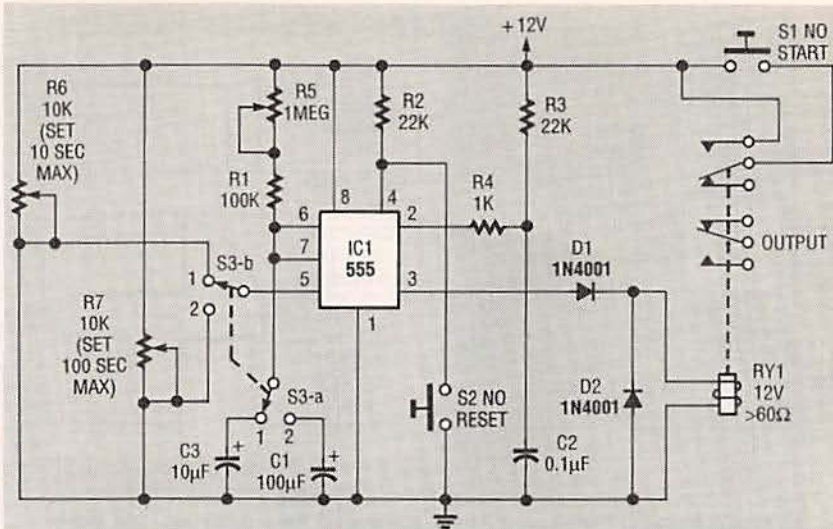


FIG. 8—PRECISION (COMPENSATED) TIMER with a relay output has two ranges: 0.9 to 10 seconds and 9 to 100 seconds.

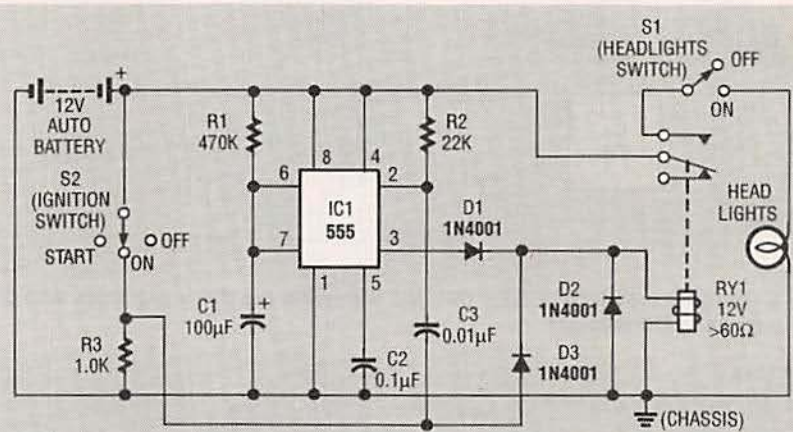


FIG. 9—HEADLIGHT TURNOFF CONTROL with automatic delay for automobiles.

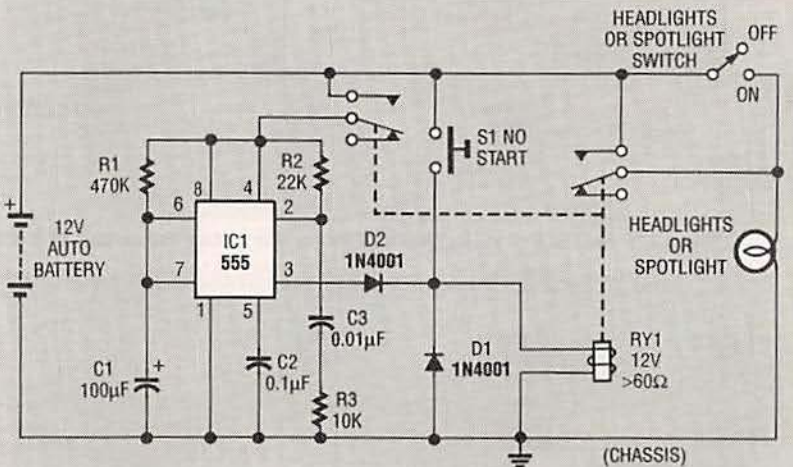


FIG. 10—HEADLIGHT/SPOTLIGHT TURNOFF CONTROL for automobiles is manually actuated.

negative-going trigger pulse to TRIGGER pin 2, initiating a 50-second timing cycle that applies current to the relay coil through D1.

Relay RY1's contacts remain closed for about 50 seconds

after S2 is turned off, keeping the positive battery supply connected to S1 during this period. That keeps the headlights on if S1 is in its on position. At the end of that 50-second time delay, RY1 de-energizes, its con-

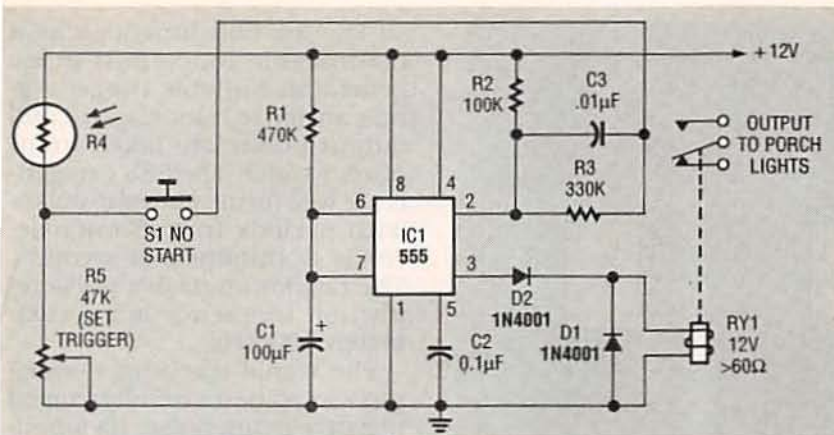


FIG. 11—PORCH LIGHT CONTROL AUTOMATICALLY turns on a light for a preset period only when triggered at night.

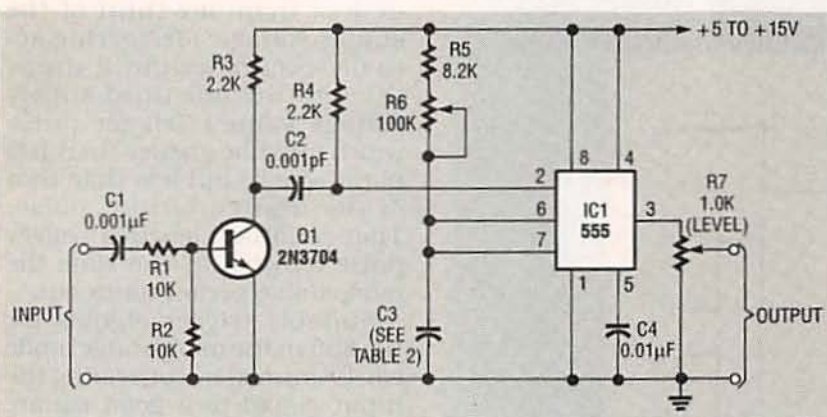


FIG. 12—ADD-ON PULSE GENERATOR can supplement a stand-alone pulse generator. It is triggered by rectangular input signals. Table 1 gives output pulse widths for various values of C3.

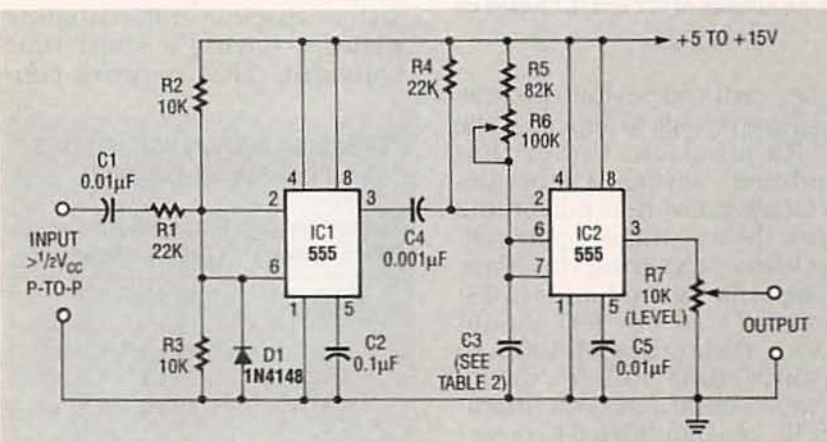


FIG. 13—MODIFIED ADD-ON PULSE GENERATOR can be triggered by any kind of input waveform including sine waves.

tacts open, and battery supply is disconnected from the 555 and S1.

The circuit in Fig. 9 is compatible with modern practice for powering the headlights switch S1 with ignition switch S2 so that headlights work only when the ignition switch is on. How-

ever, the circuit shown in Fig. 10 is applicable to older vehicles whose headlights or spotlight are independent of the ignition switch. The circuit illustrates a manual delayed turn-off light control.

That circuit works if the vehicle is parked with its lights off.

They will be turned on for a preset 50-second period as soon as momentary pushbutton START switch S1 is pressed. When the delay period times out, the lights will be turned off again automatically.

The Fig. 10 circuit includes relay RY1 with two sets of normally-open contacts. The timing sequence is started with the momentary closure of pushbutton switch S1. Normally, both S1 and the relay contacts are open, so the timer circuit is not powered and the lights are off. Capacitor C3 is discharged under this condition.

When S1 is momentarily closed, RY1's coil is energized. That action closes its first set of contacts, applying power to the car's lights while also closing its second set of contacts, applying power to the 555. However, TRIGGER pin 2 of the IC is briefly grounded through C2, so a negative trigger pulse is fed to it, and a timing cycle is begun.

Consequently, OUTPUT pin 3 of the 555 switches high when the relay contacts close, locking the relay into its "on" state (regardless of the subsequent state of S1), keeping the lights on for 50 seconds. At the end of the timing cycle, pin 3 of the IC switches to its low state, de-energizing RY1. Then both sets of relay contacts open, disconnecting power from the 555 and the lights.

Automatic porch light

Figure 11 is an automatic control circuit for a porch light. It will turn a porch light on automatically for a preset 50-second period when its sensor detects the presence of a person. However, it performs that function only at night or under conditions of reduced visibility such as might occur during a storm. The circuit is activated with switch S1, which can be a microswitch triggered by a porch gate. It might also be a pressure-switch hidden under a porch mat and triggered by a person weighing perhaps 50 pounds or more.

Circuit operation depends on a negative-going pulse that falls below the internally controlled

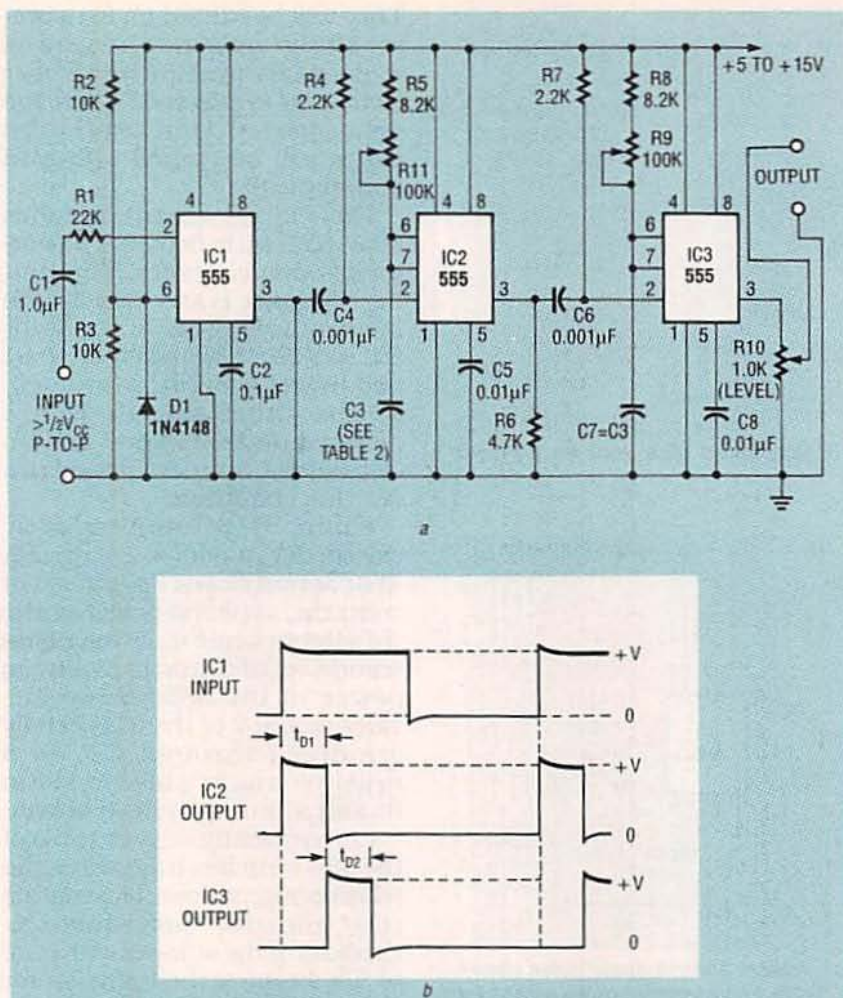


FIG. 14—ADD-ON DELAYED PULSE GENERATOR can be triggered by any input waveform (a). Waveforms at input to IC1 and those at the outputs of IC2 and IC3 based on different values of R and C (b).

one-third supply voltage being fed to TRIGGER pin 2 of the 555. If the trigger pulse does not fall below that value, the timing cycles cannot be initiated.

In Fig. 11, the photocell (resistor R4) and potentiometer R5 are in series as a light-dependent voltage divider. One side of S1 is connected to the junction between R4 and R5, and the other side is connected to pin 2 through a network of C2 and R3. In normal daylight the photocell's resistance is low, so a high voltage appears at the junction of R4 and R5. As a result, closing S1 sends a voltage pulse to pin 2 whose value is too low to pull pin 2 below one-third of the supply voltage. Thus, the timer cannot be triggered with S1 under those conditions.

However, the photocell's resistance value increases at night or

under reduced visibility, causing a low voltage to appear at the R4-R5 junction. Under that condition, closing S1 generates a voltage pulse that pulls pin 2 below the one-third supply voltage value, triggering the timer.

The cadmium-sulphide (CdS) photocell (resistor R4) should have a resistance of 1000 to 47,000 ohms under "dark" turn-on conditions. Potentiometer R5 can be adjusted to preset the minimum "dark" level for circuit triggering. The trigger signal is fed to pin 2 of the 555 through the C3 and R3, a network that shapes the trigger pulse and effectively isolates the DC component of the photocell-potentiometer network from pin 2.

Pulse generators

In all of the circuits presented

so far, the 555 functions as a monostable (one-shot) pulse generator. Suitable trigger signals are fed to TRIGGER pin 2 and output pulses are taken from OUTPUT pin 3. The 555 can generate well formed output pulses with periods from 5 microseconds to hundreds of seconds. The maximum usable pulse repetition frequency is approximately 100 kHz.

The signal reaching TRIGGER pin 2 must be a carefully shaped negative-going pulse. Its amplitude must switch from an "off" value greater than two-thirds of the supply voltage to an "on" value less than one-third of the supply voltage. (Triggering actually occurs as pin 2 drops through the one-third supply voltage value.) Trigger pulse width must be greater than 100 nanoseconds but less than that of the desired output pulse. That condition assures trigger pulse removal by the time the monostable period times out.

Suitable trigger signals for the 555 in the monostable mode can be formed by converting the input signal to a good square wave that switches between the full positive supply voltage and ground. The square wave is then coupled to pin 2 with a resistor-capacitor differentiating network having a short time constant. That network con-

TABLE 2—CAPACITOR VALUES FOR PULSE-WIDTHS

Capacitors C3 (Microfarads)	Pulse Width Range (Time in Seconds)
10.0	90 ms - 1.2
1.0	9 ms - 120 ms
0.1	900 μ s - 12 ms
0.01	90 μ s - 1.2 ms
0.001	9 μ s - 120 μ s

verts the leading or trailing edges of the square wave into suitable trigger pulses.

Figure 12 shows a timing circuit that accepts input signals already in the form of square waves or pulses. Transistor Q1 converts a rectangular input signal into a form that switches between the positive supply and ground. The output signal is

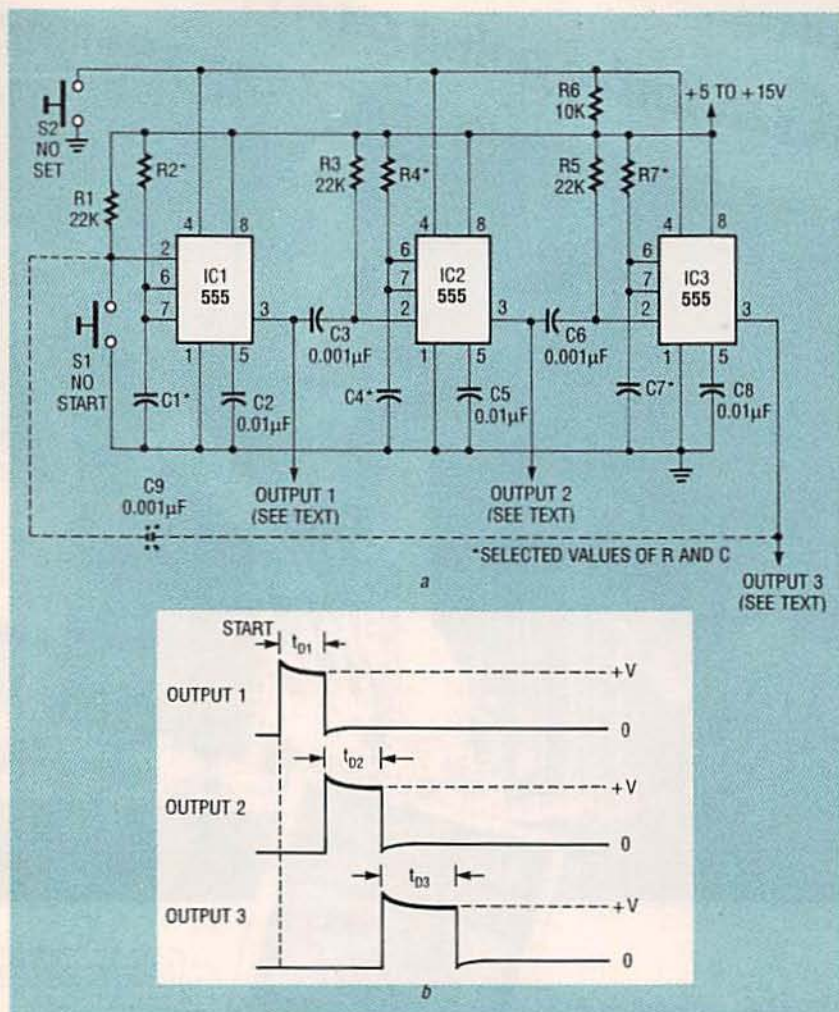


FIG. 15—THREE-STAGE SEQUENTIAL TIMER or pulse generator (a) and waveforms at three different output pins (b).

then fed to TRIGGER pin 2 through differentiating network C2-R4. The circuit can become an add-on pulse generator in combination with a separate square-wave or pulse generator. Variable-amplitude output pulses can be obtained from potentiometer R7.

The output pulse widths of the Fig. 12 circuit can be varied over more than a decade range with potentiometer R6, and they can be switched in overlapping decade ranges with the values of C3 listed in Table 2. With the component values shown, output pulse width is variable from 9 microseconds to 1.2 seconds. Capacitor C4 decouples CONTROL VOLTAGE pin 5 to improve circuit stability.

Figure 13 shows a modification of the circuit in Fig. 12 that can be triggered by any kind of input waveform, including sine

waves. Here the first 555 (IC1) is configured as a Schmitt trigger to convert all input signals into square-wave output signals. Those square waves trigger the second 555 (IC2) in the monostable mode in the same way as described earlier. The circuit can also become an add-on pulse generator in combination with any kind of stand-alone waveform generator that produces output signals with peak-to-peak amplitudes greater than one-half the IC's supply voltage.

Figure 14-a shows how two monostable circuits can be connected in series to make a delayed-pulse generator. As in Fig. 13, the first 555 (IC1) is configured as a Schmitt trigger. The second 555 (IC2) controls time delay width, while the third 555 (IC3) determines the output pulse width.

As shown in Fig. 14-b, the output pulse at pin 3 of IC3 appears at a time interval after the initial application of the trigger signal. This time delay width T_{D1} is determined by the product of the value of capacitor C3 and the sum of the values of resistor R5 and potentiometer R6, in accordance with the time delay formula given earlier. Similarly, output pulse width t_{D2} is determined with the values of C7, and R8 and R9.

This circuit can become part of a stand-alone pulse delay generator by building it into a square-wave generator case. The square-wave generator will provide the initial trigger signals needed.

A number of monostable pulse generators can be placed in series to operate in sequential form. Figure 15-a, for example, shows a three-stage sequential generator circuit. It can control lamps or relays in a pre-programmed time sequence after pushbutton switch S1 is pressed to give the START command. Note that the RESET pins (pin 4) of all three 555's are shorted together and positively biased by R6. Those pins can be shorted to ground with SET switch S2. When power is applied, S1 should be closed, ensuring that none of the 555's in the circuit are falsely triggered.

Figure 14-b shows the waveforms from the output pins of all three 555's (IC1 to IC3). The time delay t_{D1} is determined by the values of C1 and R2, t_{D2} is determined by the value of C4 and R4 and t_{D3} is determined by the values of C7 and R7 when inserted in the time delay formula given earlier.

Finally, three or more monostable circuits can be connected with capacitor C9 (shown in a dashed connection line) between S1 and pin 3 of the third 555 (IC3). This loop feeds a signal back from the output pin of IC3 to the input TRIGGER pin of IC1, permitting infinite repetition of pulse sequence. The circuit can drive LED's and digital logic. The circuit also has the reset capability provided by S2 that clears the circuit when power is first applied.

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Set up a versatile sloping-vee antenna for your shortwave receiver or ham rig to improve your transmission and reception at low cost.

SLOPING V ANTENNA

RICHARD A. FORMATO

THE SLOPING-VEE ANTENNA IS ONE of the most versatile broadband antenna designs available to amateur radio enthusiasts and shortwave listeners. It is structurally simple, inexpensive, easy-to-build, and easy to set up in the field if you want to take your rig with you on vacation. The sloping vee can achieve moderate and occasionally even high gain over a frequency span of 5 to 1, 10 to 1, or more. The antenna is functional over the high-frequency (HF) into ultra-high-frequency (UHF)-range from about 3 MHz to about 800 MHz.

The most common configuration for the sloping-vee antenna is shown in Fig. 1. It consists of two sloping, radiating elements (wires) fed by a radio-frequency source at their vertex. The source is located at a height H above the ground, and the elements are terminated by two equal resistors, R , located at or

near the Earth's surface. Technically it is an *inverted-vee* sloping antenna.

The *true* sloping-vee antenna has a vertex height, H , that is actually less than the height of its terminations. The radiating elements slope up from the ground, not down as shown in Fig. 1, making this configuration more difficult and expensive to build because two masts are required. However, both forms are called sloping vee's because they resemble a tilted letter "V."

This article presents a systematic design procedure that takes into account the unique characteristics of this antenna. A typical design for an HF/VHF 10- to 60-MHz sloping-vee antenna is discussed in detail, and measured performance data for the actual antenna is given. A frequently overlooked feature of the sloping-vee antenna at HF and a major advantage is that it combines the features of horizontal and vertical antennas, which results in virtual polarization diversity.

In a careful design, the characteristics of the communi-

cation links to be supported by the antenna must be considered. For example, the take-off angles at which the antenna must have adequate gain are determined by the transmitter-to-receiver distance and by the virtual ionospheric reflection height.

Another design constraint is the antenna's required bandwidth which is determined by the operating frequencies. For some amateur radio operators, only the HF band (3 to 30 MHz) is of concern; others want to cover the upper HF range and the 6-meter (50 kHz) band as well. High-gain antennas such as Yagis exhibit a bandwidth of a few percent of the center frequency. A well designed sloping vee, by contrast, will cover the entire HF spectrum and even exceed it.

Antenna siting is another important consideration in the design of a sloping vee. From HF well into the VHF range, the Earth's electrical characteristics (ground conductivity and dielectric constant) have a dramatic effect on antenna performance. Ground effects are especially important at low take-off angles (close to the horizon).

Shallow take-off angles are necessary for long-range transmission. For very long distances, the take-off angle could

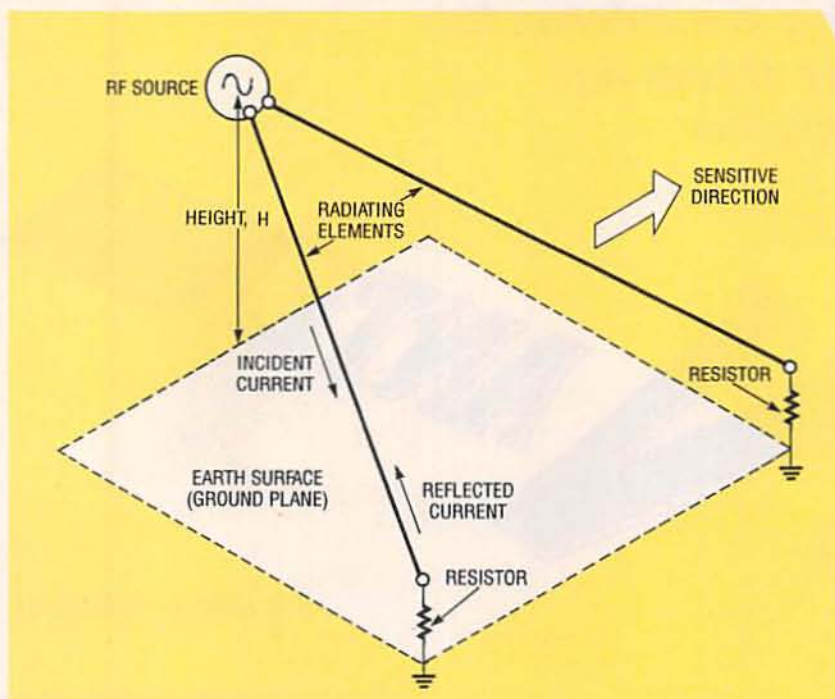


FIG. 1—A SLOPING-VEE ANTENNA is simple, inexpensive to build and erect, and provides excellent broadband performance from HF well into VHF.

be so low that mountains or other terrain features block signal transmission. Those obstructions limit the minimum take-off angle which, in turn, limits the range.

Sloping-vee operation

As shown in Fig. 1, the RF source excites current waves on the vee's radiating elements. The total current consists of two components: an incident wave propagating from the source toward the end of the element, and a reflected wave propagating from the terminating resistor back toward the source. In an ideal vee, the reflected component is zero because the terminating resistor absorbs any incident energy that would otherwise be reflected. In practice, there is a only a slight reflected component. The incident and reflected waves combine point-by-point along the element length to form a weak standing-wave pattern. An unterminated antenna, such as a center-fed, half-wave dipole, propagates a reflected wave with a large amplitude that creates a strong standing-wave pattern.

The half-wave dipole is a resonant, narrow band, standing-wave antenna. By contrast, a

properly designed vee is a non-resonant, broadband, traveling-wave antenna. Broadband operation is obtained from the vee antenna by eliminating as much of the reflected current wave as possible. The terminating resistors are capable of absorbing most of the incident energy that is not radiated from the elements. If the terminating resistor is conjugate-matched to the characteristic impedance of the radiating element, there is no reflected signal because all of the power is absorbed.

This situation is the same as the maximum power transfer condition for a transmission line feeding a load. The load absorbs maximum power when its internal impedance is equal to the complex conjugate of the transmission line's characteristic impedance Z_0 . Because Z_0 for well-designed transmission lines is nearly a pure resistance, the matched load is a resistance of equal value. The most common coaxial cable impedance is 50 ohms, and the corresponding matched load is a resistive 50 ohms. The load could be a 50-ohm dummy (essentially a resistor), or it could be an antenna with an input impedance of $50 + j0$ ohms.

The frequencies at which the vee exhibits near traveling-wave behavior determine its useful bandwidth. The precise definition of *impedance bandwidth* is the range of frequencies at which antenna input voltage standing-wave ratio (VSWR) is less than or equal to some threshold value, typically 2 to 2.5:1 for transmitters and up to 5:1 for receivers. There are different thresholds because transmitter circuits cannot tolerate high VSWR without reducing output power or shutting down; by contrast, a receiver is not limited by VSWR.

For receive-only operation, increased antenna VSWR causes higher mismatch loss into the receiver front-end, which reduces the available signal level. There is a point at which the mismatch loss is so high that receiver sensitivity (minimum detectable signal) becomes unacceptable low. Figure 2 is a plot of mismatch loss as a function of VSWR with one end of the transmission line matched. At a VSWR of 5:1, receiver sensitivity is reduced by only 2.5 dB; but at 21:1, the reduction approaches 8 dB.

An objective for the design of a vee antenna is to maximize the range of frequencies in which VSWR is less than 2.5:1 for transmission and less than 5:1 for reception. An antenna meeting the transmission criterion between 3.5 and 30 MHz, for example, could be loaded directly on all bands from 80 to 10 meters without a tuner or matching network! The same antenna could receive over an even wider bandwidth.

Design procedure

The design of a good vee involves three steps. The first is to evaluate the kinds of communication links for which the antenna is intended. The designer must answer the following questions: What are the distances and operating frequencies involved, and what is the propagation mode? The second step calls for the selection of the vee's apex angle based upon the intended operating frequency and antenna size. The third

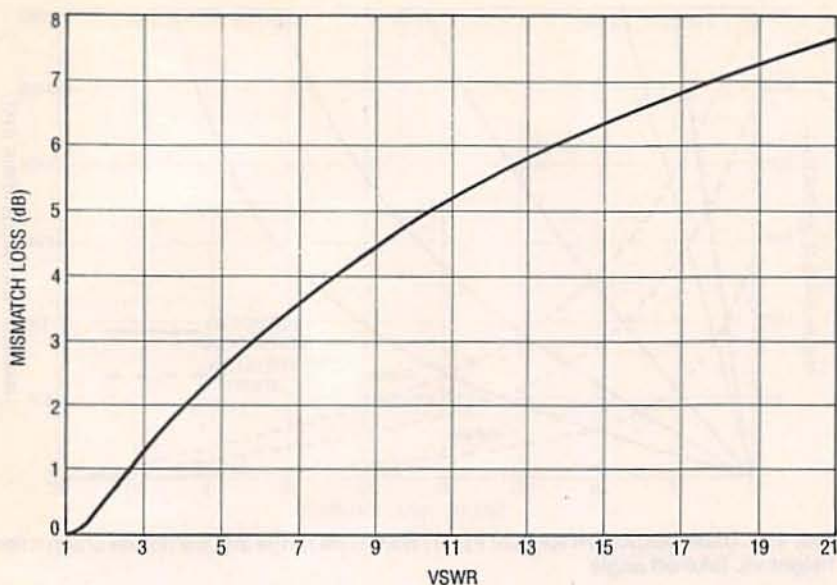


FIG. 2—PLOT OF MISMATCH LOSS in decibels vs. VSWR with one end of the transmission-line matched.

step is the computation of the antenna radiation patterns for the desired distances.

The assumed specifications for the design of a vee antenna are:

- Frequency range—15 to 50 MHz (continuous)
- Propagation mode—meteor trails at 100 kilometers
- Link distances—400 to 1200 kilometers (250 to 750 miles)
- Antenna siting—limited to an area 100 × 100 feet and a height 25 feet
- Main lobe gain—0 dBi, minimum value

Step 1—Link evaluation

Three transmission-path factors influence vee design: distance between transmitter and receiver (determines antenna take-off angles); operating frequencies (determines required bandwidth); and propagation mode (determines take-off angles). Each of those factors must be known or estimated to design an antenna matched to the path.

Signals propagating between points on the Earth's surface are bent by the ionosphere or other scattering mechanism such as a meteor reflection. The most common (but not the only) propagation mode at HF is the skywave. The transmitted signal is bent back toward the Earth's surface by the ionosphere's

changing refractive index. This process is equivalent to a specular reflection from a virtual reflection point. The simplest

model of HF skywave propagation is a straight-line signal ray from the transmitter to a location near the reflection point where it is bent back as another straight line ray from the reflection point to the receiver as shown in Fig. 3.

The attainable distance in a communication path depends, in part, on the reflection height, with higher reflections providing greater distances. HF skywave propagation is caused by reflections from the ionosphere's layers: D layer (about 50 kilometers high), E layer (about 120 kilometer high) and F layer (200 to 500 kilometers high). Meteor-trail reflections are of growing interest because of the increased availability of high-speed packet data equipment. Those reflections occur at altitudes of about 100 kilometers.

The path geometry (reflection height and transmitter-to-re-

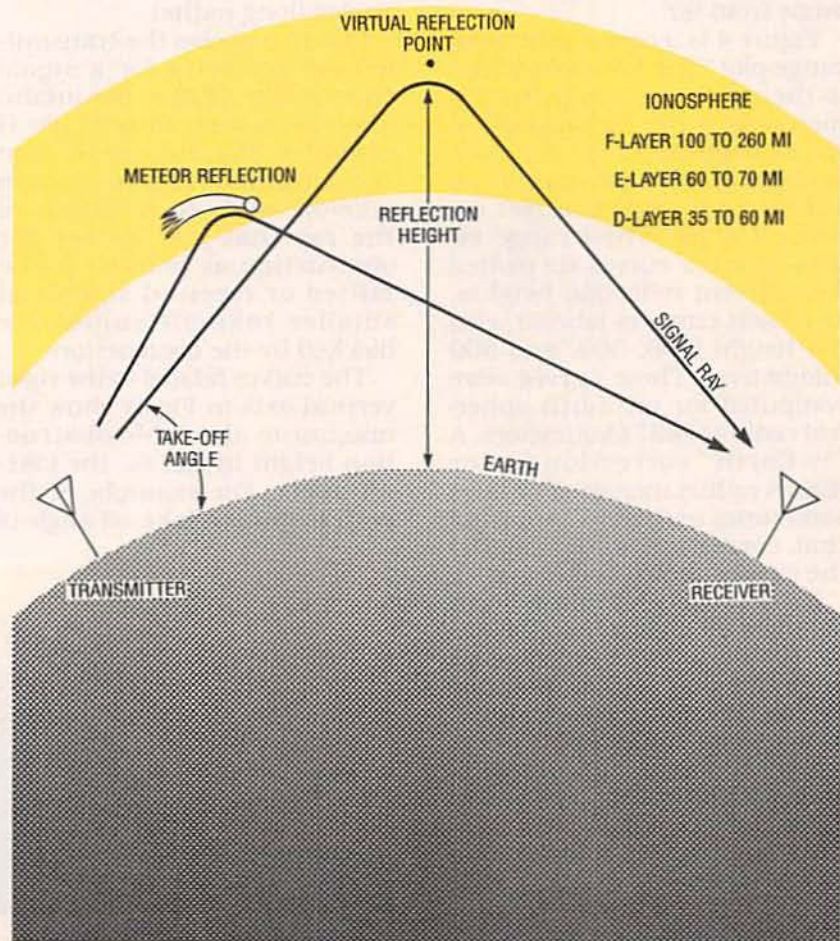


FIG. 3—DIAGRAM SHOWING RELATIONS between take-off angle, virtual reflection point, and signal range.

veiver distance) determines the range of required take-off angles for the antenna. Signal rays transmitted at too high an angle fall short of the receiver, while those transmitted at too shallow an angle can overshoot the receiver.

Figure 3 shows two important angles in vee design. The take-off (or elevation) angle is measured upward from the earth's surface to the ray direction. The polar (or zenith) angle is measured down from the vertical to the ray direction. Both angles are important because path requirements are usually described in terms of the take-off angle, but antenna performance is usually referred to a coordinate system based on the polar angle. The sum of the polar angle and the take-off angle is 90° , so the polar angle can always be determined by subtracting the take-off angle from 90° and the take-off-angle can be found by subtracting the polar angle from 90° .

Figure 4 is a communication-range plot. The left vertical axis is the maximum range in kilometers for a specific take-off angle in degrees, while the right vertical axis is the maximum obstruction height in feet vs. take-off angle. Three range vs. take-off angle curves are plotted for different reflection heights, and each curve is labeled with the height (100, 300, and 500 kilometers). These curves were computed for an Earth spherical radius of 6371 kilometers. A "1/3-Earth" correction factor (Earth radius increased by 1/3) is sometimes used at HF. Applying that correction would modify the curves shown somewhat.

Either the maximum path distance for a given take-off angle or the appropriate take-off angle for a specified distance can be determined from Fig. 5. At a take-off angle of 20° , for example, the maximum range is about 2100 kilometers (1300 miles) for 500-kilometer reflections in the F2 region. The range increases to 4000 kilometers (2500 miles) at about a 5° take-off angle.

If the path length were 3200 kilometers, the appropriate

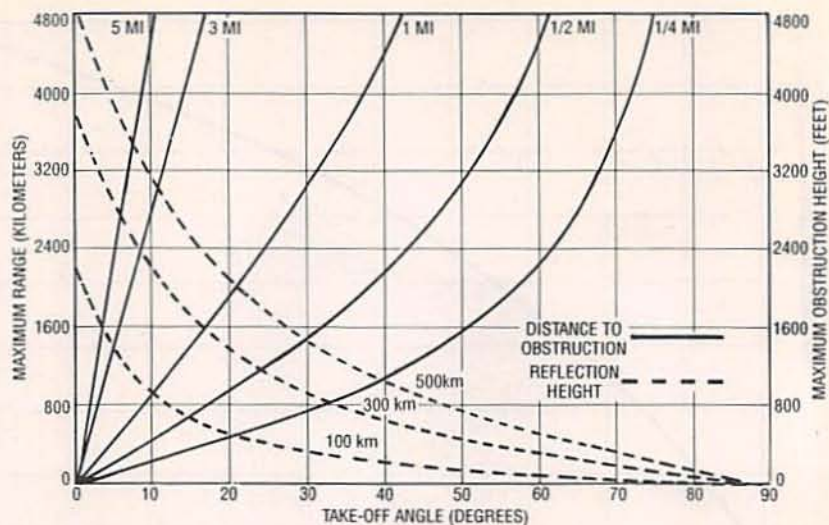


FIG. 4—COMMUNICATION RANGE PLOT: maximum range and maximum obstruction height vs. take-off angle

take-off angle for 500-kilometer reflections is about 10° , and it's about 3° for 300-kilometer reflections. Also plotted in Fig. 5 is a family of five obstruction height curves. They are important in antenna siting, especially for very shallow take-off angles (long paths).

Figure 5 shows the transmitted-ray geometry for a signal obscured by a hill or mountain. The obstruction with height H is located at a distance R from the antenna. The minimum take-off angle corresponds to the ray that just grazes the obstruction as shown. Transmitted or received signals at smaller take-off angles are blocked by the obstruction.

The curves related to the right vertical axis in Fig. 4 show the maximum allowable obstruction height in feet vs. the take-off angle. For example, if the path requires a take-off angle of

20° , a land-mass or structural obstruction $1/4$ mile away must be less than 500 feet high if the ray is to pass without being blocked. A 500-foot hill $1/4$ mile away would obscure all signals with take-off angles below 20° . Higher obstructions can be tolerated if they are further away. At a distance of $1/2$ mile, for example, the obstruction could be as high as 1000 feet before obscuring a ray with a 20° take-off angle.

The curves in Fig. 4 also show maximum range in kilometers vs. take-off angles in degrees for the vee. For 100-kilometer reflections, the most effective angles are between about 8° and 25° . The objective in designing a vee antenna is the placement of this lobe in this angular range. The 8° minimum take-off angle requires that the antenna be carefully sited to avoid lobe blockage by a nearby

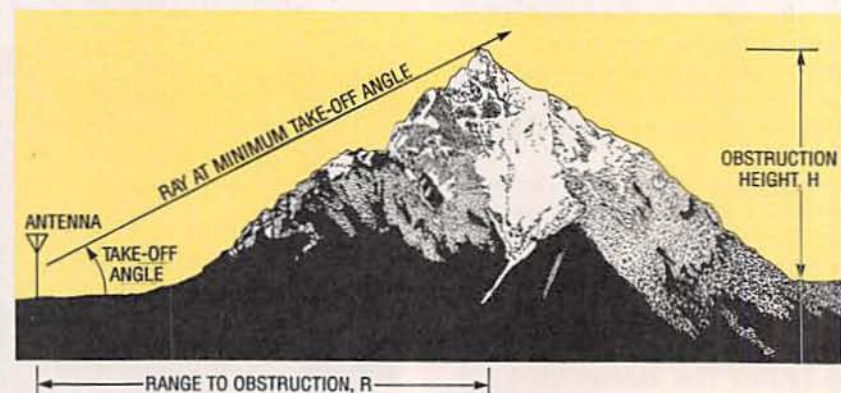


FIG. 5—DIAGRAM SHOWING MINIMUM TAKE-OFF angle to avoid a nearby signal-blocking obstruction.

hill or structure. The maximum height of that obstruction can be only about 200 feet if the antenna is to be located $\frac{1}{4}$ mile away. This requirement might easily be exceeded in hilly terrain or near tall buildings.

Step 2—The apex angle

Figures 6 and 7 plot the optimum vee apex angle in degrees as it changes with frequency and antenna element (radiator) length. The apex angle is inversely related to both frequency and element length. Thus, short elements at low frequencies must have wide apex angles while long elements at high frequencies can have small angles. The curves in Fig. 6 are for frequencies of 10, 30, and 50 MHz with respect to element lengths in meters, while those in Fig. 7 are for element lengths of 20, 40 and 60 meters with respect to frequency. Our example vee must operate over a wide frequency range (15 to 50 MHz).

It turns out that a given apex angle is optimum at only one frequency, not over a range of frequencies. Therefore, the selection of an optimum apex angle calls for both judgment and compromise. The objective is to select an angle that provides good performance at all frequencies over the stated range.

The design example calls for a vee antenna that will fit in a 100×100 foot square plot. Therefore, 40- or 60-meter elements are too long; only the 20-meter length will fit. By referring to both Figs. 6 and 7, it can be seen that for a 20-meter element the optimum apex angle at 10 MHz is 116° , but at 50 MHz it is 54° . It can also be seen that a good compromise for apex angle with a 20-meter element over the 15- to 50-MHz band can be reached by finding the apex angle for 30 MHz— 69° . That angle will now become the trial value, and it will be retained unless the gain or pattern fails to meet the design objectives. In that case, the selection process must be repeated with another choice for the apex angle.

Now look at the vee input resistance at the design apex angle. Figure 8 is a plot of input

resistance in ohms (R_{in}) vs. frequency for apex angles of 40° , 70° , and 100° . The input resistance value for a 70° apex angle at 30 MHz is about 690 ohms. (The vee is generally considered to be a 600-ohm antenna, so this is close to a match). The value of input resistance increases to 780 ohms at 15 MHz but drops to 630 ohms at 50 MHz. For design purposes, 690 ohms can be selected as a representative average value of R_{in} over the 15- to 50-MHz band.

The value of R_{in} is needed to specify the vee input balun. Because the vee is a balanced radiating system, feeding it with an

unbalanced coaxial cable requires a balun (a balanced to unbalanced transformer). Matching a 50-ohm transmitter to 690 ohms requires a 14:1 balun, which can be made by winding magnet wire on a ferrite core or purchasing the component complete.

A value for R_{in} is also needed in the specification of each terminating resistor. Those values are $R_{in}/2$ (345 ohms for the design example). Select the standard value closest to 345 ohms. That value is not critical because R_{in} changes with frequency.

The tentative geometry for the

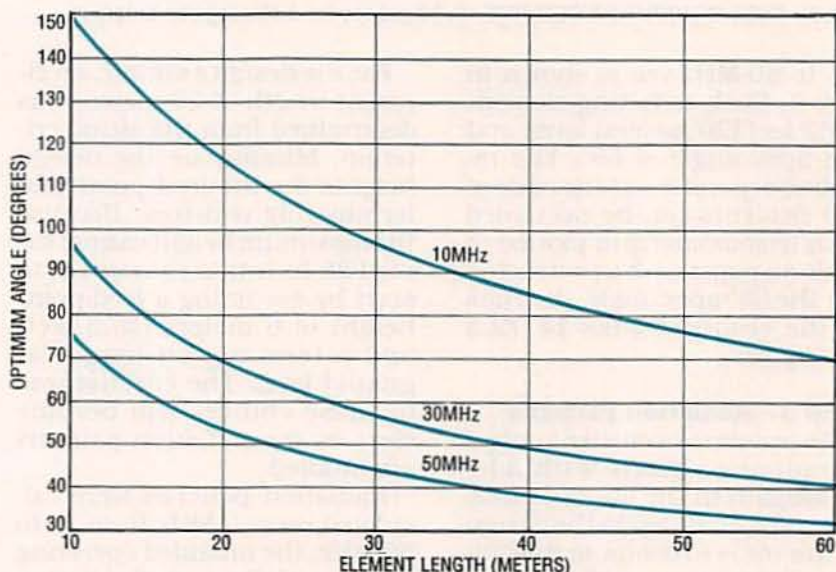


FIG. 6—OPTIMUM APEX ANGLE for sloping-vee antenna: plot of optimum angle vs. element length at three different frequencies.

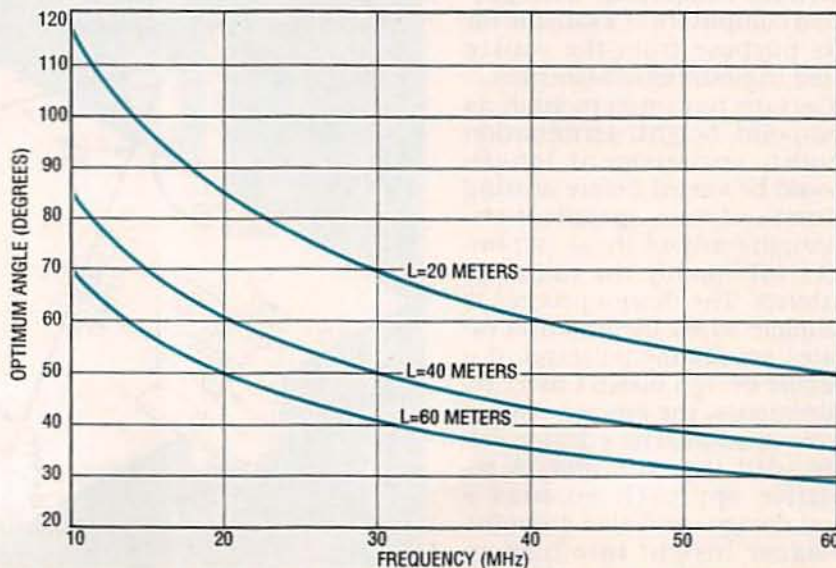


FIG. 7—OPTIMUM APEX ANGLE for sloping-vee antenna: plot of optimum angle vs. frequency for three different element lengths.

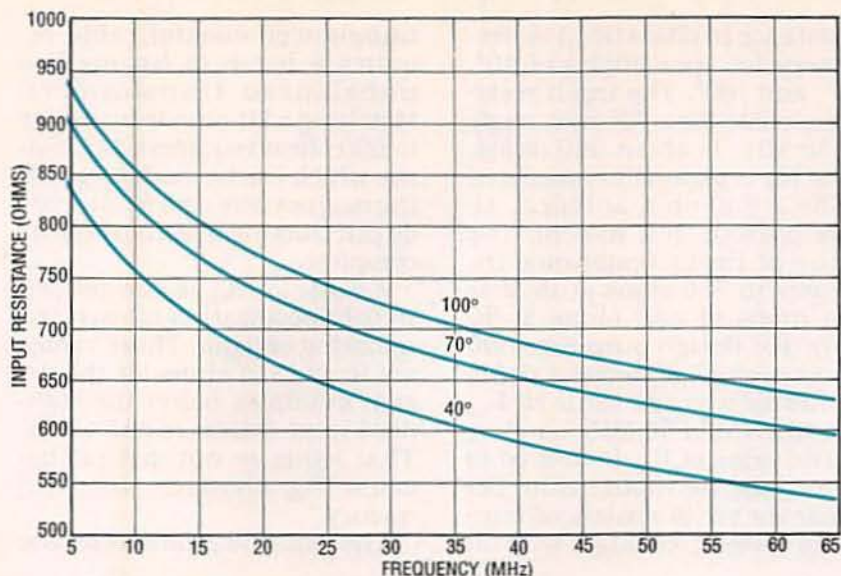


FIG. 8—PLOT OF INPUT RESISTANCE vs. frequency for a sloping-vee antenna.

15- to 50-MHz vee is shown in Fig. 9. Each radiating element is 62 feet (20 meters) long, and the apex angle is 69°. The required separation at the ends of the elements can be calculated with trigonometry or plotted to scale on paper with a protractor. For the 69°-apex angle, the ends of the elements must be 72.5 feet apart.

Step 3—Radiation Patterns

An antenna is efficient only if it radiates signals with adequate gain in the desired direction. The final step in the design of the vee is to compute its radiation patterns to verify that they meet the gain requirements. Software compatible with personal computers is available for this purpose from the source listed in Sources of Materials.

Certain parameters such as feed-point height, termination height, and element length should be varied before writing a final antenna specification. Changing any of those parameters will modify the radiation patterns. The design process is complete when the antenna radiates acceptable patterns. If a specific design doesn't meet requirements, the process should be repeated with new design values until they are met. A repetitive approach ensures a good design, and also gives the designer insight into how an antenna's performance changes with parameter differences.

For the design example, an element length of 20 meters was determined from the siting criterion. Missing are the design heights for the feed point and terminating resistors. Because the maximum height cannot exceed 25 feet, it is convenient to start by assuming a feed-point height of 6 meters (19.5 feet) and a termination height at ground level. The effectiveness of those choices will become clear as the radiation patterns are studied.

Radiation patterns were calculated every 5 MHz from 15 to 50 MHz, the intended operating range, with the tentative design

values and element lengths of 20, 40 and 60 meters. Although only the 20-meter element meets the 100 × 100 foot site limit, it's instructive to see how the pattern changes with longer elements. Figures 11, 12, and 13 show the patterns at 15, 30, and 50 MHz. Those frequencies mark the endpoints and mid portion of the desired band. In all three figures the mast height is 6 meters, the apex angle is 69°, the diameter of the element is 1/8 inch and the termination is 689 ohms.

Results at intermediate frequencies are not included here. The patterns were computed with the sloping-vee antenna located on rocky ground with a conductivity of 0.001 siemens/meter and a dielectric constant of 4. The patterns change if different ground constants are assumed, so sensitivity to ground constants was also examined, although those results are not included here.

Figure 10 shows the pattern at 15 MHz. The left vertical axis is the antenna power gain in dBi (decibels relative to an isotropic radiator, an antenna that radiates in all directions). The horizontal axis is the polar angle in degrees. Note that the polar angle, not the take-off angle, is used on the horizontal scale. A polar angle of zero is a vertical with respect to the Earth

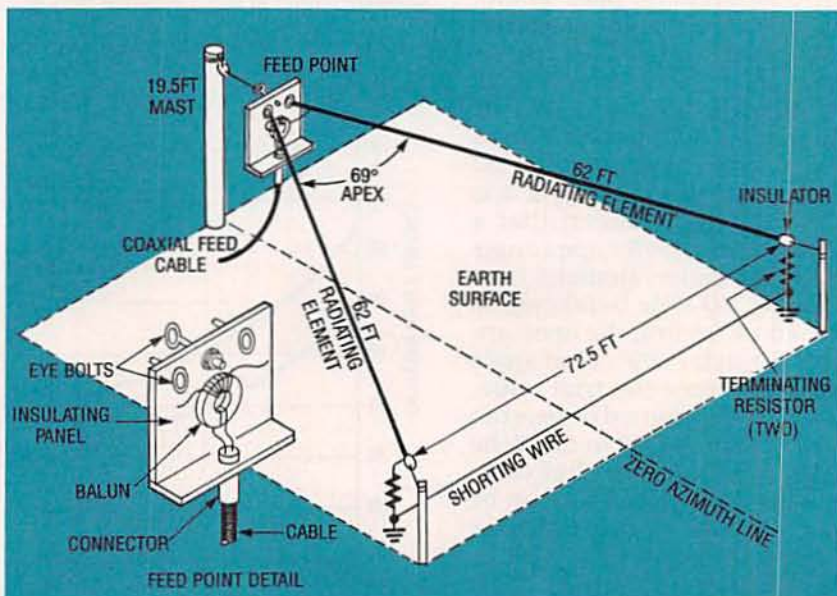


FIG. 9—FINAL DIMENSIONED DESIGN for a sloping-vee antenna that can be set up on a 100 × 100 foot plot.

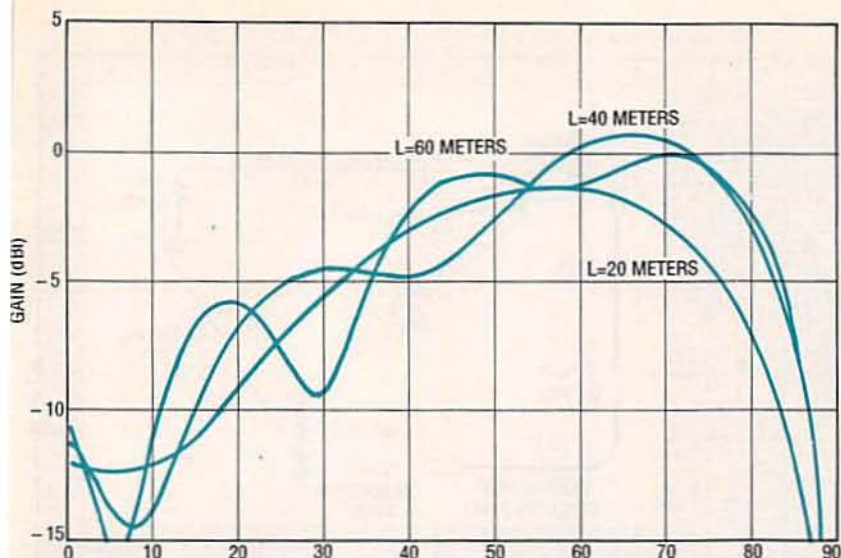


FIG. 10—GAIN VS. POLAR ANGLE for a sloping-vee antenna above rocky ground at a frequency of 15 MHz for various element lengths.

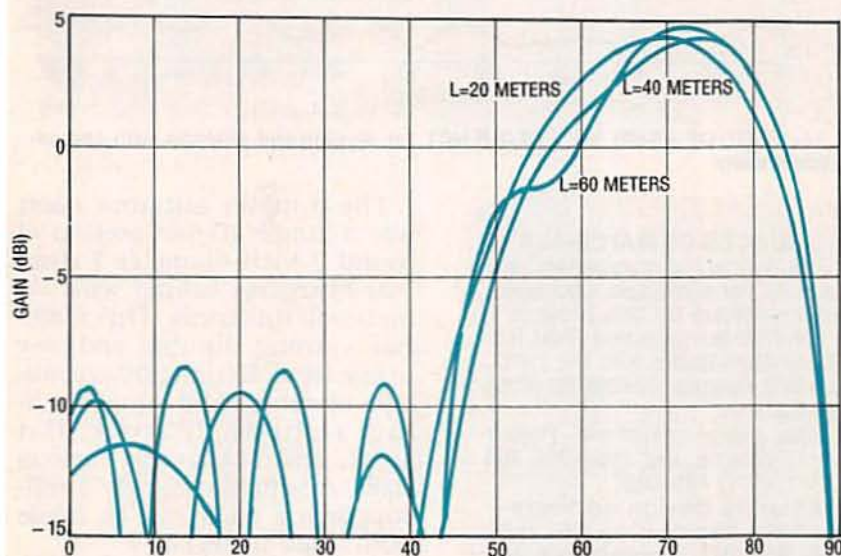


FIG. 11—GAIN VS. POLAR ANGLE for sloping-vee antenna above rocky ground at a frequency of 30 MHz for various element lengths.

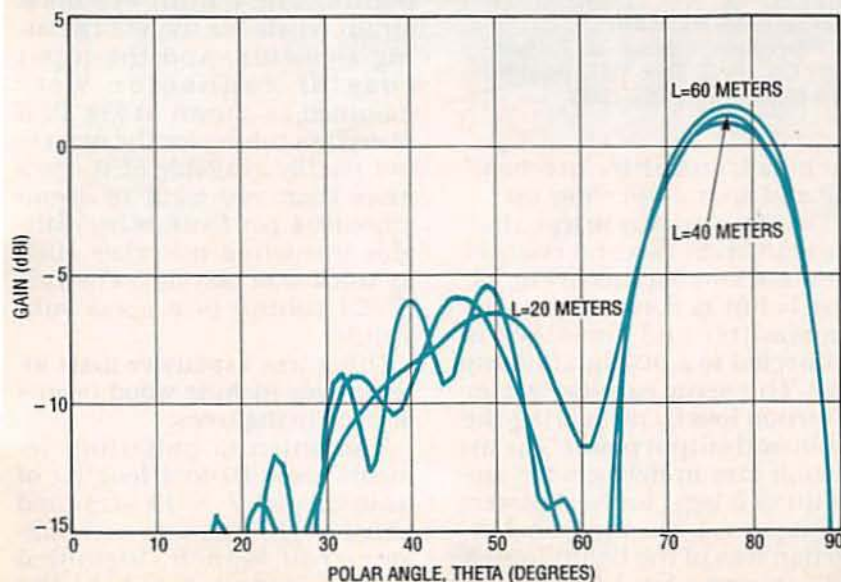


FIG. 12—GAIN VS. POLAR ANGLE for sloping-vee antenna above rocky ground at a frequency of 50 MHz for various element lengths.

(zenith), while 90° is parallel to the Earth's surface (horizon). Take-off angles of interest, 8° to 25° , correspond to polar angles of 82° to 65° in the figure. The design objective is to obtain at least 0 dBi gain in a main lobe propagating generally between polar angles of 65° to 82° .

The main lobe maximum gain at 15 MHz is -1.5 dBi at 57° for the 20-meter element. The lobe is broad, and the gain rolls off slowly on either side of the maximum. The -3 dB points are at about 32° and 74° . The highest gain, 1.5 dBi, is obtained with the 40-meter element in a broad main lobe that shows minor scalloping (sidelobing) near 40° . The pattern for the 60-meter element shows signs of breaking up—a significant secondary lobe is forming near 18° .

The 30-MHz pattern (Fig. 11) is interesting because all three elements produce a maximum gain of about 4 dBi, and their main lobe structures are very similar. The lobes are broad and smooth between 40° and 88° and the -3 dB points are near 55° and 82° . The 40- and 60-meter elements show considerable pattern scalloping between 0° and 40° , but the 20-meter element is electrically too short to develop a highly structured pattern.

Scalloping is due to constructive and destructive interference between direct rays from the antenna and rays reflected from the Earth's surface. Electrically long antennas (measured in wavelengths) are more susceptible to scalloping than shorter ones. Sidelobes waste energy by radiating it in undesired directions. Good antenna designs, therefore, minimize sidelobes as much as possible.

The 50-MHz vee pattern is shown in Fig. 12. The main lobe is again similar for the three element lengths. Maximum gain is about 6.5 dBi near 77° (13° take-off), and the -3 dB points are at approximately 70° and 83° . The main lobes are smooth and narrower than they are at the lower frequencies. The 20-meter element is beginning to show some scalloping. It has a peak sidelobe gain of -2 dBi at 50° .

However, the 40- and 60-meter antenna elements show more scalloping and even higher side-lobe gains.

An assessment of the patterns supports the conclusion that a vee antenna with 20-meter elements fed at a 6-meter height with a 69° apex and ground-level terminating resistors meets the objectives. Gain could be improved at the low end of the band with a longer radiating element, but that could violate the site limit.

The actual dimensions selected for the vee antenna are those of Fig. 9. A shorting wire connects the terminating resistors (which might or might not be connected to actual Earth ground). That wire, a current path between the resistors, is very important. In an ideal vee, the resistors are connected to a perfect ground plane that provides the current path. Omitting the shorting wire in a vee mounted on poorly conducting ground degrades performance significantly.

Antenna Construction and Measured VSWR

The antenna shown in Fig. 9 was built and tested on rocky ground in New England. It was fed through a 14:1 balun wound with 18 AWG magnet wire on a 2-inch outside diameter toroidal ferrite core. The turns ratio is the square root of the impedance ratio (in this case 3.75:1). The balun was wound with 2 turns in its primary and 7.5 turns in its secondary. If the sloping-vee is to transmit, the balun should be tested for power handling by operating at full power for several hours. Any problems that might develop

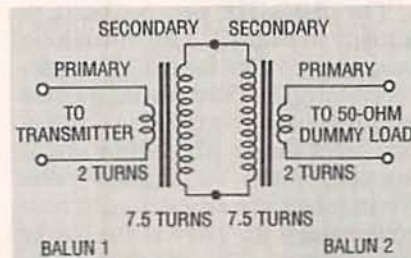


FIG. 13—BACK-TO-BACK INSERTION LOSS TEST of baluns for sloping-vee antenna.

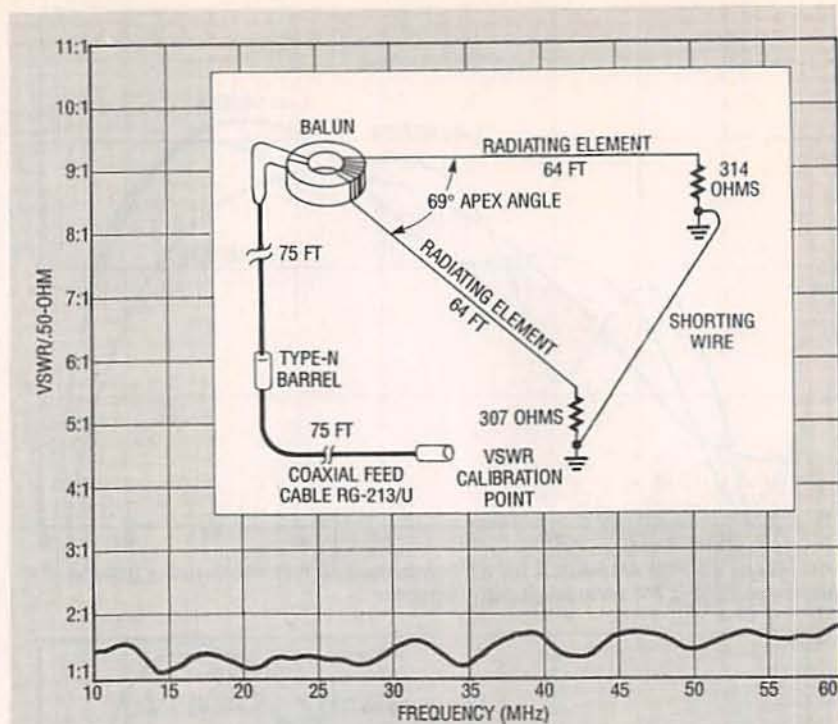


FIG. 14—PLOT OF VSWR VS. FREQUENCY for sloping-vee antenna with characteristics shown.

SOURCES OF MATERIALS

The following companies are sources for materials and computer software for this project:

- Toroidal ferrite cores (Part No. FT240-43)—Radio Kit, Inc., P.O. Box 973, Pelham, NH 03076, (603) 635-2235
- Film power resistors—Power Film Systems, Inc., Yellville, AR 72687, (501) 449-4091
- Antenna design software—Phadean Engineering Co., Inc., P.O. Box 611, Shrewsbury, MA 01545, (508) 869-6077
- Phosphor-bronze wire—Astro Industries, Inc., Dayton, OH 43432, (800) 543-5810
- Fiberglass tubing—J. T. Ryerson Co., P. O. Box 1111, Boston, MA 02103, (617) 782-6900

such as transmitter overheating and arcing will show up.

The simplest way to test a balun is to build two and connect them back-to-back as in Fig. 13. One balun is connected to the transmitter and the other is connected to a 50-ohm dummy load. This setup can also test for insertion loss by measuring the input and output power. The insertion loss in decibels for one balun is $5 \log_{10}$ (output power/input power). The measured insertion loss of the balun in this vee was a low 1.5 dB.

The 6-meter antenna mast was a single 20-foot section of round 2-inch diameter Extren 500 fiberglass tubing with 1/4-inch wall thickness. This material is strong, durable, and easy to machine. Extren 500 is available as round and square tubing, right-angle stock, flat stock, and I-beams in various sizes. A suitable base for a self-supporting mast can be made from those materials.

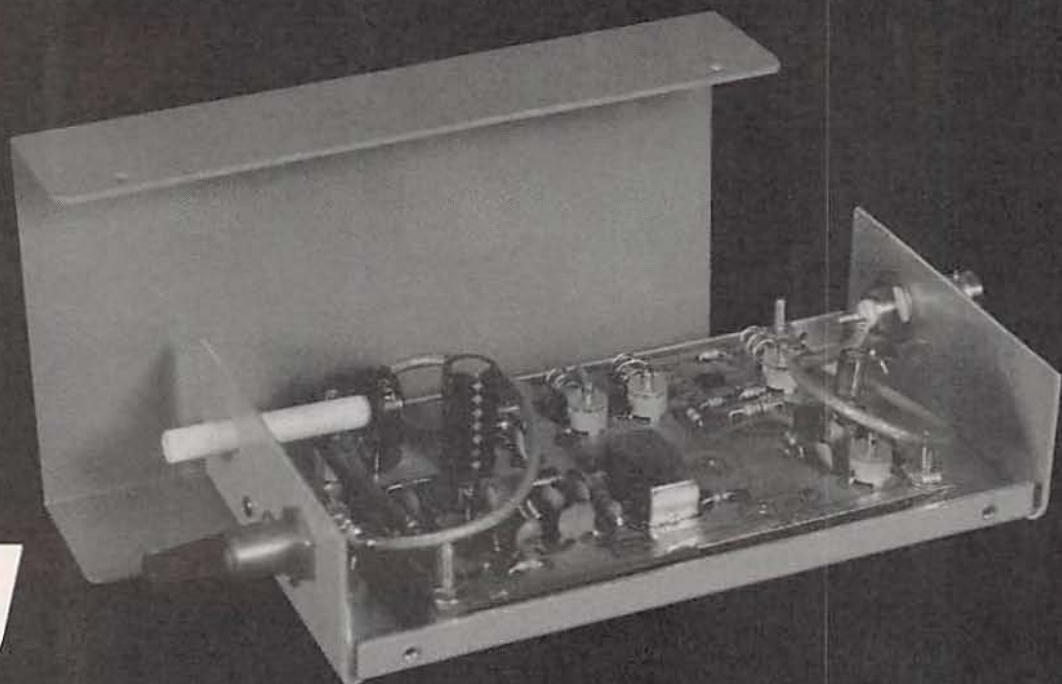
Alternatively, the fiberglass mast can be guyed at several points. The balun, eye-hook strain reliefs for the vee radiating elements, and the input coaxial connector were mounted as shown in Fig. 9. If fiberglass tubing for the mast is not readily available or it costs more than you want to spend (about \$4 per foot), other suitable insulating materials such as thick-wall polyvinyl chloride (PVC) tubing is a good substitute.

Other less expensive mast alternatives include wood beams or even living trees.

The antenna radiating elements were 62-foot lengths of uninsulated 7 × 19 stranded phosphor-bronze wire with a diameter of 1/8-inch. Stranded

continued on page 100

Receive amateur TV signals on a standard TV with our low-noise downconverter.



ATV Downconverter

WILLIAM SHEETS and RUDOLF F. GRAF

YOU CAN RECEIVE AMATEUR TV SIGNALS on a standard TV receiver with our inexpensive ATV downconverter. The downconverter converts the 420–450 MHz ATV band, which is several channels below the lower limit of the UHF band, to channel 3 or 4 for viewing on virtually any TV. The downconverter has a low-noise preamplifier stage and a double-balanced passive mixer for good performance and a wide dynamic range. That is necessary with today's crowded UHF bands. The converter draws about 27 milliamperes from a 13.2-volt DC source, so it can be used in portable and mobile applications. An extra IF stage gives an overall gain of about 25 dB.

Circuitry

Figure 1 is a block diagram of the downconverter. It consists

of three active stages and a passive diode double-balanced mixer. The input signal is first filtered so that only signals centered around 430 MHz are fed to Q1, an RF amplifier with a 20-dB gain and a noise figure of 1.5 dB. Q1 is an NEC 25137 gallium-arsenide field-effect transistor, or GaAsFET. The amplified signal in the 420–450 MHz range is fed to a double-tuned bandpass filter. The overall bandwidth of the RF stage is about 12 MHz, which is sufficient to cover the most frequently used part of the ATV band (426–439 MHz) without retuning. For operation over the entire 420–450 MHz band, you may have to repeak the filters to tune in weak signals.

The amplified signals are mixed by a diode double-balanced mixer with an oscillator signal (generated by Q2) that is

nominally 60–70 MHz lower than the received frequency. A 2-dB pad is used between the oscillator and mixer to reduce interaction. The IF output from the mixer is fed to a low-pass filter that cuts off at about 100 MHz. That reduces UHF signal feedthrough. Amplifier Q3 boosts the IF signal at 60 or 66 MHz (channel 3 or 4) by about +15 dB. The output of Q3 is fed to the TV receiver being used as an IF amplifier.

Figure 2 shows the schematic of the downconverter. The input signal from J1 is applied to a tap on L1, the input (antenna) coil. L1 is nominally a 3-turn coil and the tap is at $\frac{3}{4}$ turn so that the voltage applied from J1 is stepped up four times. Capacitor C1 tunes L1 to resonance, and is also connected to gate 1 of Q1.

Capacitors C3 and C4 provide

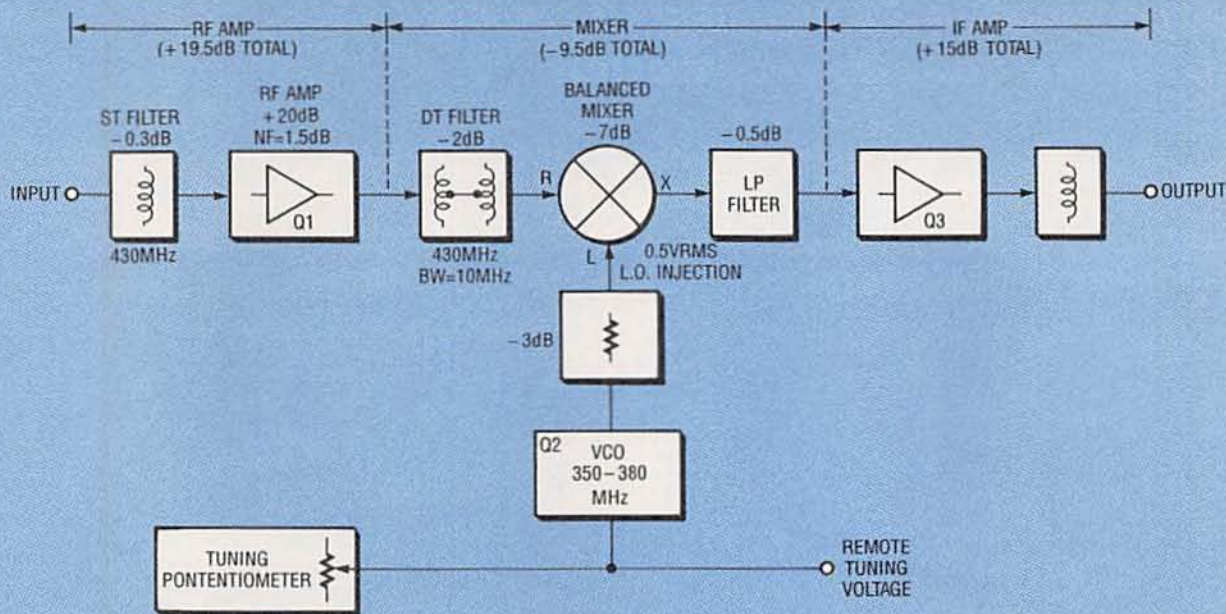


FIG. 1—DOWNCONVERTER BLOCK DIAGRAM. It consists of three active stages and a passive diode double-balanced mixer.

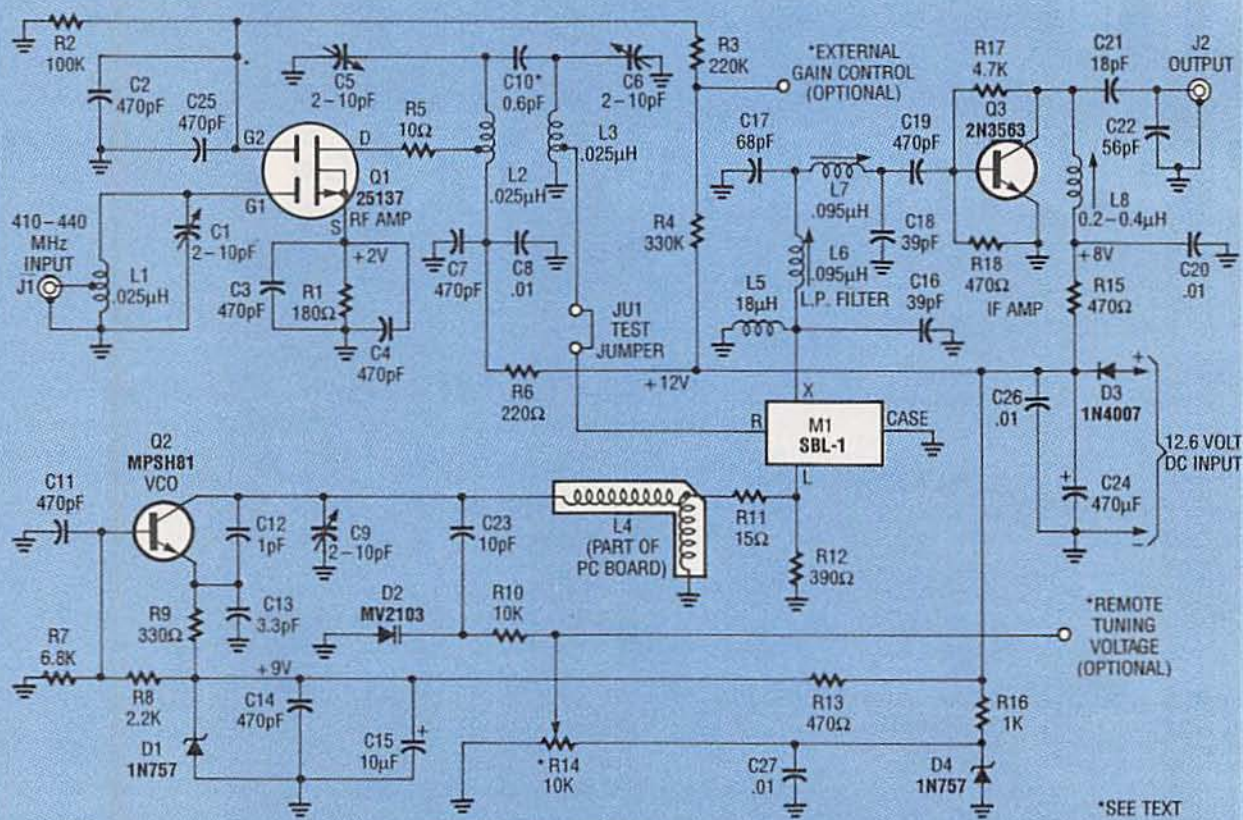


FIG. 2—DOWNCONVERTER SCHEMATIC. The input signal from J1 is applied to a tap on L1. Capacitor C1 tunes L1 to resonance and passes the signal to Q1, an NEC 25137 GaAsFET.

RF bypassing for the source of Q1, and R1 provides self-bias for Q1. Gate 2 of Q1 is biased by network R2, R3 and R4. An external gain-control signal

(which is usually not required) can be applied to the junction of R3 and R4 if it becomes necessary to reduce the gain of the converter on very strong sig-

nals. A DC voltage of +6 volts will cause full gain, and -6 volts will cause nearly a -40-dB reduction in gain. The voltage can be derived from an AGC circuit, if necessary, but a potentiometer can also be used. Capacitor C2 provides RF

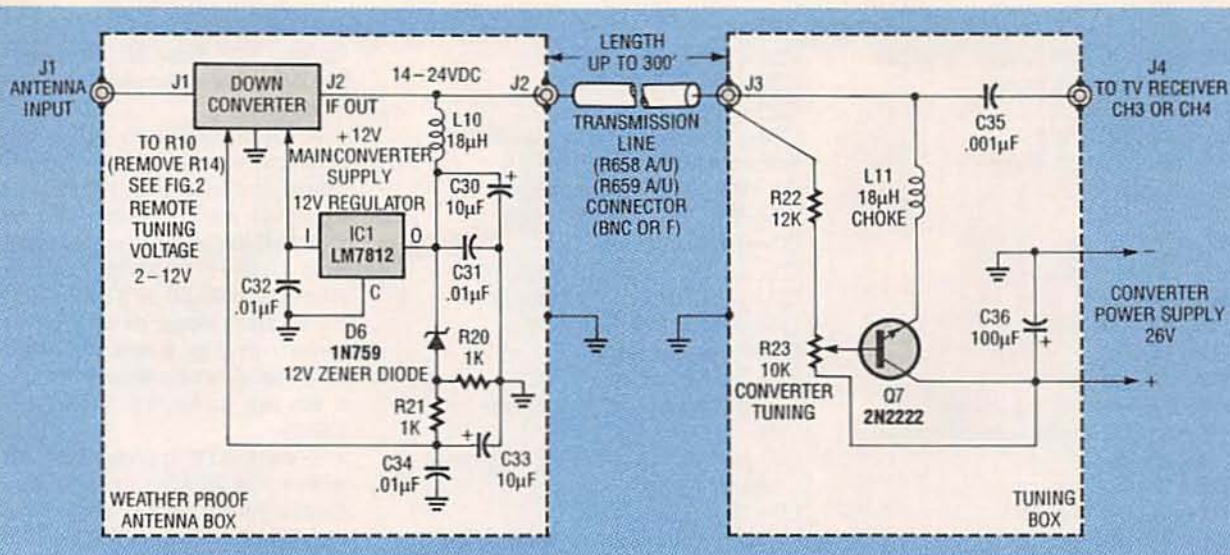


FIG. 3—THE DOWNCONVERTER can be supplied with an external DC voltage for remote-control tuning.

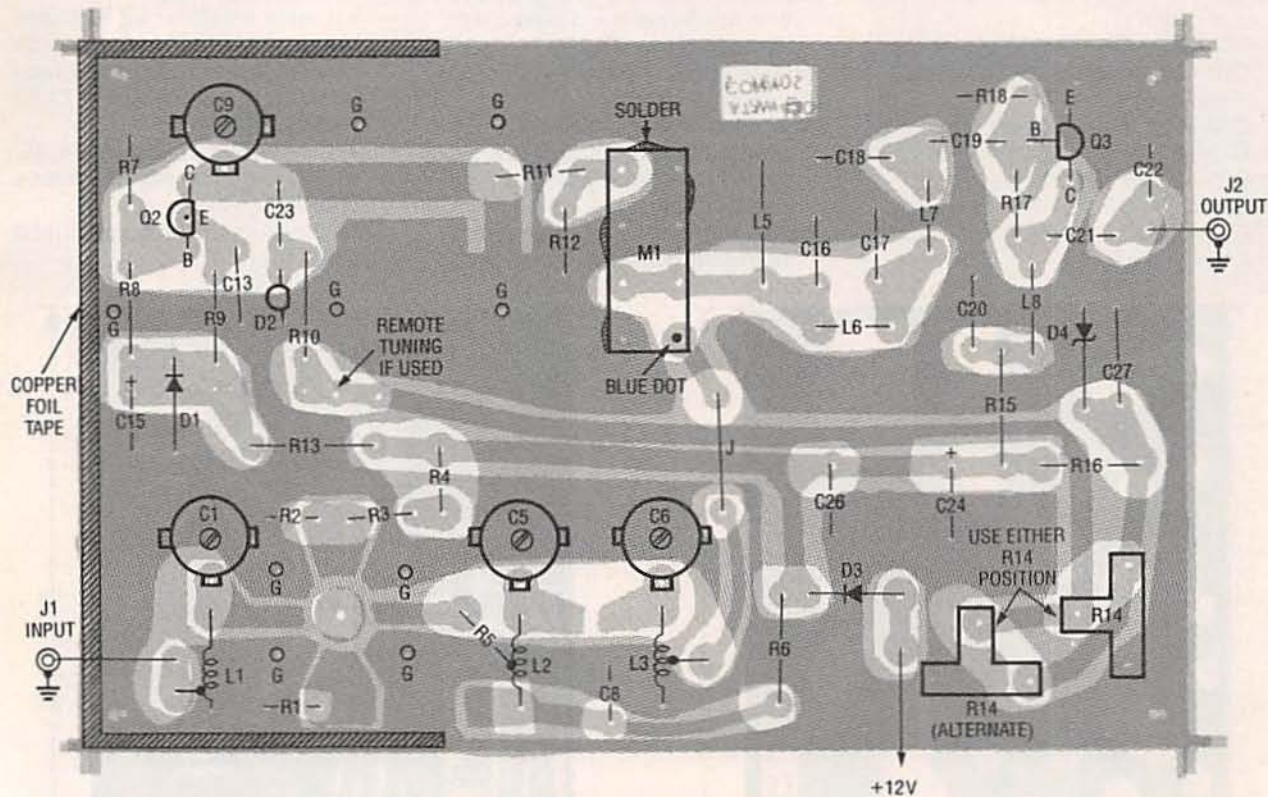


FIG. 4—PARTS-PLACEMENT DIAGRAM. This layout must be followed exactly to duplicate the performance of the downconverter. Some components mount on the solder side of the board as shown in Fig. 6.

grounding for gate 2 of Q1, and R5 reduces any UHF parasitic oscillations. The drain of Q1 is connected to a tap on L2, which is part of the bandpass filter network. Capacitors C7 and C8 provide RF grounding for the cold end of L2. DC bias is fed through R6. Under normal conditions, the drain pin of Q1 will be at +10 to +11 volts DC.

Capacitor C10 couples the signal from the first tuned circuit (C5-L2) to the second tuned circuit (C6-L3). The value of C10 is very small (0.6 pF); it determines the degree of coupling between L2 and L3. It is made from a small piece of PC board material and is mounted on the bottom of the main board. A signal from a tap on L3 is fed via

test jumper JU1 to mixer M1. The local oscillator (L.O.) signal from Q2 is also fed to the mixer.

Transistor Q2 is the local oscillator, for which R13, D1, C14, and C16 provide a stabilized 9 volts DC. Because Q2 is a PNP transistor, it allows the collector to be DC grounded, which is an advantage in this type of oscillator circuit. Resistors R7 and R8 provide base bias for Q2. C11 provides a solid RF ground

PARTS LIST

All resistors are 1/2-watt, 5%, unless otherwise noted.

- R1—180 ohms
- R2—100,000 ohms
- R3, R4—220,000 ohms
- R5—10 ohms
- R6—220 ohms
- R7—6800 ohms
- R8—2200 ohms
- R9—330 ohms
- R10—10,000 ohms
- R11—15 ohms
- R12—390 ohms
- R13, R15—470 ohms, 1/4-watt
- R14—10,000 ohms, potentiometer with shaft
- R16—1000 ohms
- R17—4700 ohms
- R18—470 ohms

Capacitors

- C1, C5, C6, C9—2–10 pF trimmer
- C2—C4, C7, C11, C14, C25—470 pF, chip
- C8, C20, C26, C27—0.01 μ F, disc
- C10—0.6 pF (must be handmade, see text)
- C12—1 pF, NPO disc or chip
- C13—3.3 pF, NPO disc or chip
- C15—10 μ F, 16 volts, electrolytic
- C16, C18—39 pF, NPO disc
- C17—68 pF, NPO disc
- C19—470 pF, disc

- C21—18 pF, NPO disc
- C22—56 pF, NPO disc
- C23—10 pF, NPO disc
- C24—470 μ F, 16 volts, electrolytic

Semiconductors

- D1, D4—1N757A Zener diode
- D2—MV2103 varactor diode
- D3—1N4007 diode
- Q1—25137 GaAsFET (NEC)
- Q2—MPSH81 NPN transistor
- Q3—2N3563 NPN transistor

Other components

- L1—L3—3 turns of 20 AWG tinned wire (approx. 0.025 μ H, see Fig. 5)
- L4—part of PC board etching, see text
- L5—18 μ H RF choke
- L6, L7—8 turns of 22 AWG enameled wire wound on No. 8 screw (approx. 0.095 μ H, see Fig. 5)
- L8—9 1/2 turns of 22 AWG enameled wire wound on No. 8 screw, with ferrite slug (see Fig. 5)
- M1—MCL SBL-1 mixer
- J1, J2—F connector

Miscellaneous: PC board, 3/16-inch copper-foil tape, coaxial cable, project case, 12.6-volt DC power supply, solder, etc.

Note: The following items are available from North Country

Radio, P.O. Box 53, Wykagyl Station, New Rochelle, New York 10804:

- A kit of parts to build the downconverter (includes PC board and all parts that mount on it, J1 and J2, and wire to wind all inductors (metal case and power supply not included)—\$59.50 + \$3.50 S&H (Note that none of the parts shown in Fig. 3 are included with the downconverter kit.)

- Metal case as shown—\$12.50

- 2-watt ATV transmitter kit with a 439.25-MHz crystal (see Radio-Electronics, June and July 1989)—\$110 + \$3.50 S&H

- A 0.5-watt, 9-volt transmitter kit with a 439.25-MHz crystal—\$112 + \$3.50 S&H

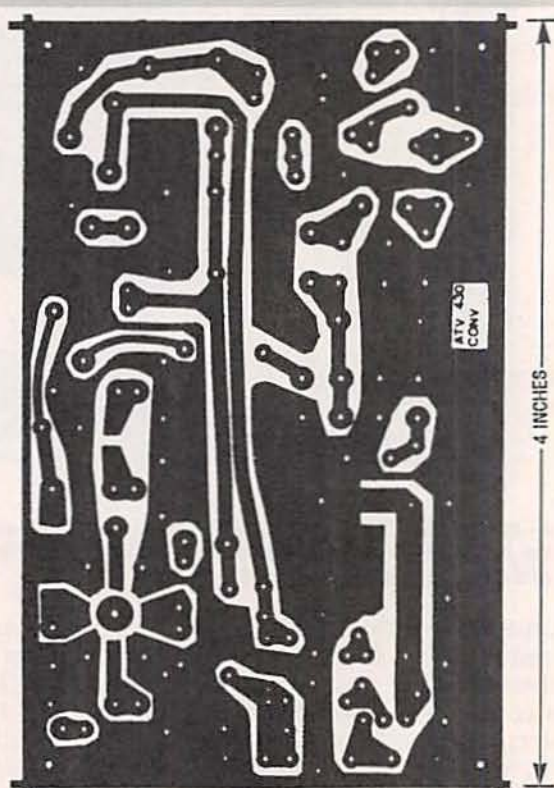
- Linear amplifier kit to boost the output of ATV transmitter to 15 watts (see Radio-Electronics, August 1992)—\$79.50 + \$3.50 S&H

- Crystals for channels 14, 15, 16, 17, or 18 (for test purposes only)—\$7.50 each

New York residents must add sales tax.



COMPONENT SIDE FOIL PATTERN.



SOLDER SIDE FOIL PATTERN.

for the base of Q2, and R9 provides emitter bias. Nominal current through Q2 is about 5 to 6

milliamperes. Capacitors C12 and C13 provide a feedback network for Q2.

Components C9 and L4 (a length of microstrip line etched on the PC board), together with

C23 and varactor diode D2, form a circuit that can be tuned via the bias on D2 over the range of 350 to 390 MHz, depending on the setting of C9. Therefore, Q2 will oscillate over that frequency range, because positive feedback is provided by C12 and C13, and Q2 acts as a grounded-base amplifier. Oscillator output is taken through R17 and R12 to mixer M1. The level at terminal L of the mixer is about 0.3 volt RMS. Resistor R11 is connected to a tap on L4, which also provides bias return for the collector of Q2, because it is at DC ground.

The output from mixer M1 at 60 to 70 MHz (the difference frequency between received signal and L.O. frequency) appears at mixer terminal X. There is about a 7-dB loss in the mixer. Coil L5 provides a DC return for the mixer IF port. A low-pass filter made up of C16, L6, C17, L7, and C18 eliminates any remaining UHF signal components appearing at terminal X. Transistor Q3 is an IF amplifier stage, which is biased by R13, R14, and R15 to a V_{CE} of 8 volts and a collector current of about 8 mA. Tuned circuit L8, C21, and C22 can be tuned to either channel 3 or 4. The signal from the low-pass filter is coupled to Q3's base via C19. Transistor Q3 provides about a 15-dB gain; its output signal appears at J2. Power for the downconverter is supplied through D3, which protects against reverse voltages, and C24 and C26, which bypass RF and noise.

Resistor R10 couples DC bias to D2 supplied from tuning-potentiometer R14. Components R16, D4, and C25 provide 9-volts DC for that purpose. If desired, R10 can be supplied with external DC for remote-control tuning, or to allow the downconverter to be mounted close to the antenna. That is commonly done to reduce transmission-line losses between the antenna and converter—losses run high at 450 MHz unless very expensive transmission line, such as 1/2-inch hard line, is used. If you are planning on remote-controlling the converter, install R14 so it's easy to move.

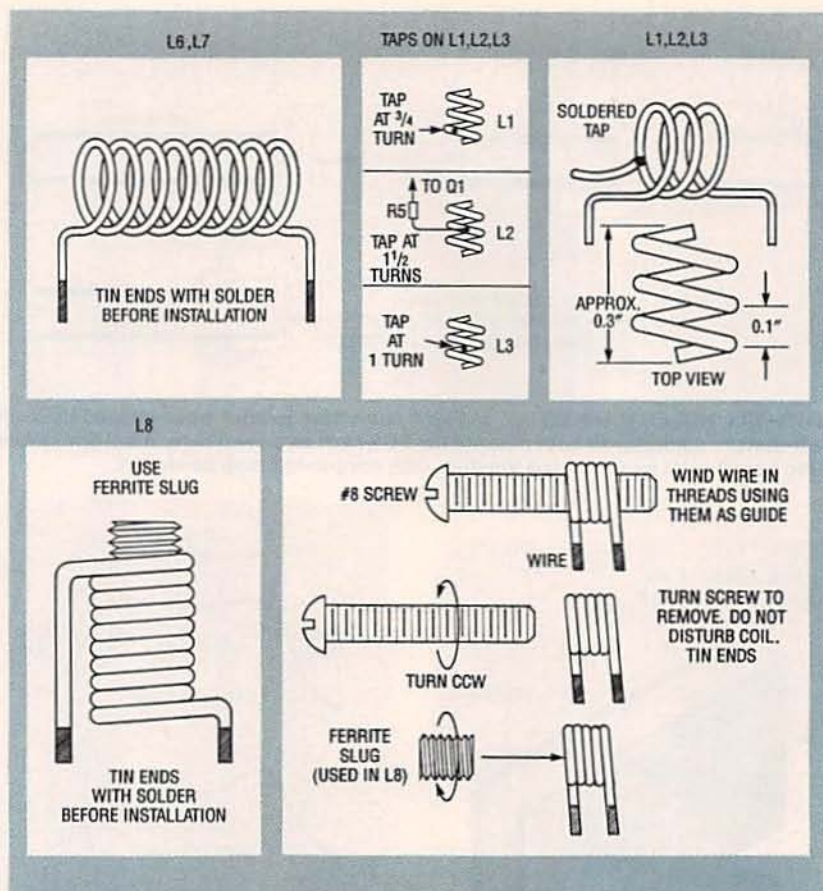


FIG. 5—COILS L1, L2, AND L3 are three turns each of 20 AWG tinned wire wound around a No. 8 screw and stretched to 0.3 inch. The lead from J1 has its center conductor soldered to L1 at 3/4 turn from the grounded end. Resistor R5 is soldered 1 1/2 turns from the end of L2 that connects to R6, C7, and C8. Coil L3 is tapped at 1 turn from the grounded end. Coils L6 and L7 are 8 turns each of 22 AWG enamelled wire wound on a No. 8 screw. Coil L8 is 9 1/2 turns of 22 AWG enamelled wire wound on a No. 8 screw with a ferrite tuning slug added.

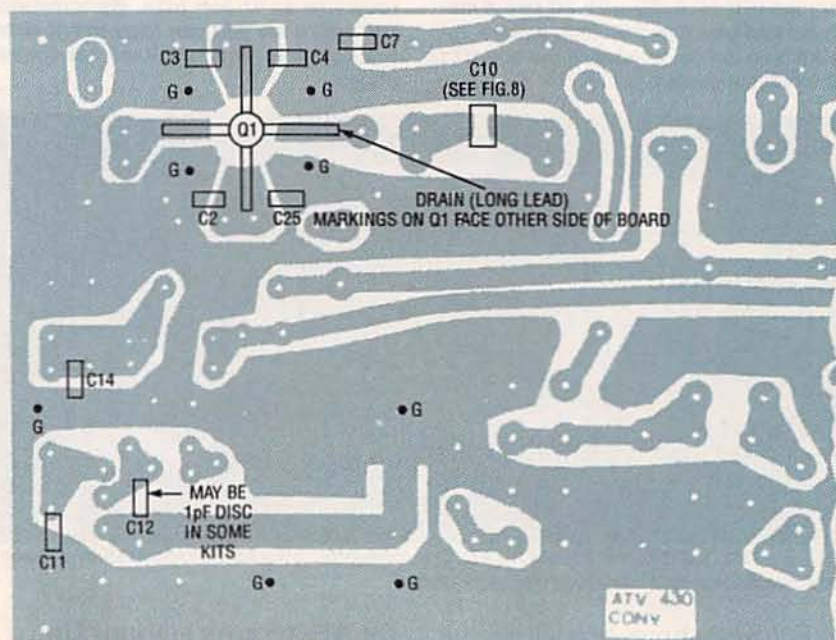


FIG. 6—ALL CHIP CAPACITORS, C10 (see Fig. 8), and Q1 mount on the solder side of the board. The markings on Q1 face the component side of the board.

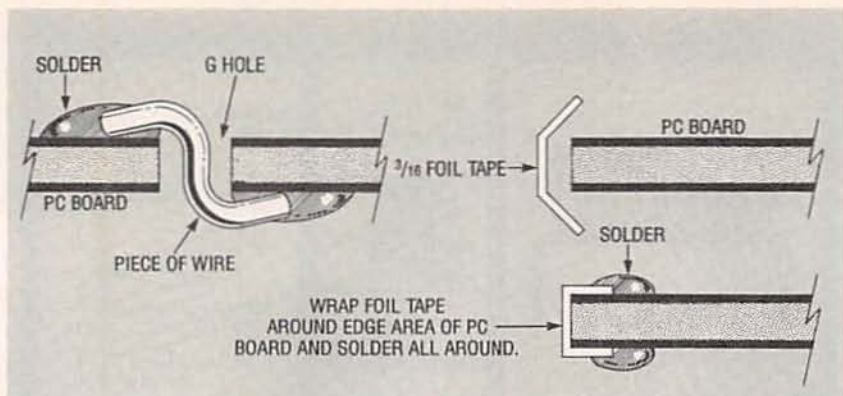


FIG. 7—ALL HOLES MARKED "G" in Fig. 4 must have jumper wires passed through them that are soldered on both sides of the PC board as shown here. Also, both sides of the board must be grounded together with copper-foil tape as shown.

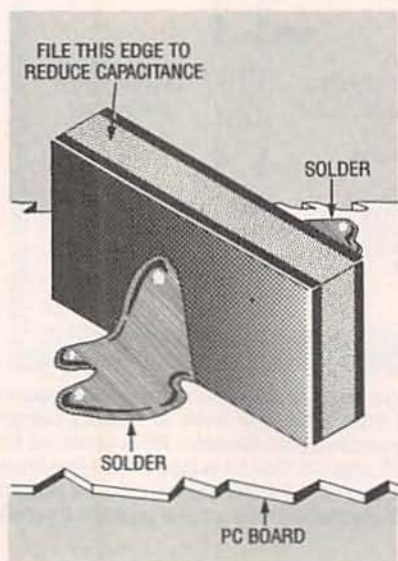


FIG. 8—TO MAKE C10, take a small square of G-10, 0.062-inch PC board material and trim it to a 3/16-inch square. Install it on the solder side of the board in the location shown in Fig. 6.

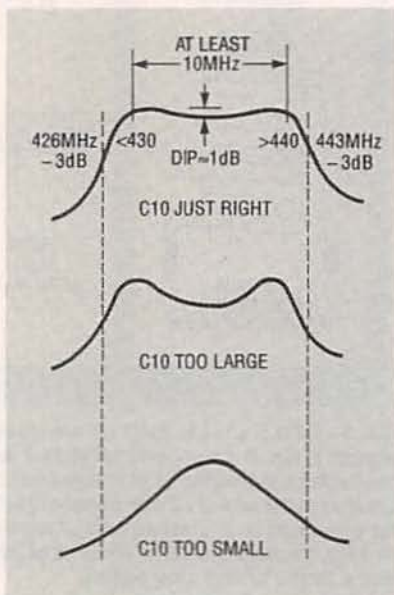


FIG. 10—PEAK THE CONVERTER for a response as shown here. By trimming C10 with a file you can experiment with the coupling and resultant bandpass shape.

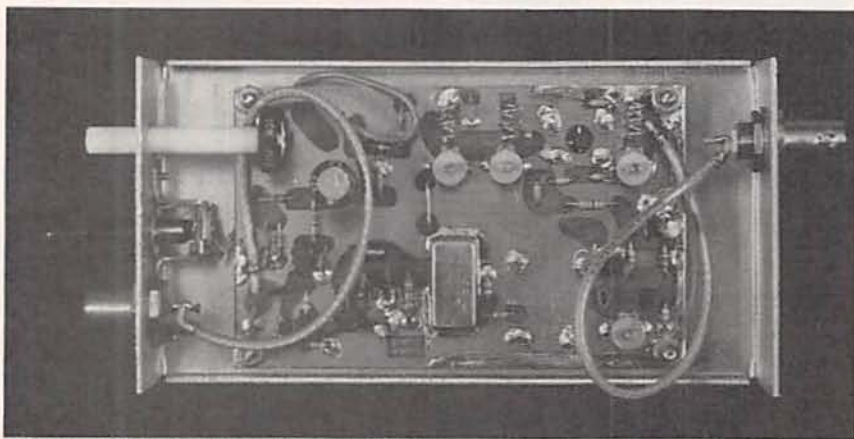


FIG. 9—THE AUTHOR'S PROTOTYPE. The converter should be mounted in a metal box, weatherproof if outdoor use is intended.

Figure 3 shows how J2 can be connected to a long coaxial transmission line that runs to

the ATV receiver station. The cable is isolated from ground and can therefore carry a DC volt-

age. The DC voltage is impressed on the cable as follows: A nominal 26-volt power source at the ATV receiver station is connected to Q7, a 2N2222 NPN transistor used as an emitter-follower. Resistors R22 and R23 produce a variable voltage of 14 to 26 volts at the base of Q7, whose emitter will follow the voltage. Power is supplied to the cable through L11, and by varying potentiometer R23, the voltage applied via R22 to the cable at J3 can be adjusted between 14 and 24 volts. Capacitor C35 prevents any DC voltage from appearing at J4.

The DC voltage is taken off the cable via the 18 μ H RF choke L10. Capacitors C30 and C31 remove noise from the DC voltage and provide an RF ground. Positive voltage is fed to the downconverter via the cable's center conductor and the outer shield serves as the negative supply lead; it is grounded to the case and ground foil.

The DC input is fed to D6, a 12-volt Zener diode (a 1N759 can be used). Capacitors C33 and C34 filter any noise from the voltage which will be 12 volts less than the voltage on the coaxial transmission line (+14 to +24 volts), or +2 to +12 volts DC. That is fed to R10, which feeds the tuning voltage to the downconverter varactor. By varying the DC voltage on the transmission line between +14 and +24 volts, not only can the downconverter be powered, but it can be remotely tuned to a desired frequency as well.

Note that the components shown in Fig. 3 are not part of the downconverter board, and they are used only if remote operation is required.

Construction

The PC board material (G-10, 0.062 inch thick glass epoxy) and layout must be followed exactly to duplicate the performance of the downconverter. The stray capacitance, coupling between elements, and L4 are all integrated into the design of the board. Any layout deviations can change those specifications. The foil patterns are

continued on page 109

HARDWARE HACKER

Apple's PhotoGrade, electronic halftones, consultants network, marketing your ideas, and two great new books.

DON LANCASTER

Oh, the times, they are a-changing. We seem to have a mix of really bad and really awesome stuff coming down lately. Let's start off with some of the sadder vibes...

Heathkit has recently discontinued production on most of its electronic kits. It's the end of an era for sure.

But a funky little outfit called *Musty Manuals* is setting out to stock and make available all of those older Heath assembly books and instruction manuals. And lots of exciting hacker kits are being made available from such outfits as *PAIA*, *Old Colony*, and *Micro Mint*. Plus, of course, through several of the advertisers in this magazine.

The technical paperback book field (especially the non-computer titles) is clearly not well. *Sams* is essentially gone, bought out by Macmillan and triaged into an ethereal shadow of what once was the most respected and diversified technical book publishers in the world. *TAB* has been purchased by McGraw-Hill and become a subsidiary. I have been getting plenty of helpline complaints about several sources that offer dated and inaccurate titles. Believe it or not, your IRS is now paying publishers to shred books, especially old technical paperbacks, through an obscure inventory ruling that has totally decimated long-term back lists and older technical titles.

But—an incredibly exciting new opportunity called *Book-on-demand* publishing is emerging in which you can produce first-quality paperback and hardback books literally on your kitchen table when and as they are ordered. With a "forever" backlist, no IRS inventory penalties, and no lower limit to the total number of sellable volumes needed. And it also includes such

exciting possibilities as a 90-percent author's royalty and rapid CD-ROM distribution. Much more on this on *GENIE* PSRT.

Very alarmingly, some community colleges are cutting back on or outright eliminating their electronics departments. And many electronic service and repair trade journals have vanished without a trace.

But—we now have got the richest and most incredible variety of cheap new chips to play with. Anywhere. Ever. We have major breakthroughs in hacker direct-toner printed circuits. We have a brand-new **Electronics Now** format with new features and fresh ideas that continues the oldest ongoing electronics magazine publishing house. And we are something like a scant eight years away from hardware that can surpass the human brain in logic and analysis capabilities.

Right now is certainly the greatest time ever to be getting into hardware hacking in a very big way.

Electronic halftones

I've recently been playing around with the new *LaserWriter G* and am very impressed with its new ability to print medium- to high-quality photo halftones. So, I thought we might review what is involved in the laser printing of photos in general, and see just why Apple's neat *PhotoGrade* process seems to beat out brute-force methods—and how we can do even better.

NEED HELP?

Phone or write your **Hardware Hacker** questions directly to:
Don Lancaster
Synergetics
Box 809
Thatcher, AZ 85552
(602) 428-4073

Many of those previous-generation laser printers were 300-DPI devices, capable of placing or not placing 300 whole dots per inch uniformly along any one selected laser scan line. That translates to 90,000 dots per square inch, or a tad over 8 million dots on a standard page. If a dot is only black or white, it can usually be represented on the page *bitmap* or in your *frame device* as a single bit. Thus, around a megabyte worth of memory must be reserved for your full-page bitmap at 300-DPI resolution.

The obvious big dilemma in raising your laser-printer resolution is this: As you go from 300 DPI to 1200 DPI, you could end up requiring *sixteen* times the memory! And your page makeup times could end up *sixteen times* as long! Yet "more" resolution is perceived to be a big user need. Or is it?

Actually, laser-printing resolution is pretty near as highly overrated as *Peterbilt* trucks or teenage sex. But that's another story for another time. I strongly feel that higher resolution is not worth losing genuine Adobe Level II PostScript, duplex printing options, low per-page printing costs, mainstream technology, good third-party supply sources, local hard-disk support, or any sleep.

A poorly scanned photo (or one that's not properly *histogram equalized*) will end up looking even worse on the premium machines.

One zero-cost way to increase your printer's resolution when you'd like "camera ready" art for conventional printing: Just work oversize and then photoreduce. Most of my *Hardware Hacker* figures are printed at 133 percent normal size and are then reduced here for an effective resolution of a scant 400 DPI. Yet I feel they look as good as most of the other technical figures.

An easy way of making a 300-DPI

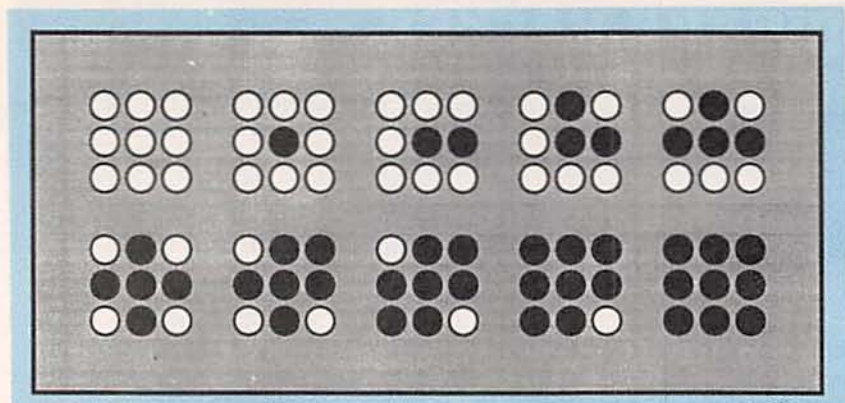


FIG. 1—A LASER PRINTER can fake a half-tone by grouping dots into a larger "cell." In this example, a 3 × 3 pixel array forms a cell that can have ten gray levels, including black and white. On a 300-DPI printer, this would form a "100 line, 0 degree" halftone screen.

printer look better is to do a plain old smoothing job. That concept was pioneered by Hewlett-Packard as *Resolution Enhancement Technology*.

Apple (and many also-rans) have copied this idea. On the LaserWriter G, Apple calls it *FinePrint*.

The smoothing is done by a custom integrated circuit that inter-

cepts and stores a few of the scan lines on their final way out to the laser scanner. By analyzing a matrix formed from the nearby dots on earlier and later lines, certain dot positions are delayed by one-half a dot, following a smoothing algorithm. The result is a really big improvement in most typography and some graphics, especially for reproducing slanted lines.

Despite all the hype, the circuitry involved is simple and cheap. And it can end up totally independent of the imaging model or language in use.

But plain old smoothing can't help halftone photos, and it may even

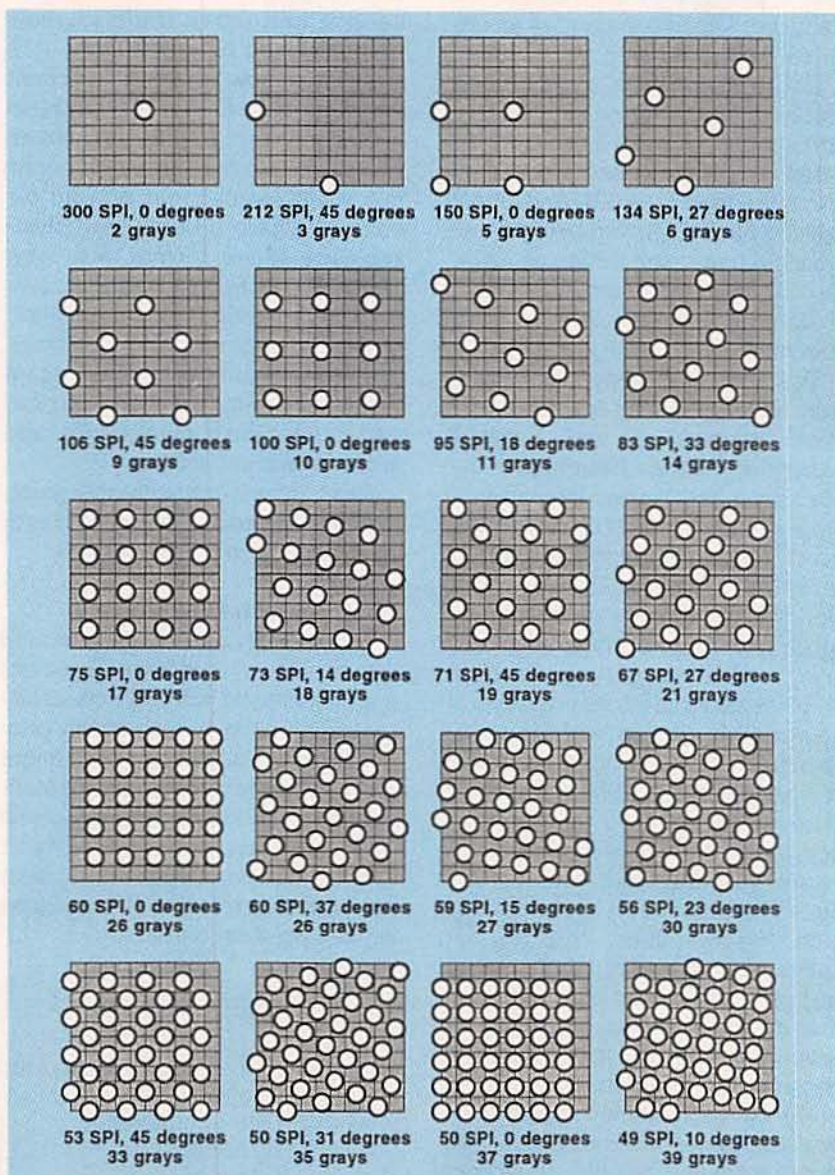


FIG. 2—THE AVAILABLE SPOT PATTERNS for a typical 300-DPI PostScript printer. Note that these are the ONLY dense patterns available. You'll get one of these regardless of what you ask for. Note the perfect tiling.

NEW FROM DON LANCASTER

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urt. Let's look further at...

The halftone process

There is only one method to print something that is truly gray on the page. And that is to use gray ink. And each different shade of true gray will need a different gray ink and another pass through the printing press. Since this is clearly not good, printers have long used a halftone process instead.

The halftone process consists of printing lots of different-sized black dots very near to each other. The dots are carefully spaced to be less than the eye's angular resolution. Instead of seeing the individual dots, your eye averages out the black dots and the white background and perceives an average gray level. The higher the ratio of white to black, the lighter the gray, and vice versa. Let's try it out. Look at a gray portion of any black and white photograph or tint box in this magazine. While it looks gray with the naked eye, under a magnifying glass you'll see all the little dots that make up the halftone. The dots are all black.

To print any photograph, a special screen is used on the litho camera to convert gray values into collections of black dots of varying size.

Traditional printers will spec their screen size as the number of halftone spots per inch. Some popular ones include 85 spots per inch for tabloid news and the 120 spots per inch for most magazines of **Electronics Now** quality.

Even higher spot densities are used on premium magazines. But they require special inks, coated papers, and extreme attention to detail. Note that even the highest spot densities used are nowhere near 300 spots per inch!

A second halftone parameter is called the screen angle. It turns out that the human eye is very good at picking out horizontal and vertical lines, but rather poor on resolving diagonals. Since the halftone process introduces visual artifacts, it is often best to set your black-and-white screens on a 45-degree angle. In color printing, the halftone screen angles become even more critical if they are to eliminate objectionable Moire patterns.

Several methods can be used to fake halftone screens on laser printers. One method is to group all the possible laser dot positions into larger spots that I'll call a cell. Figure 1 shows you how a 300-DPI printer can use nine dots to make cells of 100 spots per inch. This particular cell has a screen angle of zero. As you can see, there are ten possible gray levels here, including black and white.

We can immediately see that we could use 36 dots to form 50-spot-per-inch cells. And those cells would give us 37 possible grays. Clearly, we have a tradeoff between the number of cells per inch and the number of available grays. Use too few cells per inch, and you'll end up with the "Sunday Funnies" effect with very grainy dots. Use too few grays, and you will solarize with obvious (and often objectionable) steps between each possible gray level.

The gray-level resolution of your eye depends on context and con-

trast, but a number slightly over 256 gray levels is possible. But, because of the stupendous costs of exceeding 256 grays, most experts agree that eight bits of gray scale resolution is enough even for premium images. Television sometimes might get by with as few as six bits, good for a mere 64 gray levels.

The obvious next question is "How good can our halftones image at an unenhanced resolution of 300 DPI?" Ignoring the obvious answer of "Not good enough," we'll then go on to ask "What can we do about it?"

PostScript to the rescue

I have found that the PostScript general-purpose computer language has some really great approaches to electronic halftones. Those involve their *setscreen* and *image* operators, among many others. PostScript uses some imaging tiles that determine the screen angles and frequencies. Since these screen tiles must all abut

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each other perfectly and still must obey integer (whole numbers only) math, there are very definite limits to which 300-DPI tiles are and are not possible. If you ask for some halftone cell angle or frequency that is simply not physically possible, PostScript will substitute the nearest handy one.

Figure 2 shows you the available denser halftone cells as used on most popular 300-DPI PostScript printers. Figure 3 shows you the *secret gray map* for all of the "hidden" PostScript grays.

Typical PostScript users and most applications packages blindly insist on using the *seventeenth* most putrid PostScript gray available. While this is often incorrectly called a 60-DPI screen, its effective resolution is only 53 dots per inch. There are 33 grays with this default screen.

That sort of explains the "Sunday Funnies" effect of most poorly done PostScript screens. And one of the biggest reasons why people feel

they need "more" resolution. When in fact, their grays can all get instantly and dramatically improved by using a few dozen keystrokes!

For instance, the best PostScript 300 DPI halftone screen for typical graphics is a 106 DPI, 45-degree one which gives you absolutely beautiful grays. Sadly, you'll only get ten of those grays, but the lightest ones are very good for graphics.

Two other quite useful 300 DPI secret PostScript grays of interest are the 85-line and 35-degree "reprogray" useful for oversize cam-

era-ready art, and the 135-line, 2 degree "india ink wash" gray. The latter gives you only six gray levels and requires a careful selection of toner and paper. But the results are stunning.

One way to do a best PostScript gray is to enter these keystrokes in a PostScript commands...

```
106 45 dup mul exch dup mul
add 1.0 exch sub setscreen
```

The first number is your cell frequency; the second is your angle. The details of where and how you enter these code lines depend on

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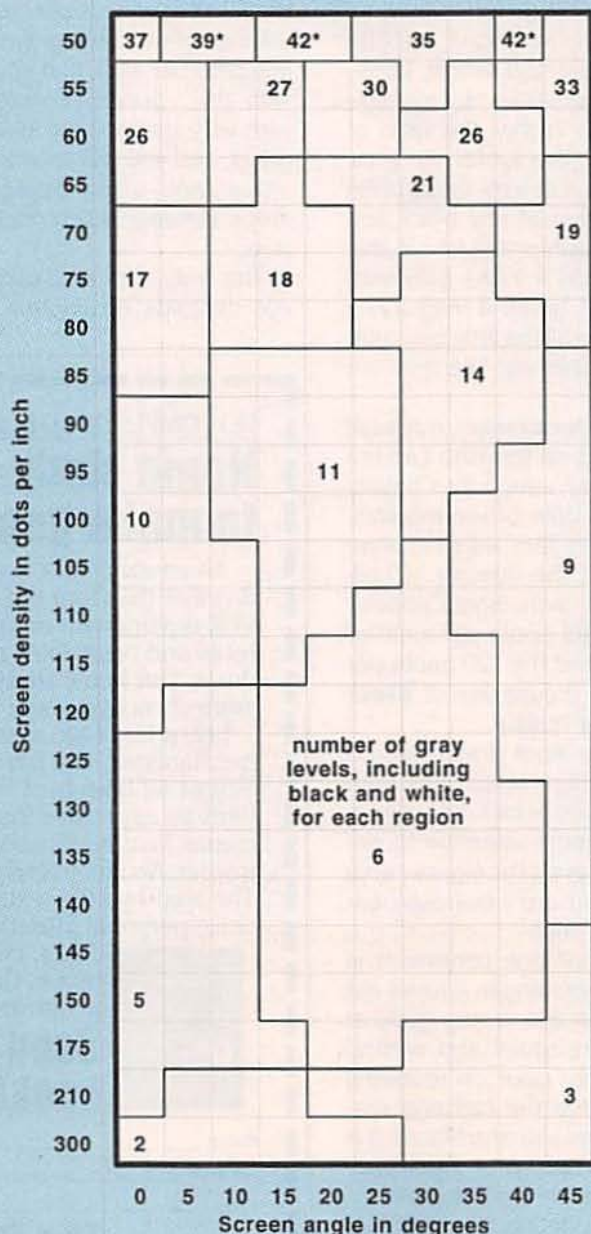


FIG. 3—THE TOP SECRET GRAY MAP for a 300-DPI PostScript printer. Most users and most application packages insist on using the seventeenth most putrid of the available grays. The best graphics gray is 106 DPI at 45 degrees.

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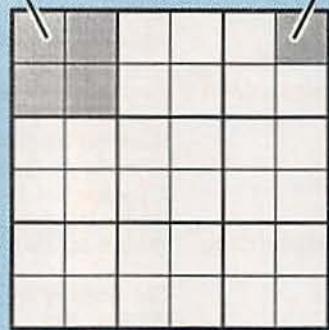
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old 300 DPI pixel size

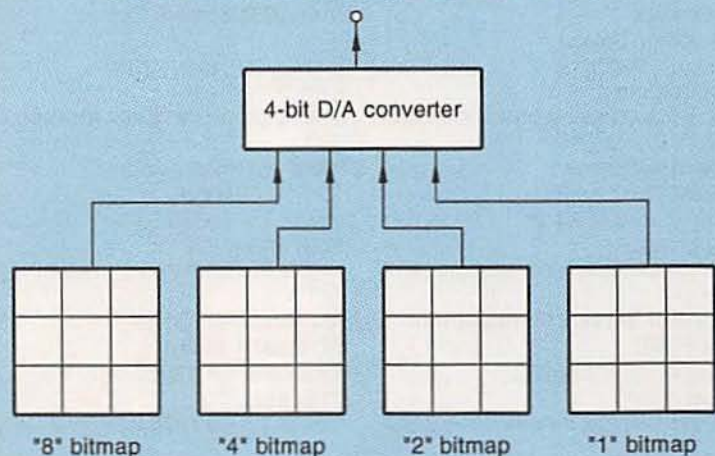
new 600 DPI pixel size



(100 DPI, 0 degree halftone cell shown)

FIG. 4—BOTH QMS AND IBM/LEXMARK chose the "brute force" 600-DPI method to improve their PostScript photo halftones. The original 100-DPI spots allowed 10 gray levels; the new ones allow 37. There is a 4x speed and 4x memory penalty for the modest (but certainly welcome) improvement.

One-of-sixteen dot size output to laser scanner



(100 DPI, 0 degree halftone cells shown)

FIG. 5—THE APPLE LASERWRITER G remains at 300 DPI, but it uses four bitmap memory planes that allow one of sixteen pixel dot sizes. That permits 144 gray levels at 100 DPI for good- to better-grade photo halftones. Or 128 gray levels at the more popular 106 DPI and 45 degree screen.

your PostScript programming style or the applications package you have. Call me if you need any further help on this.

No, none of those screens can give you any high-quality halftone photos. But the 75-line screen can give you a recognizable "auto shopper" quality photograph. Especially if the scanned image has been properly histogram-equalized.

Three key points: The halftone dots used in everyday printing are much coarser than 300 DPI. Some excellent graphic PostScript grays are available at 300 DPI. They need

only a few dozen simple keystrokes for their activation. And our halftone photo quality, when given any properly image processed input, doesn't miss by that much.

So we can potentially add only a little to 300 DPI and gain enormously on halftone photo quality. Both QMS and IBM/Lexmark picked the brute force method. As Fig. 4 shows us, they switched to a 600-DPI double resolution and then swallowed the 4:1 speed and memory penalties. At 100 cells per inch, you now have 37 gray levels. Or 50 gray levels at an 85-cells-per-inch

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density. That could make the difference between lousy and not half bad photo halftones. Especially given a proper digital image processing.

Apple has chosen the more elegant *PhotoGrade* method shown in Fig. 5. They remained at 300 DPI, but added three extra bitmap memory planes for a total of four. Then they modulated their laser dot size to one of sixteen values. You now can have *sixteen* times as many potential gray levels as you did at 300 DPI with only a single memory plane. At 106 DPI, you now have a much better 129 gray levels available. That is equal to a brute force resolution of 1200 DPI!

There is only a negligible speed penalty, since all four memory planes are written in parallel by

custom-designed LSI chips. And while you retain the same $4 \times$ memory penalty as a brute force 600×600 , you'll get *four times* the effective resolution!

The result? Good to better photo halftones out of any plain old 300-DPI laser-printer engine. Especially with premium toner and properly scanned image processing. The *PhotoGrade* is also upgradable on older NT and NTX printers with a simple plug-in board.

Can we do better?

I think we can. At least in theory. For any 100-spot-per-inch tile at plain old 300 DPI, we are using *nine* bits to call out only 10 different spot values. Since nine bits could represent 512 different state values, the *memory use efficiency* is a tad un-

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bits can yield us up to 68,719,476,736 different states, our memory use efficiency is essentially zero! Thus, *virtually all of that Apple PhotoGrade memory bitmap is totally wasted!*

Instead, let's go back to, say, 100 spots per inch at a plain old 300 DPI. Once in the center of every desired halftone spot, put out a *single* laser dot having 512 possible size values. Presto. A mind-blowing total of 512 grays at 100 DPI! Or a *perfect* 256 grays up at the usual 106 DPI! This is for photo halftone dots only; you would still be able to do special screens and weird spot functions the old way. Patterns, too.

For us to make full use of what seems theoretically designable, you would need some special automatic mode sensing for the halftone areas. And a diamond-shaped laser beam whose diameter could be controlled over a 25-decibel or 16:1 range. Down from a maximum slightly under three times larger than is now used. None of those

needs seems a really big deal.

Thus, it should be theoretically possible to build a 300-DPI PostScript laser printer with outstanding photo halftones. A 1697-DPI equivalent. At zero speed or memory penalties. Hmmm...

I have posted lots of halftone and secret gray study examples to GENIE PSRT, especially my files 129, 141, 144, 179, 180, 231, and 239. I've also uploaded some high-quality images that you can play with, either inside or outside PostScript. In particular, check out LENA.PS, MANDRILL.PS, and my enhanced LENA.HIST.PS.

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I was pleasantly surprised to find that the leading invention marketing firms are now publishing their track records—up front in their initial mailings. One of the oldest and largest discloses: Of the ideas submitted and contracted, the odds of getting a royalty license are 100:1 against,

continued on page 93

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The *PhotoGrade* does
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AUDIO UPDATE

Format future shock

LARRY KLEIN

Are we lost in a forest of new audio formats? Is there a future for DAT, DCC, and the mini disc—not to mention recordable CD's?

I have always considered myself relatively immune to the effects of "Future Shock." As you may recall, the dreaded FS Syndrome describes the disturbed and disoriented behavior of those suffering input overload brought on by too many life changes happening too fast.

Students of sociology are aware that the organization of any society roughly reflects the way that the people in it make their living. And the kind of work that people do, in turn, derives from the technological level of the society. Since technology is cumulative, it follows that change, for better or worse, is inevitable. (I could cite historical data for all this, but for the sake of argument, just take my word for it). It has been suggested in other contexts that the way to deal with the inevitable is to relax and, if possible, enjoy it. But for many audiophiles, their fun is threatened by the proliferation and confusion of many competing formats.

All this is by way of a psycho-historical introduction to the present state of home audio electronics. In past articles I've looked at the question of new formats and examined the factors that make them into hits or misses. As I see it, the majority of audio consumers are most interested in a format's convenience and only secondarily in its fidelity. Although I certainly don't discount the very low distortion and noise-free qualities of the CD format, its obvious attractions—for the average consumer—mostly reside in its durability and convenient handling. My evidence for all this is the fact

that several years ago the compact, convenient-to-use, and relatively rugged prerecorded cassette started to outsell LP's despite the LP's superior sound quality and lower price. For the same reasons, the latest figures show that CD's are now outselling cassettes in dollar volume. Next year's figures will probably show superior sales in absolute numbers as well.

What does all this tell us about the relatively sudden proliferation of new audio formats—and consumer reactions to them in the past several years? Are the Japanese (and others) engaging in a strange rite of mutual commercial throat-cutting? For example, no sooner did the CD format establish itself than digital audio tape (DAT) was introduced. Although the two formats were not really competitors any more than LP's and open-reel tapes were, consumer confusion was rampant. And consumers stayed away from the DAT format in droves!

Then, in 1986, the word was out that various companies were working on a recordable CD. About four years ago one company held a press conference during which it was claimed that their digital recorder/player would be on the market in about two years—and would cost less than \$500! It didn't happen then, but recently Carver and Philips announced the imminent release of a new breed of compact-disc recorders. A clue to the target market for the machine is given in the Carver press release: "Professional user net price of the PDR-10 is under \$8,000." In truth, I don't have a feel for the professional in the recording industry, but audio consumers are not likely to be waiting in line to invest so heavily in an unproven product with (for them) somewhat obscure advantages.

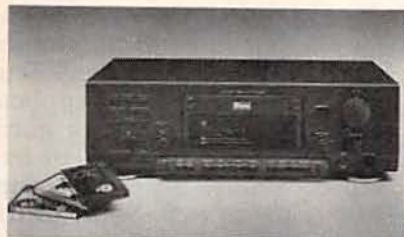
Planned obsolescence?

Over the years, I've occasionally defended the hi-fi industry against the recurrent charge of engaging in "planned obsolescence." The conversion from 78's to LP's, tubes to transistors, mono FM and record to stereo all struck me as worthwhile advances in the audio art rather than nefarious plots to sell new products. With today's technologies I'm not so sure.

Is Japan so filled with technologically obsessed marketers that they compulsively create new audio formats oblivious to consumer needs and reactions? Is their guiding philosophy something like the classic advertising agency approach, "Let's run it up the flagpole and see if anyone salutes."? If so it's an expensive and frequently self-defeating way to run an industry.

Several years ago, the consumer electronics trade publication *Twice* ran an interview with Hiroki Shimizu, general manager of JVC's Personal Audio Products Division. Mr. Shimizu's comments were so startlingly different from the usual self-serving presentations heard at new-product press conferences that they are worth quoting. Shimizu was troubled by what he called the ethical (!) aspects of today's proliferation of formats. He suggested that the industry was coming out with too many products too fast without considering the interest—or best interests—of the consumer. DAT technology, according to Mr. Shimizu, came too fast and the application came later; as a result the market has not taken off. The application should come first, he said. In his view the most important thing is how the new product will fit into the market.

Other voices of discontent are heard in the land. A writer in *The*



PHILIPS' DCC900 will be one of the first Digital Compact Cassette decks on the market.

New York Times suggested that the proliferation of competing formats is part of a conspiracy involving Sony (CBS Records), Matsushita (MCA Records), and Philips to somehow protect their record-company royalties from the predations of rabid home recordists. (If the recording machines don't sell because of consumer confusion, they won't be used to copy copyrighted material.) However, it seems improbable to me that the music and audio-product divisions of a company would play those sort of internal games with so much cash and prestige on the line.

Future formats

Do I have any advice to offer those seeking to keep their heads above water in the flood of new audio products? For one thing, read the articles extolling the virtues of this or that new format with a critical eye. Remember that most writers and editors believe that readers are automatically turned on by the *New!* Experience has shown, however, that large numbers of excited words devoted to the advent of a new audio format don't reliably predict its success.

Given the snowballing of technology, it's hard to make predictions, but certain developments seem inevitable. In a science-fiction story I wrote in 1977, I predicted that the turn of the century would see a fiber-optic cable that linked most homes in America. Among its many services would be the ability to call up any musical composition, pop or classical, from the world's recorded library. Separate musical software as such would be obsolete, as would, of course, the players that deliver it. I think such a development is inevitable, and it would finally put an end to all the format shenanigans. Or would it? **R-E**

HARDWARE HACKER

continued from page 91

and the odds of any positive cash flow that exceed costs are 600:1 against!

Those figures sound about right to me. Sometimes I've done almost that well on my own. And sometimes not. Selling an idea is a real rough row to hoe. One that could become a near impossibility if you are not a fully trained and well experienced insider knowledgeable about what is going on in trade journals, politics, economics, and the tech literature of the target field.

An invention-marketing firm is just a hired gun, similar to an ad agency or a resume-typing service. You pay them for their time and effort for such services as patent searches, listings in product newsletters, and participation in invention fairs—cash up front.

As we've seen a number of times in the past, the core problem lies in the absurd mythology surrounding today's patent system. Very simply, patents have little or nothing at all to do with the selling or marketing of an idea. For most individuals and most small-scale technical startups, *any involvement whatsoever with the patent system is virtually certain to end up as a net loss of time, energy, money, and sanity.*

Just about all hackers will tend to grossly overvalue a new idea. At one time way back in the golden age of inventing, ideas were occasionally worth as much as a dime a dozen. Today, they are worth less than ten cents a bale in ten-bale lots. Ideas gain value *only* when you can clearly demonstrate your end users actually getting off on them. And then *only* when those ideas are *already* in some saleable, competitive, promotable, and distributable form.

The key secret to selling an idea is very simple: *The buyer must come to you.* For our special resource sidebar this month, I have gathered together some ideas that can help you to profit from your ideas.

Two essential magazines are that *Midnight Engineering* and the *continued on page 108*



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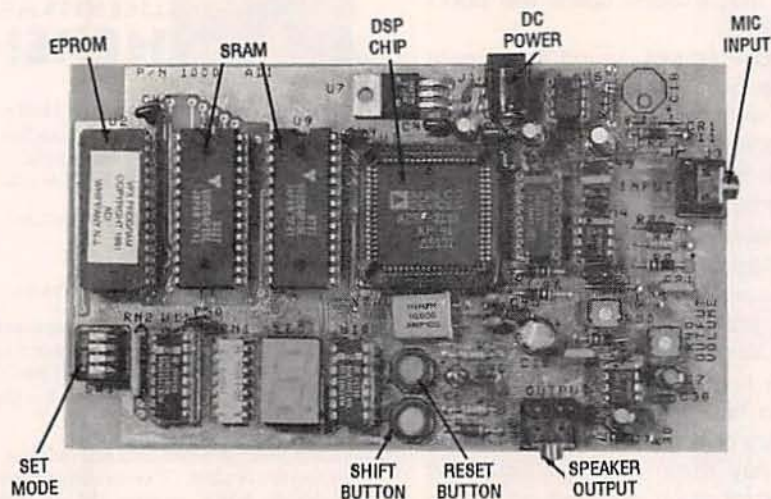


FIG. 9—THE VFX PROTOTYPE. Carefully check the board for solder splashes and bridging before applying power.

button and the LED display should count fast enough so that all the segments (an "8") appear dimly lit.

Remove power from the board and install the two RAM's (IC8 and IC9). Apply power to the board. The LED should again display "6." Press the SHIFT button and the LED should display "0." If any RAM errors occur, they will cause the LED display to increment.

Next install IC3 and IC5. Connect your speaker or headphones to J2 and reapply power. Press the SHIFT button twice and a tone should be heard in the headphones or speaker. Install IC4 and connect a microphone to J3. Apply power and press the SHIFT button three times. Then speak into the microphone and your voice should be heard through the headphones. Adjust potentiometers R50 and R40 for minimum distortion. Now that your VFX board is working, you can change the DIP switches according to Table 1 for the other three effects.

As mentioned before, there is a test mode that can help troubleshoot the VFX processor. It is activated by setting the DIP switches as shown in Table 1

and pressing the reset button. The test mode individually tests the system RAM, the CODEC, and the LED display.

In the test mode the external SRAM is constantly written to and read, and the number of errors are displayed on the LED. If the LED display is blank and all the power supplies are normal, there is something wrong with the LED or the driver. If the LED has a number other than zero, there might be a problem with the SRAM.

The CODEC data is received and immediately retransmitted, so the microphone input is echoed back the headphones. If there is no output or if the output doesn't sound like the input, there is a problem. If there are no other fault indications and the microphone and speaker are working, there might be a problem with the CODEC. If nothing happens and the power supplies are normal, there might be a problem with the digital signal processing chip or the EPROM.

Where to go from here

The VFX processor is intended to demonstrate in, an enjoyable way, the capabilities of

digital signal processing. The four applications programmed into the VFX board are just four out of many possible applications. The VFX processor hardware is capable of being reprogrammed to perform other functions as well. Some of the possibilities are speech recognition, active noise cancellation, voice compression/recording and a spectrum-shifting hearing aid.

For example, the VFX processor could easily recognize the numbers from 0 to 9 and display them on the LED indicator. That requires that the speech be converted into the frequency domain and the spectral peaks of the sound be compared with pre-stored templates. The closest matching sound is selected and displayed on the LED. The processor could then generate the DTMF signals for that number to make a voice-activated telephone dialer.

A voice compressor/recorder converts an audio input into the frequency domain, picks out the most prominent spectral energies, and stores them in data memory as frequency and amplitude. The technique can reduce the amount of data that must be stored compared to that from conventional digitizing processes from 6.5K words per second to 650 to 300 words per second. The VFX board with 8K words can record approximately 12 to 25 seconds of compressed speech.

Active noise cancellation is being developed for applications ranging from muffling the sound of automobile engines and industrial machines to eliminating the background hissing noise in fighter-aircraft intercom-system headphones. Similar applications for the VFX board are being developed. Let us know if you have any other applications you would like programmed into the VFX processor. If you are interested in programming your own applications, look into the EZ-LAB system sold by Analog Devices that has been referenced in this article. It is an affordable way to implement small- to medium-sized algorithms. R-E

DRAWING BOARD

Video scrambling.

ROBERT GROSSBLATT

Looking at a line of video on an oscilloscope or waveform monitor can be a real eye opener. As we discuss the various factors involved in video scrambling, you'll need a good understanding of video to follow along. You'll also need some equipment to view the waveform, other than on a TV set. For a good background on video, get your hands on the series of Drawing Board columns I did on video from January to November 1990. You'll probably be able to find them in your library if you don't have the back issues.

The starting point for any would-be unscrambler (hereinafter referred to as "us") is that scramblers (hereinafter referred to as "them") start out with a signal that's exactly the one we want to wind up with. Video originates in the clear, gets messed up one way or another by them, and is sent to us. Our job is simply to undo what they've spent a lot of money doing.

You don't have to be a rocket scientist to mess up video—that is true both aesthetically and scientifically. The hard part is to do it in such a way that you can put it back together again. This means that there has to be a rigorous approach—almost a mathematical one—to tearing the signal apart.

Take a look at—and get intimately familiar with—the typical line of video shown in Fig. 1. While most of the time on the line is devoted to the picture area, it's the control area where the real work is done. The signal in the picture area determines what you'll be seeing on the screen but the stuff in the control area is what tells your TV where to put the picture and how it's supposed to appear.

The control area is blown up in Fig. 2, and the information in it is a graphed function of time and voltage. By the way, most video people

like to talk about "units of video" rather than voltage for the same reason that audio people like to talk about decibels rather than voltage.

When the NTSC video standard was established, the two most basic decisions made were that it would range from 0 to 1 volt peak-to-peak, and that one voltage range would be reserved for picture and one would be reserved for control. As we go through our discussion on scrambled video, I'll talk sometimes about video in terms of IRE units and other times about voltage. The

two are directly related as shown on the Y axis of Fig. 2.

The bottom line of the picture is 0 IRE units which is about 0.3 volts up the IRE scale. That point is important because it's both the defined level for black video (no picture on the screen) and the upper limit for any control signals. (There's a slight ambiguity here when you examine the colorburst but we'll get to that later.) For the moment, we can consider everything above 0.3 volts as picture and everything below that as non-picture.

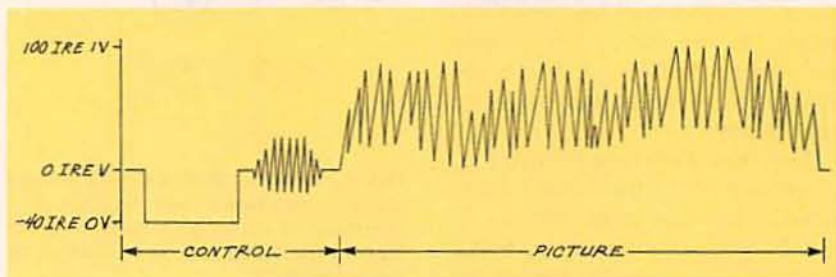


FIG. 1—TYPICAL LINE OF VIDEO. Most of the line is devoted to the picture area, but it's the control area that we're interested in.

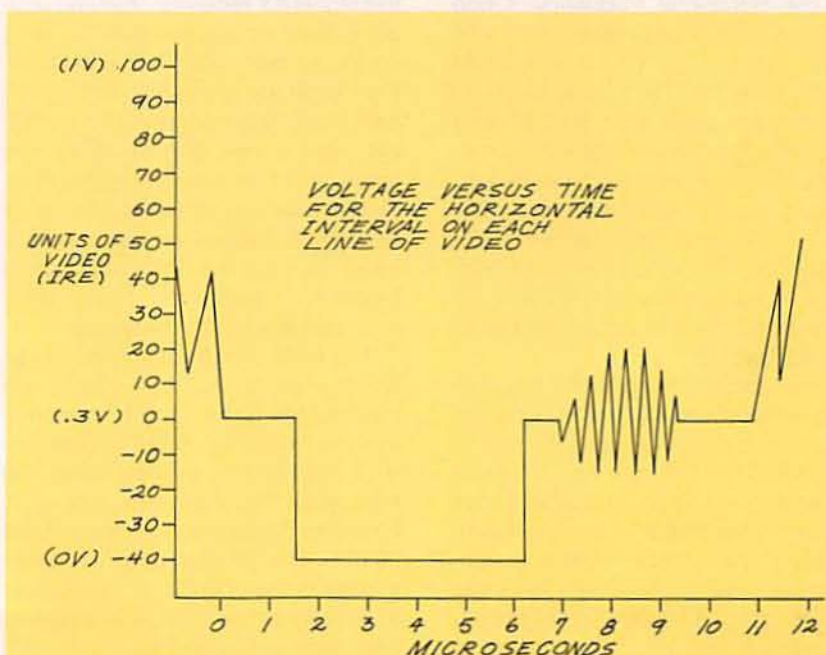


FIG. 2—THE CONTROL AREA. The NTSC video standard says that the signal can range from 0 to 1 volt peak-to-peak.

That signal definition is the basis for most of the hardware in every NTSC-compatible TV ever made. Your TV contains circuitry that expects control information to be below 0.3 volts and picture information from 0.3 to 1 volt. That's important because it is the starting point for scramblers; when you get rid of some of the control information, a standard TV can't display the picture. Remember that the horizontal sync pulse defines the end (or, depending on your point of view, the beginning) of a line of video. If the TV doesn't see it, it won't know how to display the line on the screen, and the result will be that the TV will end one line and start another one at some random point on the screen.

The freewheeling retrace frequency of the TV will come close to the one sent by the broadcaster, but it won't match exactly. What you'll see on the screen will be something like Fig. 3. The curved line running down the center of the screen is the horizontal interval sent by the broadcaster.

Three things are happening in Fig. 3. The first is that the line is curved because the horizontal circuitry in your TV runs at a frequency that's not exactly the same as the broadcast horizontal frequency. The TV can accept a certain amount of drift in the horizontal frequency. Once upon a time a horizontal control was built into on the TV so you could hand tune the TV to the received signal. Although that control isn't around any longer (except sometimes as a trimmer on a circuit board inside the TV), the tolerance is still there. Modern TV's can automatically lock onto the broadcast horizontal frequency so there's no reason for the horizontal control to be accessible.

The second thing that's happening is that the line is in the center of your screen. The reason for that is simple. The TV's horizontal circuit uses the received horizontal pulse as an instruction to move the beam back to the left side of the screen. Because the scrambled signal has anything but a recognizable horizontal sync pulse, the TV zips the line back to the left side of the screen whenever it reaches the right side.

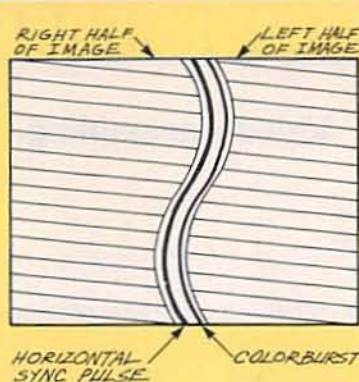


FIG. 3—A FREEWHEELING RETRACE won't match the frequency sent by the broadcaster. The curved line running down the center of the screen is the horizontal interval sent by the broadcaster.

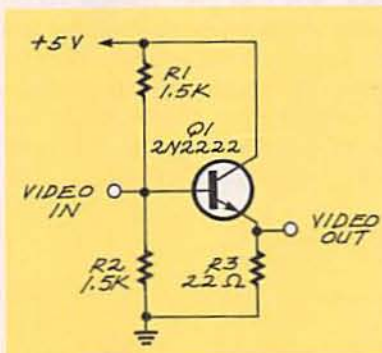


FIG. 4—A VIDEO BUFFER isolates one stage of hardware from another. The transistor is set up as a buffer and the level of the video can be controlled by the value of R2.

Because that has nothing to do with the signal it's receiving, the line usually shows up at some random spot on the screen. The TV's freewheeling frequency is close to the broadcast horizontal frequency, so the TV will start a new line at about the same point in the broadcast line. That means you'll see the broadcast horizontal interval on each line at more or less the same horizontal location on the screen. The result is a curved line down the screen.

The third thing happening on the TV screen is that the colors are messed up. Because the horizontal sync is missing, the TV circuitry isn't seeing the colorburst in the right place, so there's no reference for either the intensity or color of the picture. The TV then uses whatever it sees in the colorburst location as a reference for both the intensity and color of the image.

You can see now that by simply getting rid of horizontal sync, the

resulting video signal will be completely messed up. The best way to appreciate that, and a good way to get into video hardware, is to build something to demonstrate how all this stuff really happens. That's right, our first piece of hardware is going to be something that will let you scramble video. And, as far as the law is concerned, I'm pretty sure that nobody's going to become very upset.

We'll need a source of real video. That can be anything from an NTSC generator to a line-level video signal from the back of a VCR. You'll also need a scope to look at the video waveform and a TV to look at the picture. You can do without the latter but the former is a must. I'm not going to beat you up any more about getting a scope, but if you don't have one, get one. If you don't get one, this series of columns, while informative, will be somewhat less than useful from a practical point of view.

To get started, because we're building circuitry that is going to use an external signal, the first thing we have to do is buffer it. That is done for two reasons. The first is that we have to be able to control the level seen by our video circuitry, and the second is so that a wiring error on the breadboard isn't going to send unpleasant voltages back to the signal generator or VCR. The results could be a bit nasty.

Video buffers are just like any other buffer—they're simple circuits that isolate one stage of hardware from another. Think of it as being like an electronic fuse. The easiest way to build a buffer is with a single transistor as shown in Fig. 4. The transistor is set up as a buffer, and the level of the video can be controlled by the value of R2. You can also put a potentiometer in series on the line feeding the video to the base of the transistor and trim the level that way.

Although the NTSC video standard calls for a signal that's 1-volt peak-to-peak, most VCR manufacturers don't strictly follow that standard when it comes to a video output signal. If you put the signal on a scope, you'll probably find that it's a bit higher than that. If that's the

continued on page 109

COMPUTER CONNECTIONS

The Cheshire Cat, multimedia, and vision.

JEFF HOLTZMAN

Vision, according to the American Heritage Electronic Dictionary, can be defined in five ways: 1. The faculty of sight. 2. Unusual foresight. 3. A mental image produced by the imagination. 4. Something, as a supernatural sight, perceived through unusual means. 5. One of extraordinary beauty.

In the business world, definition 2 is what people usually think of. Actually, definition 3 is most important. Persons with unusual foresight help bridge short-term gaps between today and tomorrow. Persons with imagination set long-term goals and directions, and inspire others to try to move in those directions to achieve those goals. Companies are typically founded by Type-3 people, and run by Type-2's.

Starting about 250 years ago during the dawn of the industrial revolution, technical vision and imagination in the western world focused on building tangible items to ease the time involved in producing, transporting, and defending necessities. After about 200 years of widespread social effort, most of those problems were solved, so persons with visionary imagination shifted focus to a different set of problems. From these origins was born the computer industry.

Early work in that field centered on doing the same kinds of activities people had been doing—e.g., accounting and typing—only faster. Things started to get interesting when Ted Nelson, Doug Englebart, and others realized that the computer had created a whole new world, a "virtual" world. Again the American Heritage, this time on virtual image: *An image from which rays of reflected or refracted light appear to diverge, as from an image seen in a plane mirror.*

There is a virtual world behind the CRT, from which *imaginary* light rays are diverging, rays that until recently

were visible only to mathematicians, computer scientists, and software engineers. Now, thanks to Nelson and company, and more recently to video games and the Macintosh (and let's not forget Microsoft Windows), that Cheshire cat image is becoming accessible to more and more people.

Graphics editors let artists reach in and take hold of some of that virtual Play-Dough a proprietary term. On-line references let writers and researchers tap into the knowledge of the world. Three-D CAD programs let architects and product designers "build" prototypes without cutting wood or metal. Medical imaging devices let medical technicians and researchers non-intrusively create images of body parts. Serious and popular composers use synthesizers to create new musical forms.

Computer technology has penetrated many disciplines, but it still has a long way to go. Take video editing for one. The traditional method for editing videotape and film is to do a lot of physical fast-forwarding and rewinding. The efficient way to do the job is via random access, instantly jumping from any frame to any other. Due to the immense storage required for video information, effective random access completely dwarfs the storage and bandwidth capabilities of today's most powerful personal computers and low-cost networks.

Multimedia

This is where Type-3 vision comes in. That vision centers around a topic of growing public interest: multimedia. Don't be misled by popular computer, video, and games magazines. Multimedia is not just putting a sound board in a PC, or adding a CD-ROM drive to a Nintendo. The real promise behind multimedia is twofold: 1) To bring the whole world into that virtual image

behind the CRT, and 2) To connect your virtual image to mine and everyone else's.

The requirements for rich multimedia are simple: 16-bit audio, full-screen 30-frame-per-second video, 24-bit (photographic-quality) imaging, fast access to lots of textual and numeric data—all of which must be available on-demand, synchronously, instantaneously, at any time, and (eventually) anywhere in the world.

It would take a powerful mainframe to provide that kind of capability today. On the other hand, a run-of-the-mill 486 today exceeds the computational power of a mainframe of a decade ago. Assume then that within the next decade, "computers" that meet those requirements become available. Those "computers" will have built-in general-purpose digital signal processors (DSP's) for compressing and decompressing audio and video data, and for doing fax and modem chores as well. Semiconductor memory will be measured in the gigabytes, and permanent storage will be measured in the terabytes (on *personal* computers; mainframes will have even more). Optical storage may finally, after decades of promise, become cost effective.

Tomorrow's computers will have built-in connectivity to office systems, commercial databases, entertainment banks, and interactive educational courseware. Transmission speeds of these new networks will make Ethernet and Token Ring look like box turtles.

Those systems will have built-in docking technology (both hardware and software) for portable notepad/planner systems based on today's fledgling pen-input technology. They will have lightweight, flat, high-resolution, true-color displays—and printers—and will accept keyboard and pen input indiscriminately. They will communicate via a universal dig-

ital communications system that will probably come about as some sort of joint venture between AT&T, the cable TV companies, the independent networks (CNN, FNN, Fox), media giants like Time-Warner, and major computer companies.

There will be gobs and gobs of data flowing around, and lots of confusion about who owns rights to what. New kinds of copyright issues will keep lawyers busy for the next century. Students and researchers will have unprecedented opportunities to cheat. Illegal data tapping and decoding (akin to today's cable TV descramblers) will provide a data underground and new forms of law enforcement (the Data Police).

That technology will not replace today's TV, VCR, stereo system, video game, fax, telephone, or computer. However, those technologies will come to be seen as modular, interoperable pieces of a larger system in which all the pieces can plug and play—for those who want to.

From this perspective, multimedia begins to look like *everything* connected with computers, consumer electronics, and entertainment. Grandiose? Maybe. But ask yourself why IBM is contemplating a half-billion dollar deal with Time-Warner, why IBM and AT&T are both working like crazy to get fiber-optic data rates to work over copper cabling, and why Apple is partnering with Sharp and Microsoft with Sony.

Personal computers revolutionized typing, accounting, and publishing in the 80's. The 90's will see even more radical and pervasive changes.

That's the vision. Question: How will you participate?

Product watch

For years the phrase "reasonably priced tape backup" was a contradiction in terms, but that is no longer the case. Figure 1 shows one of the best deals around: the Jumbo 250 from Colorado Memory Systems. It's a high-quality 250-megabyte QIC-80 tape drive that can fit in a 3.5 inch or 5.25 inch bay, and it runs off a standard floppy-disk controller.

The Jumbo 250 includes a special cable adapter that runs from the drive to the floppy controller; the cable from the floppy drive(s) plugs



FIG. 1—COLORADO'S JUMBO 250 packs 250 megabytes of data on a \$20 tape cartridge in less than two hours.

into the Jumbo's cable. Other than mounting the drive and copying software to your hard disk, that's the extent of installation.

Backup software included with the drive runs in both menu-driven and command-line modes; the latter allows unattended backup via scheduled batch files. If hard-disk capacity exceeds that of a tape, the software will store additional data on additional tapes. In addition, the software has several options, including password protection, the ability to back up and restore Novell NetWare bindery (user access rights) files, and several types of software-based data compression. Using compression is faster than not using it; I have no trouble backing up about 170 megabytes of data on a single tape in less than an hour.

You can use the menu-driven mode to create a tag list, or list of files to back up, and then use the command-line mode to back up the files on the list. One nice feature is its ability to append multiple backup volumes to the same tape, which gives you the ability to perform daily backups simply and quickly. My main complaint with the software is that it forces you to restore files to their original locations. Sometimes, especially in a networked environment, it's helpful to be able to restore files elsewhere.

Many installation options are available, including a case for external mounting, numerous special cable and connector arrangements for special PC's (such as PS/2's), and several dedicated tape-controller boards that provide increased

speed and hardware data compression. Colorado also sells software to control the drive under several varieties of Unix (SCO, Interactive AT&T, and Intel).

The drive includes a one-year warranty, toll-free technical support and access to a BBS. If you shop around, you can pick one up for \$250 mail order. By way of comparison, just a few years ago my trusty 80-megabyte Irwin backup unit cost three or four times that amount. For small offices and Windows power users, this is a must-have item.

For more power and flexibility in tape backup software, check out Sytos Plus. It has several nice features, including the ability to work with multiple devices, including the Colorado, numerous digital audio tape (DAT) and 8mm formats, IBM's optical read/write disk, and hard and floppy disks; others are being added all the time.

Sytos also supports OS/2, whereas Colorado does not (yet). Sytos is routinely bundled with numerous high-capacity tape drives; the company claims more than a million users.

Probably the nicest feature is Sytos' more integrated way of creating backup sets. Whereas Colorado's TAPE.EXE forces you to create tag lists and then manually create batch files with numerous parameters, Sytos allows you (in the menu mode) to create "procedures" containing both tag list and configuration options, and then run various procedures from the command line.

Sytos also has more extensive

documentation than Colorado. It covers different kinds of backups, and methods for creating backup schedules.

Sytos will allow you to restore files from tape to new locations with new names; the only feature it lacks (and that Colorado supplies) is a gauge that indicates progress in formatting a tape.

News bits

What's larger than a calculator and smaller than a notebook PC? Better yet, what's the size and weight of a paperback book, has a 2-bit RISC processor, a multitasking, object-oriented operating system, and a 6- x 3-inch LCD screen or pen input and visual display? Easy: Apple's Newton, the first handheld device for jotting, sketching, scribbling, figuring, doodling, making lists, and subsequently moving that data to a larger computer or another user via fax, modem, or network. Initial specs include flash EPROM, 1 to 20 megabytes of RAM, PCMCIA expansion cards, sound output, an infrared data link to other Newtons and desktop Macintoshes, and wired links to both Macs and PC's. In addition to the text and graphics doodle pad, Newton will have an address book, scheduler, and an intelligent assistant that will understand and act on commands like "fax this story to Brian." Newton is scheduled for release around January of 93, and reportedly will cost \$500-\$1000. There are also rumors of another Apple-developed handheld, this one called Sweet Pea, with CD-ROM and the ability to play QuickTime scripts. It sounds a lot like the device Microsoft is developing with Sony.

IBM has publicly demonstrated FDDI running on copper shielded twisted pair (STP) cabling, thus paving the way for a potential ten-fold increase in bandwidth to desktop computers—and other devices. Not to be outdone, AT&T Paradyne has announced a similar technology, with claims that it could spur the nascent multimedia industry by delivering on-demand and interactive video services.

Nintendo and Sega are going at it neck and neck, and in the process,

PRODUCTS DISCUSSED

- Jumbo 250, Colorado Memory Systems, 800 South Taft Ave., Loveland, CO 80537, (303) 669-8000.
- Sytos Plus, Sytron Corporation, 124 Flanders Road, P.O. Box 5025, Westboro, MA 01581-5025. (508) 898-0100.

taking a pot-shot at the computer industry. Sega plans to introduce two places by Thanksgiving a \$300 CD-based game that delivers quality audio and live-action video; Nintendo plans to introduce a similar \$200 unit early next year. Sega is working with Sony to produce games related to movies, e.g., Spielberg's *Jurassic Park*. Early reports indicate that Sega's device will include only half-speed, quarter-screen animation, whereas the Nintendo unit will do a full 30 frames per second.

R-E

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SLOPING VEE ANTENNA

continued from page 78

phosphor-bronze wire is preferred over stranded copper or aluminum wire because its spring qualities avoid kinks. It is almost impossible to tangle this kind of wire, especially important if you want a field-transportable antenna system. Nevertheless, if phosphor-bronze wire is too expensive (about \$2 per foot) or difficult for you to obtain stranded copper or aluminum wire can be substituted. The shorting wire was 16 AWG bare, stranded-copper wire.

Solder all connections if the antenna installation is permanent. But if you plan to set up and take down the antenna frequently, be sure that there are clean metal-to-metal mechanical connections between all conductive components.

The terminating resistors

must be capable of handling a significant amount of power if the antenna is to be used for transmission. Non-inductive carbon-film power resistors, rated for 300 ohms $\pm 10\%$, were specified for the test antenna. They had measured DC resistances of 307 and 314 ohms. As a general rule, the resistor power dissipation rating should be 10 to 20% of the maximum transmitter output power. Check the termination resistors for overheating.

For receiver-only applications, almost any low-power dissipating resistor with the correct resistance value will be satisfactory. The test sloping-vee antenna showed good VSWR performance and reception with 300-ohm, 1/4-watt carbon resistors.

The measured impedance bandwidth of the 15 to 50 MHz vee is shown in Fig. 14. A network analyzer measured the input VSWR of about 150 feet of

RG-213/U coaxial cable and was below 2:1 at all frequencies between 10 and 60 MHz; it was particularly good between 20 and 30 MHz. The undulations in the VSWR curve shown in Fig. 14 were caused by the transmission line's frequency-dependent transformer action acting on the sloping-vee input impedance.

VSWR measured directly at the antenna input is slightly higher because cable loss lowers VSWR. This measurement was made, and the VSWR was just over 2:1 in the following band: 38 to 40 MHz; 44 to 47 MHz; and 52 to 57 MHz. At all frequencies below 58 MHz, the sloping-vee input VSWR was less than 2.5:1. The test antenna easily exceeded the bandwidth design objective, and it provides very good broadband performance. In field tests the sloping-vee performed well as a transmitter antenna down to frequencies of about 4 MHz. R

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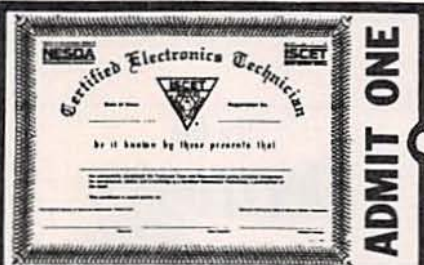


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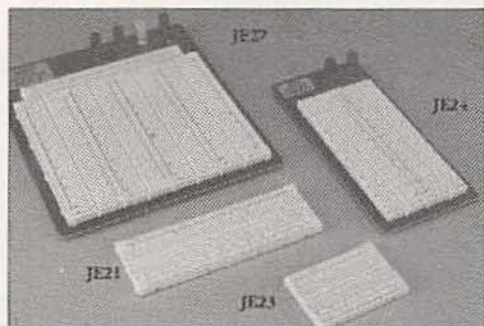
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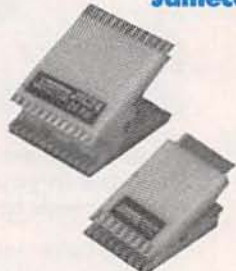
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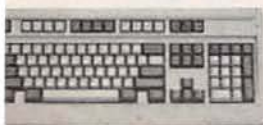
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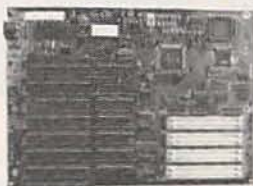


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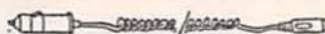
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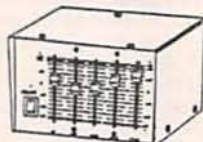
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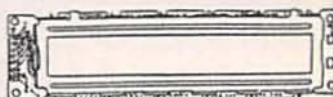


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HARDWARE HACKER

continued from page 93

Whole Earth Review. There are bunches of independent and non-profit inventor's organizations out there. One I can heartily recommend is Ed Zimmer's *Inventor-Entrepreneur Network*. For other regional sources, check out the *Encyclopedia of Associations* that you will probably find at your local library.

No, I just do not know of anyone anywhere who is dumb enough to buy raw, unproven, or undeveloped ideas. But I do know of several someones who sometimes might be interested in looking at tightly targeted products *if those products are now in their pre-production prototype stage and currently under active end-user beta testing*.

For instance, Mark Gottlieb of *Design Tech International* is looking for innovative approaches to low-end consumer electronics, especially for those items that can be blister packed and need no consumer smarts to use.

Dennis Carper of *Redmond Cable* is seeking tested and proven interconnect and adaptor products that clearly solve obvious and well-defined problems.

John Simonton of *PAIA* (and a frequent author in **Electronics Now**) sometimes seeks out items with kit possibilities, especially if they are related to MIDI or electronic music.

And Steve Ciarcia of his *Micro Mint* is occasionally interested in any embedded processor applications—if they are unique.

Besides my own PSRT RoundTable on *GENie*, you might also want to check out their HOSB, short for *Home Office and Small Business*. I've also formed my loosely knit *Synergetics Consultants Network* that centers on our voice helpline. Give me a call if you need more information.

New tech lit

From *Texas Instruments*, seven pounds of revised linear data books. Volume I is on op-amps; volume II is on A/D, DSP, and video; and volume III is on voltage regulators and

really oddball stuff.

A pair of very readable new books: *The Triumphs and Trials of an Organ Builder*, by Jerome Marlowitz, CEO of *Allen Organ*, and published by the *Vox Humania Press*. Among the other things, it reveals how trivially easy it is to have a technically solid and perfectly valid patent busted in court. Just because some epsilon minus does not happen to like you.

Plus *Accidental Empires* by the pseudonym *Robert X. Cringley* newly published by *Addison Wesley*. Subtitled *How the boys of Silicon Valley make all their millions battle foreign competition, and still can't get a date*. This book has double handful of very funny one liners in it. But otherwise it reads like something that Cringley would write.

I've found very few trade journals devoted to electronic servicing. One useful new one, though, is *MSM, the Magazine of Service Management*. The magazine puts a big emphasis on computer service and identification of sources for printer and disk-drive replacement parts and assemblies.

A great collection of navigation books, GPS (global positioning satellites) and otherwise, is offered by the *Navtech Information Service*. And a new *Spread Spectrum Scene* labor-of-love newsletter has recently started publication.

Two firms apparently still offer top octave generators and other classic electronic organ chips. The first is *Fistell Microelectronics* and the other is *Keyboard Systems*. The latter also builds workaround replacement modules for chips that are truly unavailable.

Turning to some of my own products, yet another obvious and major product selling resource is my recently improved *Incredible Secret Money Machine II*. The autographed copies are available per my nearby *Synergetics* ad.

As usual, I have gathered many of the resources mentioned together into the *Names & Numbers* or the *Product Marketing Resources* sidebars. Be sure to check those out before you use our no-charge tech helpline or call for a free hacker secrets brochure.

R-E

ATV DOWNCONVERTER

continued from page 84

provided for you to make your own board, and the parts-placement diagram is shown in Fig.

First install resistors R1–R13, and R15–R17. Next, install all capacitors except the chip capacitors and C10. Install mixer Q1, and then wind and install coils L1, L2, L3, L5, L6, L7, L8.

Coils L1, L2, and L3 are three turns each of 20 AWG tinned wire wound around a No. 8 screw as a form (see Fig. 5) and then stretched to a length of 0.3 inch with the turn spacing evenly maintained. All three of these coils must be tapped as shown in Fig. 5. The lead from Q1 (which can be coaxial 50-ohm line) has its center conductor soldered to L1 at $\frac{3}{4}$ turn from the grounded end. Resistor R5 is soldered $1\frac{1}{2}$ turns from the end of L2 that connects to R6, R7, and C8. Coil L3 is tapped at $\frac{1}{2}$ turn from the grounded end.

Coils L6 and L7 are 8 turns each of 22 AWG enamelled wire wound on a No. 8 screw. The screw is removed after winding the coil. Coil L8 is $9\frac{1}{2}$ turns of 22 AWG enamelled wire, wound the same way as L6 and L7. However, after winding, the No. 8 screw is removed and a ferrite tuning slug is screwed into the winding as shown in Fig. 5. RF choke L5 is installed as if were a resistor.

Install Q2, Q3, D1, D2, and D3. Now install the chip capacitors. Chip capacitors require special installation procedures—and they all mount on the solder side of the PC board. Figure 6 shows where all of the chip capacitors, C10 (which we'll get to in a moment), and Q1 are mounted on the solder side of the board. As for the chip capacitors, first tin the area on the PC board where a chip is to be installed. Then hold the chip in place with the tip of a small screwdriver or tweezers and tack solder one side. After it's tacked in place, fully solder both sides of the chip.

Now install Q1, whose long lead is the drain. Make sure you

use a grounded iron and work in a static-free area. Treat Q1 as you would a delicate CMOS IC. The tuning potentiometer (R14) can be mounted in different positions for added flexibility; it can be mounted off the board for remote tuning purposes.

Make sure all holes marked "G" in Fig. 4 have jumper wires passed through them and soldered on both sides of the PC board as shown in Fig. 7. Also, both sides of the board must be grounded together with copper foil tape, also as shown in Fig. 7. Once the tape is in place, solder both sides.

Next make capacitor C10. Take a small square of G-10, 0.062 material (the same as the PC board material) and trim it to a $\frac{3}{16}$ -inch square. Install it on the solder side of the board as shown in Fig. 8. Connect coaxial 50-ohm cables to J1 and J2, and DC power leads to D3 and ground. Set trimmer capacitors C1, C5, and C6 to about 20% of maximum, and set C9 to about 80% of maximum. If you use R14, it can be set halfway. If R14 is not used, R10 should be temporarily connected to a supply of about +8 volts. Figure 9 shows the author's prototype.

Tune up

Tuning consists of peaking the tuned circuits for best reception. Using a frequency counter connected across R12, adjust C9 for a nominal frequency of 370 to 375 MHz. If installed, R14 should vary that by about ± 15 MHz. If R14 is not installed, 0 to +12 volts applied to R10 should do the same. The oscillator might stop if less than 2 volts is applied to R10—which is acceptable as long as you can obtain a frequency range of 30 MHz.

Connect the converter to a TV set tuned to channel 3 and to an external antenna for ATV reception. Find a signal and peak L1, L2, and L3 for the best picture. You can also use an RF signal generator tuned to 435 MHz if no on-the-air signal is available. As a last resort, you can also peak L1, L2, and L3 on noise.

It is also possible to experimentally peak the converter on

UHF channels 14, 15, or 16 if no other signals are available. Set C9 for a L.O. frequency of around 410 to 420 MHz. Note: This is only to see if everything works if there's no other way to obtain an ATV signal and you have no access to a signal generator. You will later have to re-peak the converter to 420 to 450 MHz.

If a sweep generator is available, simply peak the converter for a response as shown in Fig. 10. By trimming C10 (use a file on the edge of it) you can also experiment with the coupling and resultant bandpass shape. You can also do this with a calibrated RF signal generator and a receiver and/or RF voltmeter, but this will take more time.

The converter should be mounted in a weatherproof metal box, if outdoor use is intended. A metal box reduces stray signal pickup, and also protects the converter from damage.

If you will be remote-tuning the converter (as was shown in Fig. 3), the converter should be mounted right at the antenna or very close to it. That permits a short cable from J1 to the antenna, reducing signal losses. The converter can then be mounted as far as 300 feet from the TV monitor. R-E

DRAWING BOARD

continued from page 96

case, you should trim the level because the circuits we'll be building expect a 1-volt signal.

The only other thing to notice here—there just isn't much to the circuit at all—is that the video signal being fed to the base of the transistor is related to both positive voltage and ground through R1 and R2. The circuit is going to run on a regulated 5-volt supply; it must be steady because the level of the supply voltage is going to have an effect on the level of the video. Wire up the circuit shown in Fig. 4 and get the video source in place. When we get together next time we'll start designing some kind of circuit to screw up the signal. R-E

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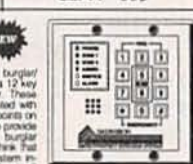


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